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Simulation of Transient Prescription Experiments in the
Transient Reactor Test Facility (TREAT) Using Serpent

by

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Transient Reactor Test Facility (TREAT) Using Serpent

Thesis Abstract -- Idaho State University (2018)

The Transient Reactor Test Facility, or TREAT, is a test reactor designed for putting materials and fuels under extreme conditions that ran for almost 35 years until it was put on standby in 1994. After the nuclear accident at Fukushima Daiichi in 2011, there became a renewed awareness of the need for the accident testing for reactors. There were calls for TREAT to be brought back into operation. This would allow further accident testing of nuclear fuels and materials to restart. TREAT achieved its first criticality after 23 years on November 14, 2017. But something else has happened while TREAT was offline. Computers have gotten faster, and accurate simulations and models of reactor behavior has become financially and technologically viable. Using Serpent, a Monte Carlo reactor physics code developed at the VTT Technical Research Centre in Finland, we can show that it is possible to accurately model transients for TREAT.

Key Words: Kinetics, Modeling, Monte Carlo, Serpent, Transients, TREAT

Introduction to TREAT

TREAT is a graphite moderated, air-cooled research reactor designed to test reactor fuel pins under extreme conditions of overheating and overpowering. These operations are called transients tests, where the target is placed in the reactor and subjected to a rapid pulse of high-

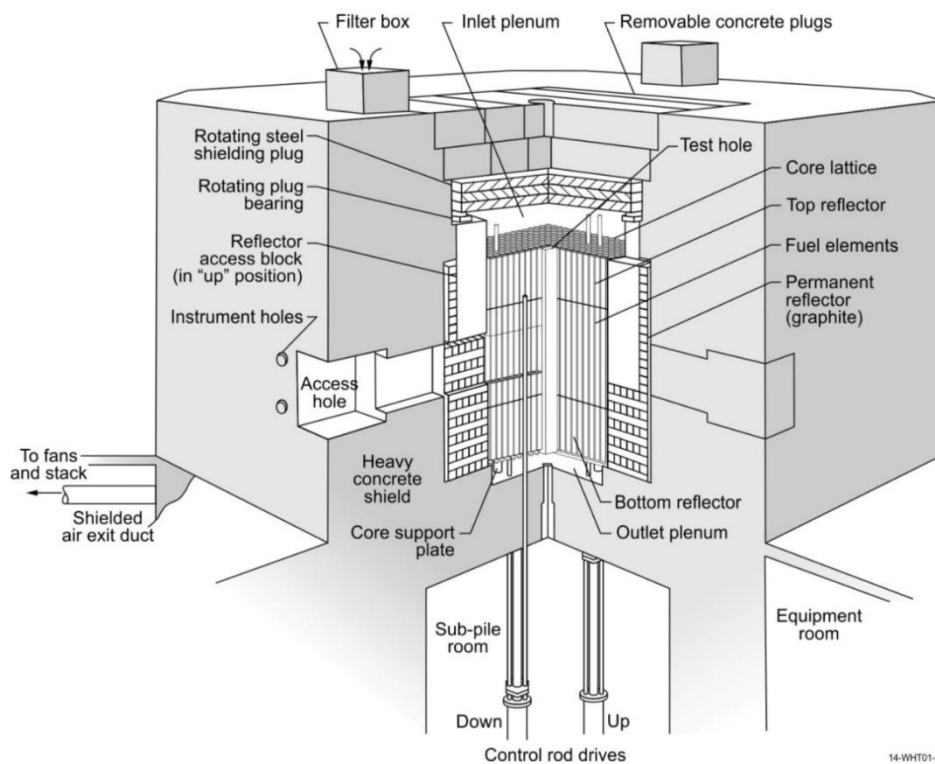


Figure 1 — TREAT Design [Bess & DeHart, 2015]

power radiation. The transients can emulate fuel meltdowns, metal-water reactions resulting from both high and low pressure steam, thermal interaction between overheated fuel and coolant, and the transient behavior of ceramic fuel for high temperature systems [Freund, 1958]. TREAT is a great resource for engineers to safely test their designs for worst-case scenarios.

The TREAT complex was constructed in 1958 at Argonne National Laboratory's Argonne-West, now part of Idaho National Laboratory. Located 28 miles west of Idaho Falls, TREAT is comprised of two buildings, the reactor building and the control building. The reactor building is an aluminum-sided structure with a steel frame and has a 35 ft. tall high bay area where the reactor, fuel storage pit, instrument room, and equipment are housed. The control rod driving mechanisms are housed directly underneath the reactor in the basement. There is also a

bridge crane for moving materials into and out of the reactor. The control building was single-story and made of concrete, and houses the control room, where the reactor is remotely controlled [ANL-6034]. In the 1980s it was changed to a portable building. The TREAT

facility's close proximity to hot cells at the Materials and Fuels Complex- the Hot Fuels Examination Facility and the Fuel Conditioning Facility, allows ample opportunity for post-irradiation testing to be done with the transients run at TREAT. In 1994, TREAT was placed on standby. After the accident at the Fukushima Daiichi Power Plant in 2011, an effort was made to have TREAT restarted to continue performing safety tests on nuclear fuels and materials. A congressional mandate to restart TREAT for more accident-tolerant fuels was passed. TREAT achieved its first criticality after 23 years on November 14, 2017.

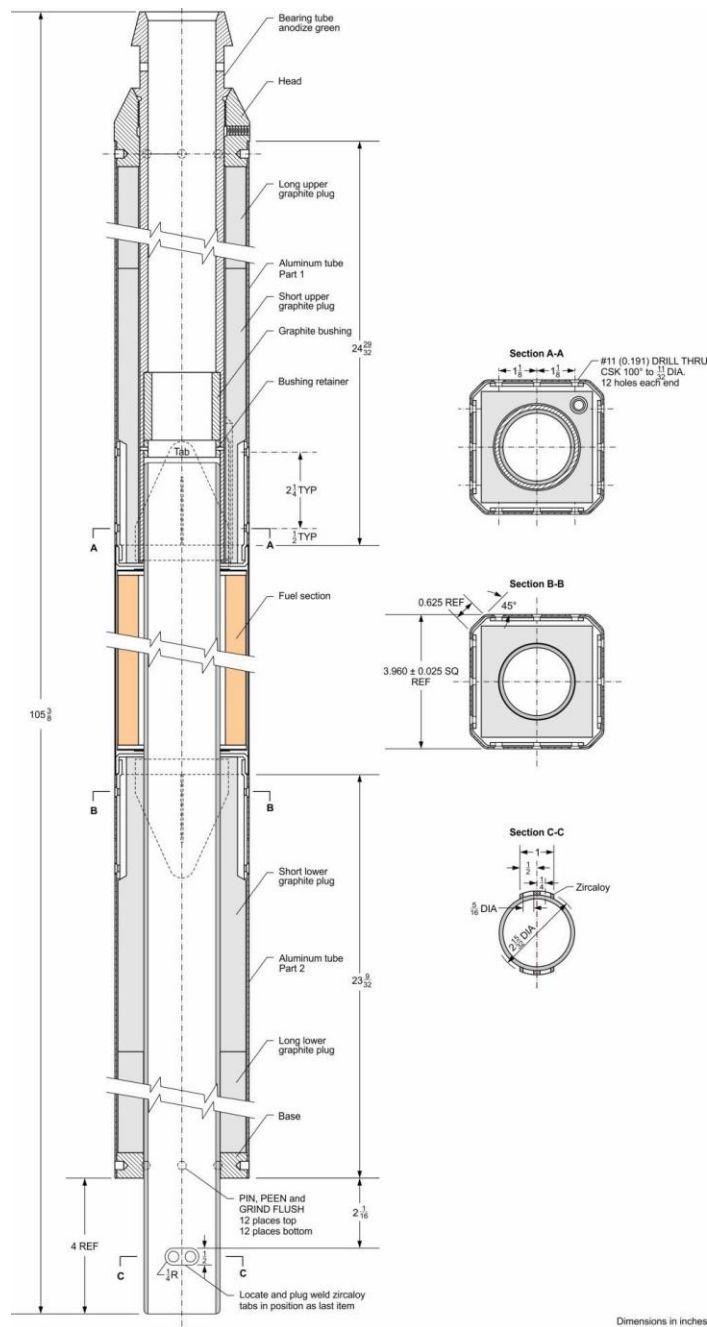


Figure 2 — Fuel Assembly

The fuel used by TREAT is UO_2 mixed in graphite. The graphite serves as both a moderator and a heat sink. TREAT has a very

strong negative temperature coefficient. The carbon-to-uranium-235 atom ratio of TREAT is 10,000: 1. The uranium is enriched with a weight percentage of 93.24 wt.%.

The fuel was produced by a baking process that resulted in partial graphitization. First, they took the uranium, in the form of U_3O_8 , graphite flour, thermax (a carbon product from Thermatomic), and Koppers coal tar and pressed it together. This mixture was then baked at $950^{\circ}C$, allowing it to partially graphitize. The heat converted most of the U_3O_8 to UO_2 , but the carbon could not fully graphitize at this temperature. Only 59% of the carbon was turned into graphite after baking [Bess & DeHart, 2015]. The reason $950^{\circ}C$ was chosen was to avoid the uranium converting to uranium carbide [Pavone, 1957].

Reactor Core

TREAT's core region is a 6 ft. 4 in. square by 4 ft tall. It has fuel composed of graphite-uranium blocks clad in zircaloy. Graphite-uranium fuel was chosen because of three advantages for a reactor that will receive large pulses of thermal neutrons. Those advantages are thermal shock resistance from the extreme heat input of transients, a large negative temperature coefficient of reactivity, and graphite's ability to serve as a heat sink for the heat generated during transients. Attached above and below the fuel are blocks of graphite reflector clad in aluminum, making the 8 ft. tall 4 in.² fuel assembly. There are also control rod fuel assemblies, which differ from the standard fuel assembly by having a hole down the center of the assembly so the control rods can be vertically moved. Some assemblies contain no fuel, and act as a thermal buffer for the fueled regions of the core. The thermocouple fuel assemblies are fitted with thermocouples to measure temperature in specific regions in the reactor. The positioning of the thermocouples was made with the hottest sections of the reactor in mind. Finally, at the very center of the core is the test hole, where the test sample is placed. The assemblies are arranged in a 19x19 square lattice, with 2 in.

air gaps [Bess & DeHart, ANL-6034, Transient Workshop Summary]. The core is surrounded in 2 ft. of permanent graphite reflector, and then with 5 ft. of concrete shielding.

Control Rods

TREAT's control rods are 16.78 ft. long [Bess & DeHart, 2015] and are made up with an upper grappling adapter, followed up with a boron carbide poison section cladded in steel, a graphite section cladded in zircaloy, and then two more graphite sections cladded in steel (see Fig. 3).

The rods are connected at the base of the control rod drives [Bess & DeHart, 2015]. TREAT has three types of control rods based on functionality, although they are identical in make and manufacturing. There are the control/shutdown rods, compensation rods, and transient rods, and

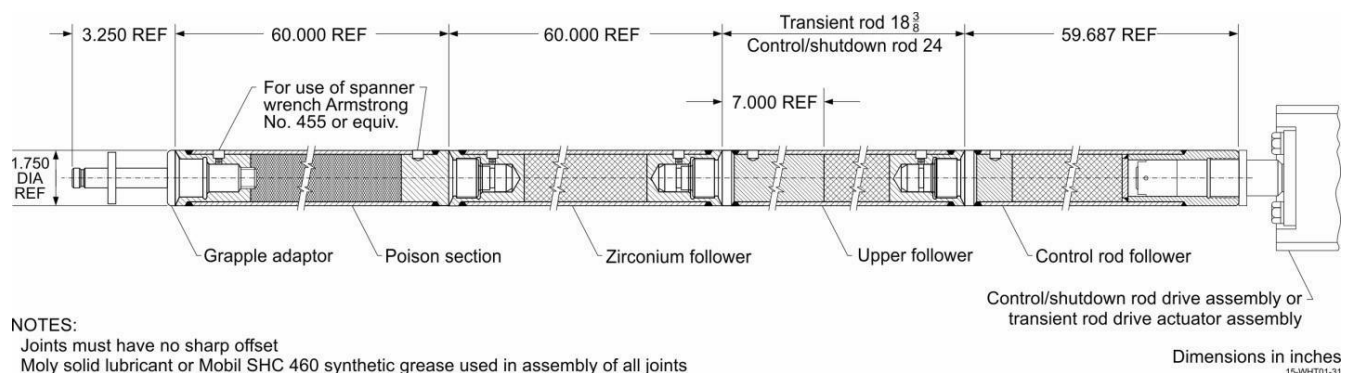


Figure 3 — Control Rod Configuration

they are distributed throughout the core in two rings. The inner ring is comprised of compensation rods, which are collectively worth \$11.60 in reactivity. The control/shutdown rods make up the upper and lower control rods in the outer ring. Their collective worth in reactivity is \$11. Finally, the transient rods make the left and right sides of the outer ring, with a collective reactivity worth of \$4 [CONF-820406—29].

Heat Removal

TREAT is air-cooled with a once-through induced-draft system. Up to 6,000 cfm (cubic feet per minute) of air is drawn through the reactor by two turbocompressors. The air passes through filters as it enters the reactor and is filtered again as it exits through a 60 ft. stack into the atmosphere. This amount allows for constant 100 kW steady state operations and will cool the reactor after a transient in several hours [Bess & DeHart, 2015].

Transient Operations

There are three modes of operations possible for TREAT. There are two transient modes and a steady-state mode. The steady state mode is limited to 100 kW but can provide the neutron flux required for neutron radiography. The first transient mode is a single burst of power by a sudden increase in reactivity. These result in a Gaussian shaped power curve and last under a second before negative temperature coefficient of reactivity terminates the reaction. Peak power can reach up to 18 GW, and core energy generation peaks at 2900 MJ, though these peak values are only reached for under 100 ms. The second transient mode is for ‘shaped transients,’ where shape refers to the fact that the shape is formed using control rod motion after the initial transient rod pull. The later rod movements are done by computer control rather than by manual control. These transients last for tens of seconds and can reach up to a peak power of 10 GW. A variety of shapes are possible, depending on what is needed for the experiment [INL/EXT-09-16392].

Introduction to Monte Carlo Methods

“Monte Carlo” was a name applied to a class of mathematical methods by Los Alamos scientists in 1940, during the development of nuclear weapons [Kalos & Whitlock, 2008]. The Monte Carlo method is a technique using a large amount of random numbers in a probabilistic model to approximate the solution to a numerical problem. The use of this method can range from economics to quantum mechanics.

We will be using the Monte Carlo method to simulate the steady-state neutron behavior as described by the neutron transport equation. In particular, we are interested in determining the critical eigenvalue, k using:

$$\begin{aligned} \hat{\Omega} \cdot \nabla \psi(\vec{r}, E, \hat{\Omega}) + \sigma(\vec{r}, E) \psi(\vec{r}, \hat{\Omega}, E) = \\ \int d\hat{\Omega} \int dE' \sigma_s(\vec{r}, E' \rightarrow E, \hat{\Omega}' \cdot \hat{\Omega}) \psi(\vec{r}, \hat{\Omega}', E') \\ + \frac{\chi(E)}{k} \int dE' \nu \sigma_f(\vec{r}, E') \int d\hat{\Omega} \psi(\vec{r}, \hat{\Omega}, E') \end{aligned}$$

Where:

$\hat{\Omega}$ is the unit vector solid angle.

$\psi(\vec{r}, E, \hat{\Omega})$ is the angular neutron flux

$\sigma(\vec{r}, E)$ is the total macroscopic cross section

E is the energy

ν is the average number of neutrons produced by fission

$\sigma_s(\vec{r}, E' \rightarrow E, \hat{\Omega}' \cdot \hat{\Omega})$ is the macroscopic cross section for scattering

$\sigma_f(\vec{r}, E')$ is the macroscopic cross section for fission

And k is the multiplication factor, which is included in the equation to ensure a balance.

k is also known as the eigenvalue.

It's important to understand that our intention is to have a critical system, where the value of k is close to 1, so that k disappears from the solution.

First, we will construct a distribution of fission neutrons and track them through their lifetimes to determine the number of fission neutrons created in the subsequent generation. The first generation is calculated with an initial guess and is then fed into a steady-state form of the transport equation or its appropriate multigroup approximation [Lewis & Miller, 1993]. The eigenvalue k will converge to a value as more random calculations are made. Here, k will be defined as the ratio of the number of neutrons in the j th generation, F_j , and the $j-1$ generation, F_{j-1} .

$$k = \frac{F_j}{F_{j-1}}$$

After a sufficient number of iterations, the number of neutrons per generation will converge to a value that will remain close to constant. This ratio is the eigenvalue, k . For transients, an initial state neutron source distribution must be used as a basis. Then we can change the system and see how this neutron distribution interacts with its altered environment.

Calculation methods of Serpent

Serpent 2 is a Monte Carlo reactor physics code developed at VTT in Finland. The software makes its particle interaction calculations via pseudo-random number generators. Let's say for example, you have a particle with a total microscopic cross section of $\sigma = 100$ b, and is distributed in the following manner:

$$\sigma_s = 50 \text{ b} \quad \sigma_f = 20 \text{ b} \quad \sigma_\gamma = 30 \text{ b}$$

Let's say our particle collides with a neutron. To determine what happens to the particle, we generate a random number R between 0 and 1. If the value is $0 \leq R \leq 0.50$, we designate it as a scatter. If the value is $0.51 \leq R \leq 0.70$, it absorbs the neutron and fissions. If the value is $0.71 \leq$

$R \leq 1$, the neutron is absorbed and a gamma is emitted. Once a neutron has been absorbed or has left the system, Serpent will “kill” it and cease tracking it.

Transients in Serpent

The primary reason we are using Serpent for modelling is its ability to simulate transients.

There are two stages in the simulation of transients. First, we run a source-generating steady state model that gives us a neutron source distribution file.

This file stores neutrons at random points of their lifetime in a uniform period of time and includes both prompt and delayed neutrons. We are only creating delayed neutron precursors in this

step. The precursors give us the delayed neutron population. The source distribution file is basically a snapshot of the simulation in a random point of time. In it, we can see the neutrons in their random position in x, y, and z in cartesian coordinates with a random energy. The second stage is the transient itself, where a time-dependent action occurs, say the movement of a control rod. The source distribution file is used to generate neutrons over the allotted period of time, and detectors (known as tallies in MCNP) can be used to gather information on fission energy

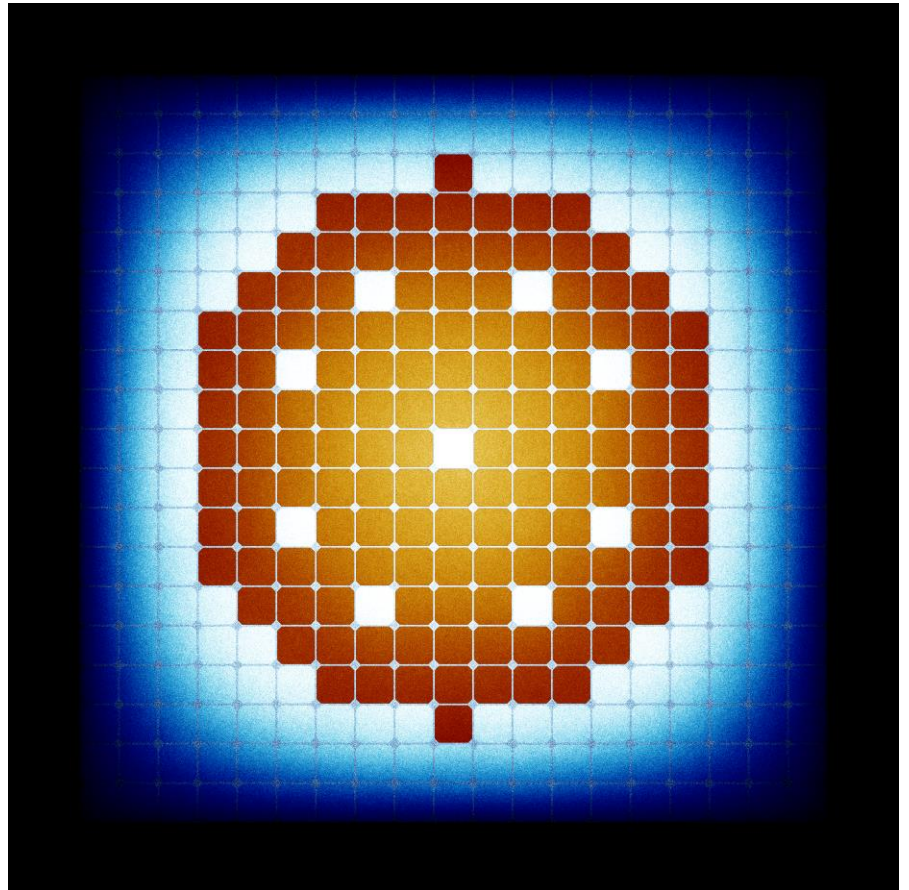


Figure 4 — *TREAT Fission Mesh*

deposition, neutron population, (n,f) interactions in particular geometries or materials, and much more. [V. Valtavirta et al., 2016].

Uncertainty and Shannon Entropy

One important factor with Monte Carlo methods in nuclear experiments is making sure we get accurate values for k-eff, reaction rates, and the source distribution. When using Monte Carlo to calculate values we start with an initial guess for the answer, and repeatedly make guesses until we converge to an average value. This method is a generational method. Each iteration, or “batch,” is calculated with the previous generation’s fission neutrons. However, we have to make sure that we have used a sufficient number of iterations that our initial guess is not influencing our final answer. Therefore, Serpent runs inactive cycles before running the active cycles. The inactive cycles are calculations made with their results discarded due to their proximity to the initial guess.

When using Monte Carlo techniques, we must make sure that our statistics are good enough that our data is not affected by our initial seed. One of these methods is verifying the Shannon entropy. Shannon entropy is the application of entropy on probability. A good explanation of this can be found from “Shannon Entropy, Information Gain, and Picking Balls from Buckets” by Luis Serrano from Medium on November 5, 2017. A link to the article has been included in the appendix.

Shannon entropy is another way of presenting the uncertainty in a stochastic assessment. Serpent allows for the calculation of the Shannon entropy of k-eff via the Set History card. Serpent will make an initial guess to the value of the Shannon entropy, and each history will reevaluate the entropy, and over time it will converge to a value.

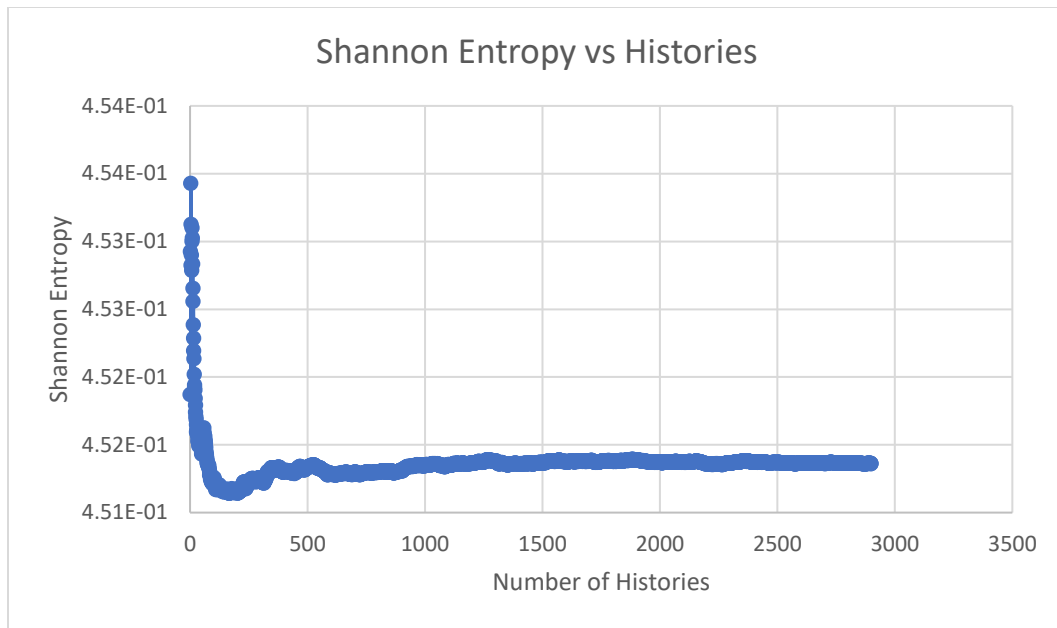


Figure 5 — Shannon Entropy vs Histories for M8CAL Steady State

Methods

Our objective is to use Serpent 2 to simulate a power excursion at TREAT. Starting from a steady state ($k\text{-eff} = 1.000$) condition, the transient control rods will be fully removed. Power will exponentially increase over the following seconds. The model will measure the change in power over time. Now, in an actual transient, power will exponentially increase until the negative temperature coefficient of the graphite drives reactivity down. This simulation would allow INL to have a Serpent model for TREAT that could be modified for any given experiment.

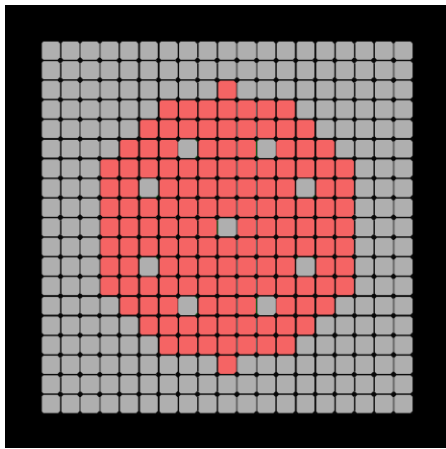


Figure 6 – Preliminary TREAT Simple Model

Simulations were done using the INL supercluster Falcon. Falcon has 972 nodes, each equipped with two 18-core processors with 128 GB RAM per node. Because of HPC time limitations, not all runs were allowed to reach completion.

Simple Model

The first step was to use a simple, steady state model of TREAT and create a time-dependent transient simulation from this. This model did not have control rods that entered fuel assemblies, but instead had graphite rods that appeared between the fuel assemblies, making up full squares in the 19x19 lattice. When in preliminary stages, the model was further simplified to a 3x3 lattice with 1 graphite rod and 8 fuel rods. B₄C, boron carbide, was added to the model, and placed in the vertical center of each graphite rod. This was to allow for an increase in reactivity upon rod removal. I learned to use the *trans* (transformation) card and show instantaneous control rod movements, with an appropriate change in reactivity. Next, I used the *transv* (transformation velocity) card to give the control rods a velocity and slowly move out of the reactor over 1

second. Geometric plots were used to give a visual verification of the control rod movement. Because of the simplicity of the design of this model, which is for steady state operations, it did not have the graphite follower included in its base design, so it needed to be added. I then added detectors, to track the energy deposition in the fuel over time.

The L91-60-1 Model

After successfully getting the simple model to show a power excursion, the next model to apply the transient was the L91-60-1 model of TREAT. This model is made up of multiple input files and one main file that would call to the other files. These separate files setup the geometry, the materials, the control rods, the fuel assemblies, the geometric plots, and the detectors. Because

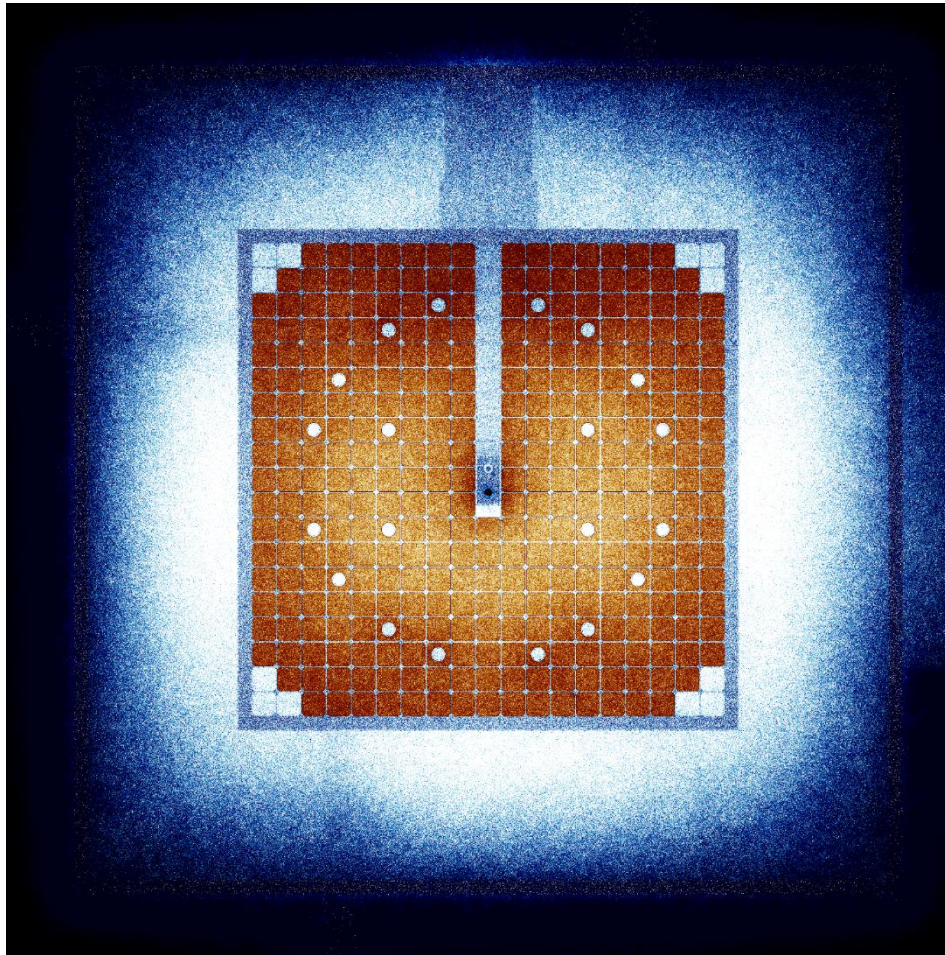


Figure 7 —L91-60-1 TREAT Model Mesh

this is a fully detailed model, control rods would drop into their respective fuel assemblies. While the transient, control/shutdown, and compensation rods are all identical, they are defined with different universes. Each rod type was raised by a differing

amount for the $k_{\text{eff}} = 1.000$ model. Control/shutdown rods are always raised fully out 58.5 in, compensation rods are placed at 28.72 in for the critical position, and transient rods raised 26.5 in. The steady state case is run with 5,000,000 neutrons for 4000 generations, with the first 50 used as inactive cycles. The transient case is run with 5,000,000 neutrons for 1000 cycles but will time out due to 48-hour time constraints. A full run would take 250 hours with our presets, which are 20 nodes with 24 cores.

The M8CAL Model

For our final model, we used the M8CAL TREAT core. This model is the same as L91-60-1, modified to have the transient prescription experiment inserted into the center hole. The objective is to see how the Serpent TREAT model experiment compares to the measured data from a real experiment. We initially chose to model Transient No. 2893T, a 2.6 % $\Delta k/k$ increase in reactivity, conducted on May 14, 2018, but later switched to Transient No. 2890T, a 1.5 % $\Delta k/k$ increase in reactivity, conducted on May 2, 2018. This was due to the desire to try a smaller change in reactivity. First, we set up the control rod positions for the steady state source generation file. The compensation rods were fully removed at 58.5", the control/shutdown rods are raised 27.1", and the transient rods were raised 27.9".

Next, we prepared for the transient. For the simulation, the movement of the rods was averaged, and a uniform movement was made for all 4 rods. The transient rods were moved 12.1" out to be fully raised at 40".

The problem we discovered is that our Serpent model was supercritical at the critical rod positions, with $k_{\text{eff}} = 1.0225 \pm 4.1 \times 10^{-5}$. If k is not sufficiently close to 1.00, the data results of the transient will be affected drastically. If the change in reactivity is small, the transient will have minimal changes. Large changes in reactivity will give an unrealistic power increase of up

to 50 orders of magnitude. We made a slight increase in the boron content in the fuel, while remaining within the uncertainty in the total boron content of TREAT fuel, to make $k_{\text{eff}} \sim 1$ at the critical positions. Another realization was the necessity of a sufficient number of neutrons being used per history. This was discovered by seeing a difference in results from models that only differed in the number of neutrons per batch (200,000 neutrons for 100 cycles vs 20,000 neutrons for 1000 cycles). After discussing with Dr. Ville Valtavirta from VTT, he suspected that for super prompt critical systems, Serpent is particularly sensitive to the number of neutrons per batch, due to the fact that a small number of fission chains experience the largest multiplication and most of the power increase comes from a relatively small number of initial prompt chains. For the full model run we wanted to use 50 million neutrons, but due to memory limitations we created 50 separate identical input files, each running 100,000 neutrons for one cycle. Serpent generates its random seed based off the computer time when the input file is read, so each run had a unique seed and varying results.

One way we can measure the accuracy of our Serpent simulations is by the reactor period. The reactor period is the time it takes the neutron density to change by a factor of e . To calculate the reactor period from Serpent, we can find the slope of the neutron density over time and take the reciprocal. Because we have a semilog format (time is linear, neutron density is exponential) we will solve for the slope with the following equation:

$$\text{Slope} = \frac{\ln(Y_f) - \ln(Y_0)}{X_f - X_0}$$

Where Y_0 is the initial value of the Y-axis, Y_f is the final value of the Y-axis, X_0 is the initial value of the X-axis, and X_f is the final value of the X-axis. Then we take the reciprocal:

$$\tau_e = \frac{1}{\text{Slope}}$$

It should be kept in mind that this method is only valid if the data is linear. So, we need to do a linear fit to the data and determine the slope of the fit line. From here, we can compare our result with the measured values.

Pitfalls and Troubleshooting

When making input files, many errors had to be avoided. One of the first issues discovered was with not having a high enough value for the “set nbuf” and “set pbuf” cards. These are the neutron buffer and precursor buffer cards and are multiplication factors that determine the amount of memory allotted for the upcoming generation of neutrons and precursors. These values had to be raised for the transient simulations with a high count of neutrons. Another issue was with the time intervals. One error that commonly came up was “Population exceeds maximum at 3.00E+00 seconds, adjust time cut-off.” From a discussion on the Serpent forum, this comes from the neutron population weight increasing 16 orders of magnitude from the initial weight. By changing the number of time bins, this error can be avoided. However, having too many time bins can also affect the output of the detectors, resulting in minimal changes in power and neutron populations. Another important factor that should be considered is which cross-section data library you are using in Serpent and how it relates to both past models. Due to the slight differences between libraries, particularly the major changes in carbon cross sections in recent evaluations, one might have different critical rod positions for their model.

Results

The sss2_treat model was used for learning how to use Serpent. Its simple design allowed for an easy opportunity to learn to make control rod movements and produce a transient.

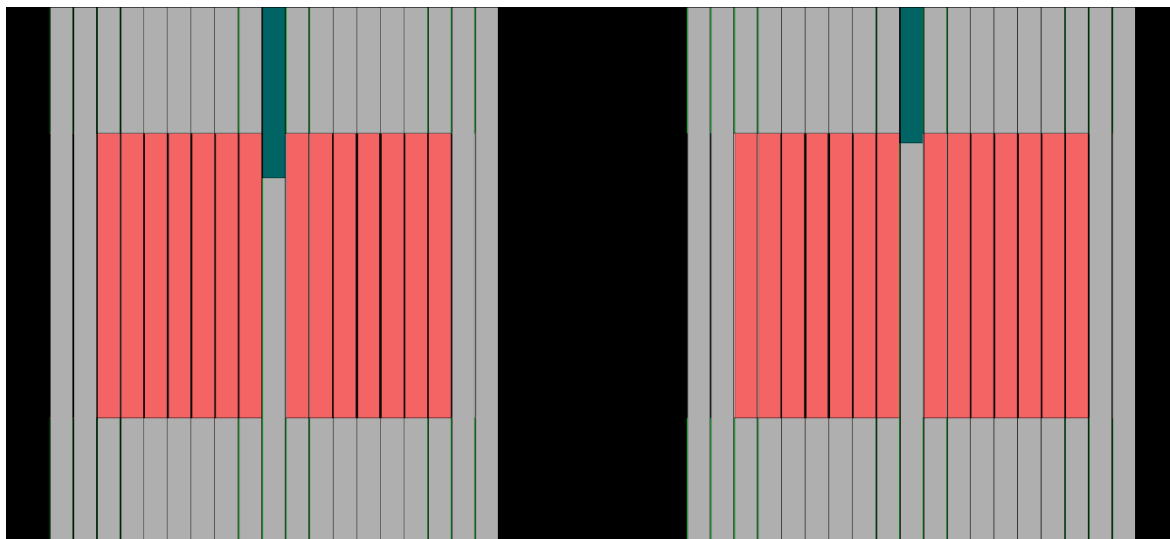


Figure 8 —TREAT Simple Model Control Rod Movement at $t=0$ (left) and $t=0.2$ (right)

Moving the boron portions of the control rods (blue-green) results in an increase in reactivity,

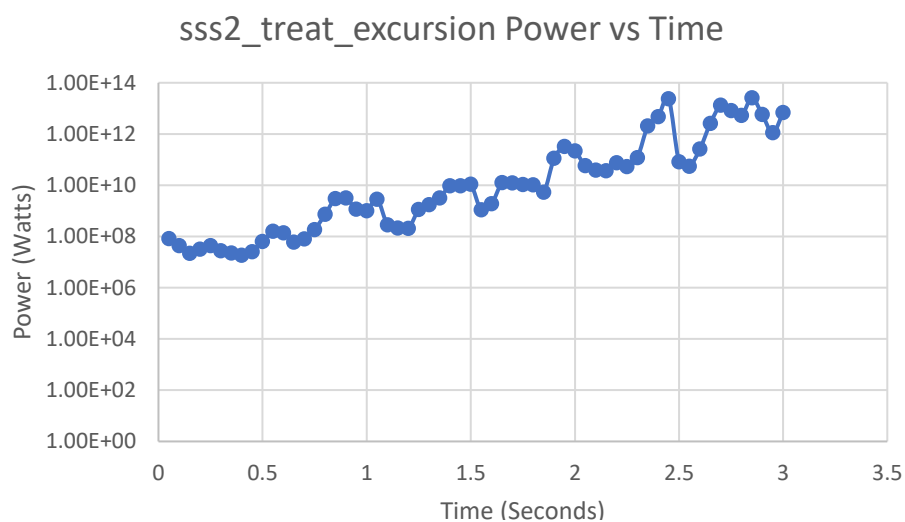


Figure 9 - sss2_treat Model Change in Power

giving us a small transient. The transients done using the sss2_treat_excursion were done with only 5000 neutrons for only 200 batches, so the data will be a bit rough, but show proof of concept.

Using the L91-60-1 model for a generic TREAT experiment showed some promise. It should be noted that for the L91-60-1 run, the power was normalized to 1 watt. During the transient, the total power was raised to $1.00954 \pm 0.92266 \times 10^{13}$ Watts. On the detector end, neutron populations raised from 1.4×10^7 neutrons/cm³ to 8.5×10^{20} neutrons/cm³. Near 1.5 seconds, we see an inflection point in the power generation and neutron population (Fig. 10 and Fig. 11). The likely cause of this is the random walk of Monte Carlo. As you make more and more random movements, it's possible to have a divergence from the original path, or trend. This change cascades through the rest of the run, unless the random walk by chance returns to the prior path.

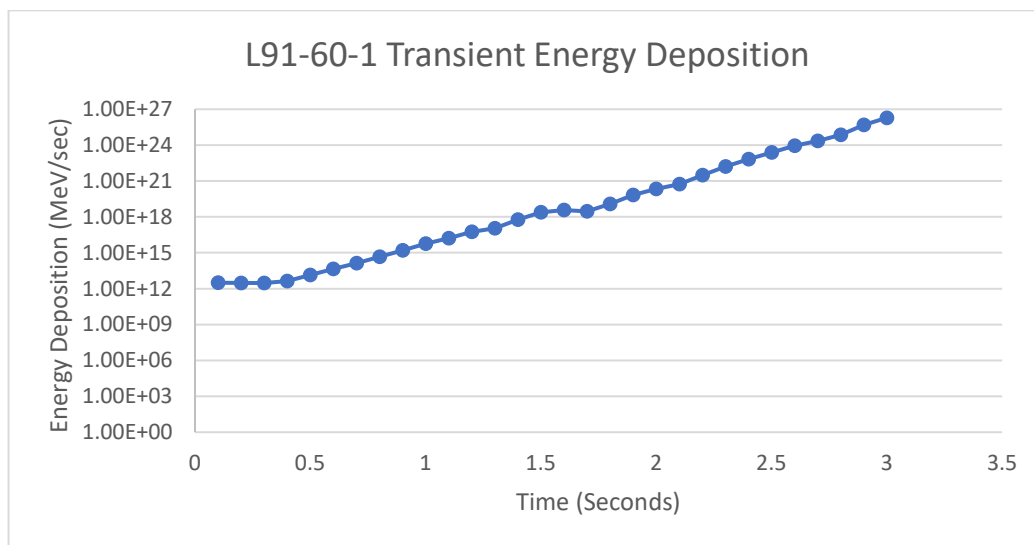


Figure 10 - L91-60-1 Energy Deposition

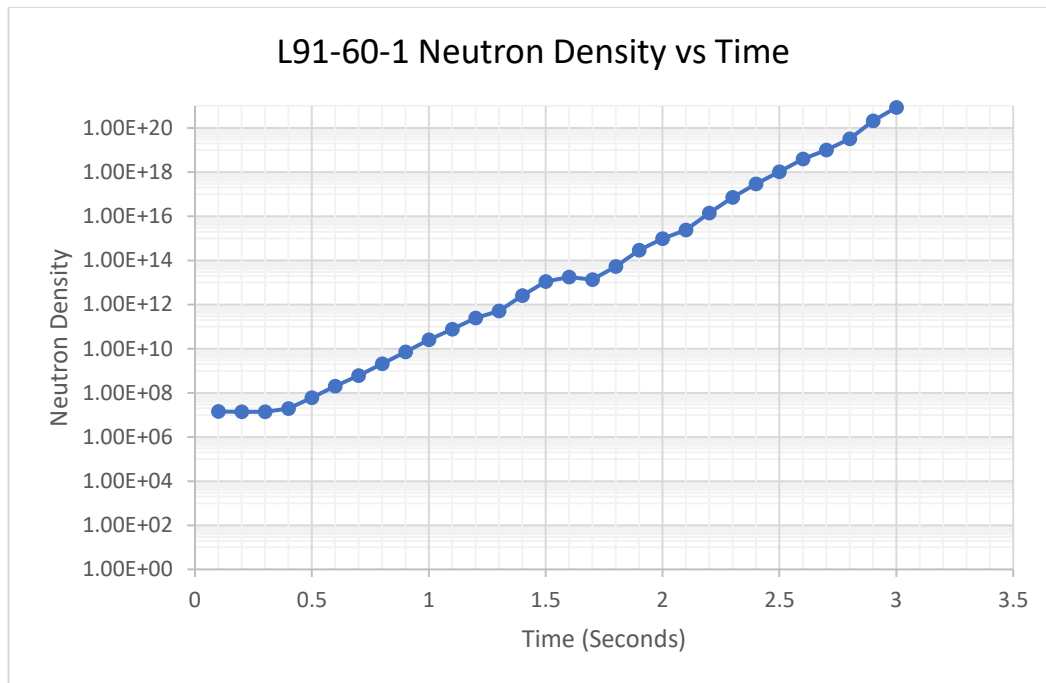


Figure 11- L91-60-1 Change in Neutron Population

The reactor period was calculated with both the neutron population and the energy deposition, equaling 10.5716 and 10.5739 respectively.

The transient prescription configuration using recent (2018) measurements is the final model used, and the goal was originally to simulate the 2893T 2.6% Clipped transient experiment, but later changed to the 2890T OTP-18-002 1.5% transient. This decision was made because it was considered worthwhile to model a smaller change in reactivity due to issues with memory and neutron populations. It was mentioned earlier that if k_{eff} is not close to 1.000, the transient will not perform correctly. For a large reactivity change ($12\% \Delta k/k$), Serpent will give results of up to 10×10^{75} watts, as seen in one faulty simulation from the 2.6% model.

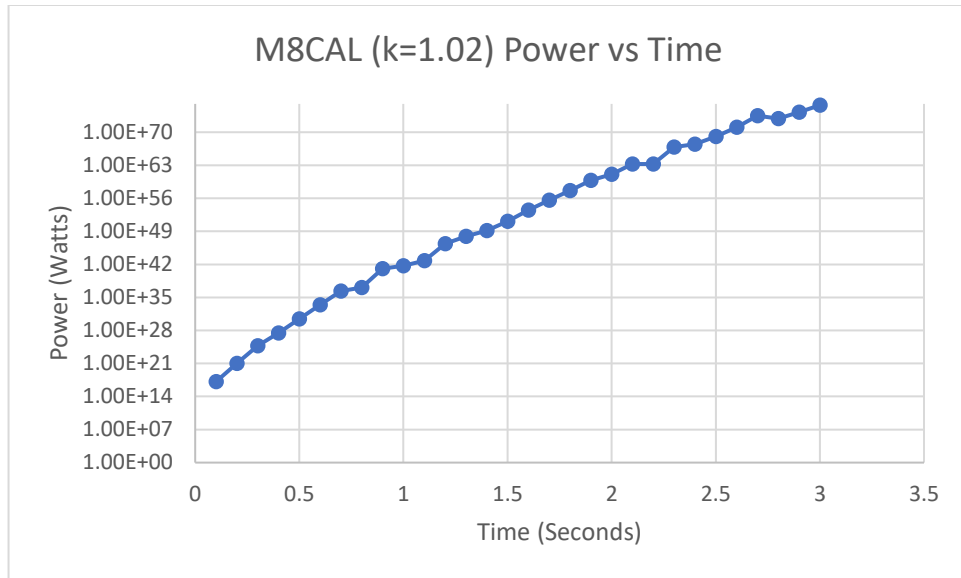


Figure 12 - M8CAL 2.6% Massive Change in Power

When we switched to the 1.5% run, we again focused on the changes in neutron population and reactor power, and then inspected the reactor period. The experimental measured reactor period for experiment 2890T was 0.112 sec^{-1} . The reactor period from our 50,000,000 particle run, which is the average of fifty separate 100,000 particle runs, was $0.130 \pm 0.0123 \text{ sec}^{-1}$. Our reactor period was within two standard deviations of the measured result. In the experiment, the reactor power went from 1kW to around 611MW, an increase of 5 orders of magnitude. In our model, reactor power went from 1kW to 86GW, an increase of 7 orders of magnitude. A larger increase in power is to be expected due to the current lack of thermal feedback in Serpent. Looking at Figures 13 and 14, we see a discontinuity after 1 second has passed. Again, the probable cause is random walk. Another side effect of the random walk is the increase in error in each time step.

1.5% $\Delta k/k$ Transient Change in Neutron Population with Error

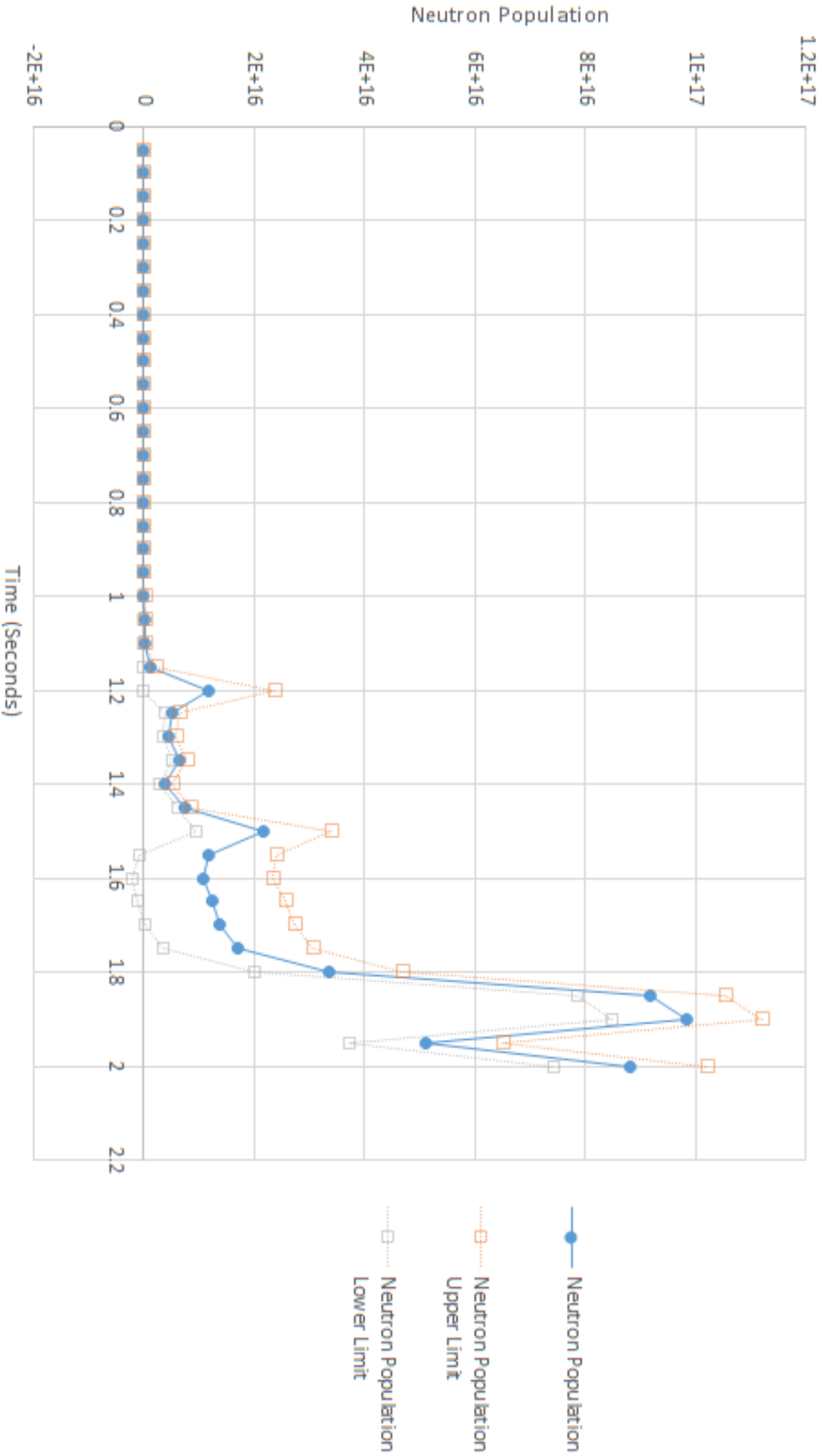


Figure 13 - 1.5% Change in Neutron Population

1.5% $\Delta k/k$ Transient Change in Reactor Power with Error

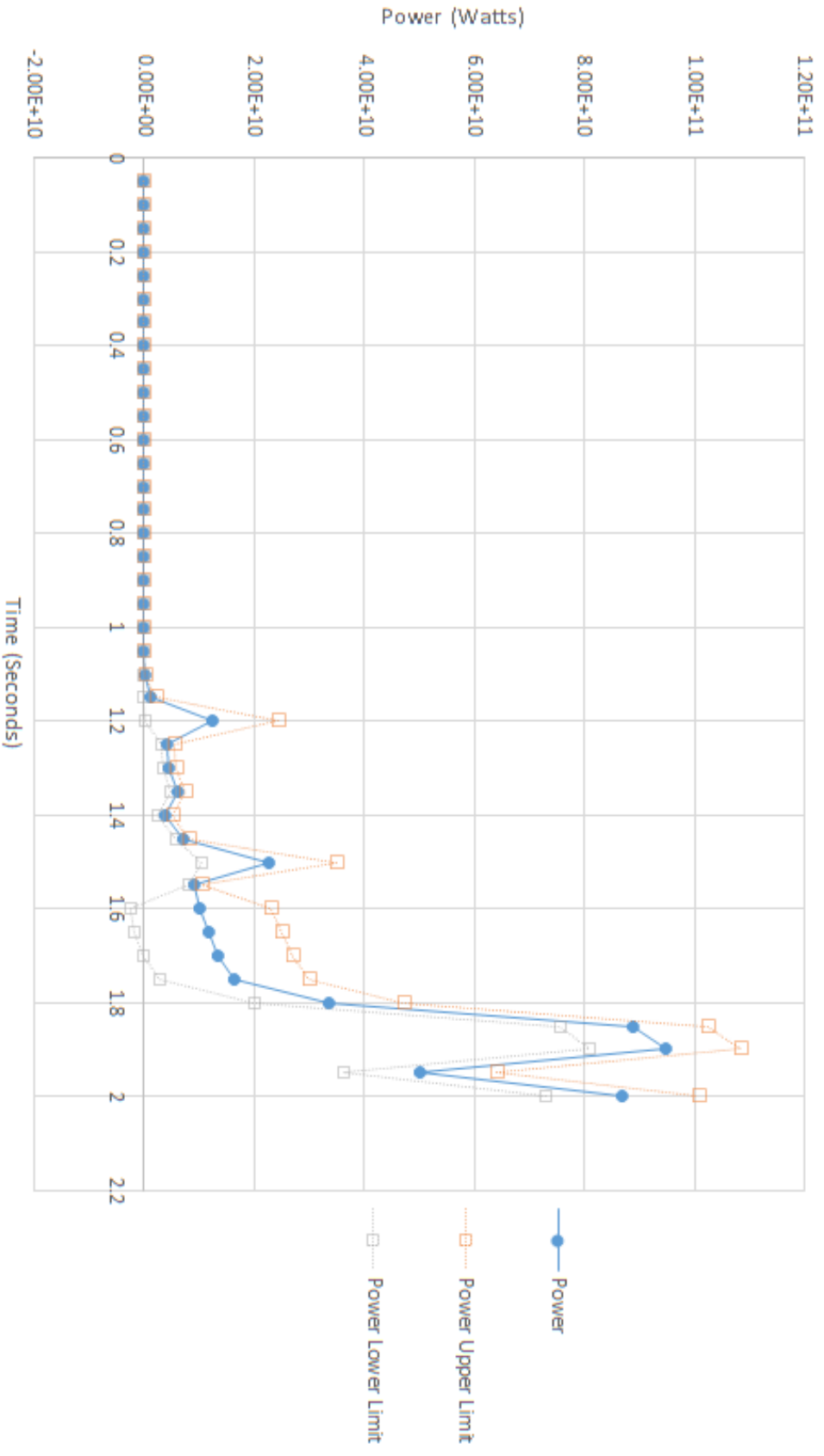


Figure 14 - 1.5% Change in Power

Future Work

Moving forward, there are more things that can be done for modeling transients with Serpent. The FINIX code, developed at VTT Finland, supports multi-physics simulations such as coupled reactor-physics/fuel-performance or thermal-hydraulics/fuel-performance simulations [Ikonen et al, 2015]. FINIX may be coupled with Serpent 2 at the source code level, which allows for direct memory access between Serpent and FINIX to simplifying solution transfers. A coupled Serpent/FINIX model would be able to provide the negative reactivity feedback that is not directly available within Serpent 2. Other less sophisticated coupling approaches are also possible with Serpent [Leppänen et al., 2012]. The negative temperature feedback from the graphite in TREAT will dramatically lead to a reduction in reactivity. Another consideration would be an alteration of the duration of the transient. Experimental transients can last from about a second to several minutes. Our models ran from 2 to 3 seconds, which may have been unnecessarily long for our circumstances. In the future, an effort should be made to simulate the different transient modes of TREAT. Lastly, attempting to model more transient TREAT experiments with varying amounts of changes in reactivity would be good to test the consistency of Serpent's transient modelling.

Appendix:

Input Files

File: sss2_treat_steady_state.i

```
set acelib "/home/wetzmark/endfb7u.xsdata"
```

```
% treat fuel element
```

```
surf 8 octa 0.0 0.0 4.8260 6.0313
```

```
surf 9 octa 0.0 0.0 4.9657 6.2288
```

```
surf 10 octa 0.0 0.0 5.0292 6.3186
```

```
surf 11 octa 0.0 0.0 4.9022 6.1390
```

```
surf 20 cuboid -5.08 5.08 -5.08 5.08 -121.76125 125.88875
```

```
surf 21 cuboid -5.08 5.08 -5.08 5.08 -250.0 125.88875
```

```
surf 40 pz 61.11875
```

```
surf 50 pz -61.11875
```

```
surf 60 cuboid -96.52 96.52 -96.52 96.52 -121.76125 125.88875
```

```
surf 70 pz 125.88875
```

```
surf 80 pz -121.76125
```

```
surf 81 pz -250.00
```

```
% universe 1 - fuel element
```

```
cell 1001 1 fuel -8 -40 50
```

```
cell 1002 1 air -9 8 -40 50
```

```
cell 1004 1 clad -10 9 -40 50
```

```
cell 1005 1 air -20 10
```

```
cell 1006 1 graphite -11 -70 40
```

```
cell 1007 1 graphite -11 -50 80
```

```
cell 1008 1 aluminum -10 11 -70 40
```

```
cell 1009 1 aluminum -10 11 -50 80
```

```
cell 1010 1 outside 20
```

```
% universe 2 - graphite element
```

```
cell 2001 2 graphite -8 -40 50
```

```
cell 2002 2 air -9 8 -40 50
```

```
cell 2004 2 clad -10 9 -40 50
```

```
cell 2005 2 air -20 10
```

```
cell 2006 2 graphite -11 -70 40
```

```
cell 2007 2 graphite -11 -50 80
```

```
cell 2008 2 aluminum -10 11 -70 40
```

```
cell 2009 2 aluminum -10 11 -50 80
```

```
cell 2010 2 outside 20
```

```
% universe 4 - movable boron carbide element
```

```
cell 4001 4 boron_carbide -8 -40 50
```

```
cell 4002 4 air -9 8 -40 50
```

```
cell 4004 4 clad -10 9 -40 50
```

```
cell 4005 4 air -21 10
```

```
cell 4006 4 graphite -11 -70 40
```

```
cell 4007 4 graphite -11 -50 81
```

```
cell 4008 4 aluminum -10 11 -70 40
```

```
cell 4009 4 aluminum -10 11 -50 81
```

```
cell 4010 4 outside 21
```

```
% universe 3 - core array
```

```
lat 3 1 0.0 0.0 19 19 10.16
```

```
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 2 2 2 2 2 2 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 2 2 2 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 2 2 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 2 1 1 1 4 1 1 1 4 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 1 1 4 1 1 1 1 1 1 1 1 4 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 1 1 1 1 1 1 4 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 1 1 4 1 1 1 1 1 1 1 1 4 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 2 1 1 1 4 1 1 1 4 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 2 2 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 2 2 2 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 2 2 2 2 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
```

```
% universe 0 - full model
```

```
cell 100 0 fill 3 -60 -70 80
```

```
cell 200 0 outside 60
```

```
cell 201 0 outside 70
```

```
cell 202 0 outside -80
```

```
% MATERIAL DEFINITIONS
```

```
therm graph gre7.00t
```

```
mat fuel sum rgb 245 100 100 moder graph 6012
```

```
92235.03c 8.65408E-06
```

```
92238.03c 6.31316E-07
```

```
6012.03c 8.62392E-02
```

5010.03c 1.14290E-07
 5011.03c 4.44130E-08
 26000.03c 1.85516E-05

mat clad sum rgb 222 222 222

50112.03c 7.53438E-07
 50114.03c 5.12648E-07
 50115.03c 2.64092E-07
 50116.03c 1.12938E-05
 50117.03c 5.96536E-06
 50118.03c 1.88126E-05
 50119.03c 6.67220E-06
 50120.03c 2.53062E-05
 50122.03c 3.59631E-06
 50124.03c 4.49732E-06
 40000.03c 4.20848E-02

mat graphite sum rgb 175 175 175 moder graph 6012

6012.03c 8.37491E-02
 5010.03c 4.44130E-08
 5011.03c 1.78768E-07
 26000.03c 1.80175E-05

mat boron_carbide sum rgb 0 100 100

6000.03c -0.217390
 5010.03c -0.15573939
 5011.03c -0.62687061

mat zirc2 sum rgb 100 100 245

26000.03c 9.55002E-05
 50112.03c 4.68066E-06
 50114.03c 3.18478E-06
 50115.03c 1.64064E-06
 50116.03c 7.01616E-05
 50117.03c 3.70592E-05
 50118.03c 1.16872E-04
 50119.03c 4.14504E-05
 50120.03c 1.57212E-04
 50122.03c 2.23417E-05
 50124.03c 2.79392E-05
 40000.03c 4.25479E-02
 24000.03c 7.59773E-05
 28000.03c 3.70193E-05
 72000.03c 2.21330E-06

```

mat air sum  rgb 10 10 10
              6000.03c 7.58114E-09
              7014.03c 3.94836E-05
              8016.03c 1.06081E-05

mat aluminum sum rgb 0 200 30
              13027.03c 6.03073E-02

set pop 5000 100 200
set power 500e6
set cpd 1 6 -121.76125 125.88875
set savesrc "./steady_state_source" 1e-1 0.25 1 1 1

% --- Transformations
trans U 4      0 0 122

set nbuf 1000

% --- Geometry and mesh plots:

plot 3 1000 1000  0 -115.0 115.0 -115.0 115.0
plot 3 1000 1000  70 -115.0 115.0 -115.0 115.0
plot 3 1000 1000 -70 -115.0 115.0 -115.0 115.0
plot 1 1000 1000  0 -115.0 115.0 -115.0 115.0
mesh 3 5000 5000  0 -115.0 115.0 -115.0 115.0 0 100
mesh 3 5000 5000  0 -115.0 115.0 -115.0 115.0 -5 5
mesh 3 5000 5000  0 -115.0 115.0 -115.0 115.0 50 60

set bc 1
set his 1

File: sss2_treat_excursion.i

set acelib "/home/wetzmark/endfb7u.xsdata"

% treat fuel element

surf 8 octa 0.0 0.0 4.8260 6.0313
surf 9 octa 0.0 0.0 4.9657 6.2288
surf 10 octa 0.0 0.0 5.0292 6.3186
surf 11 octa 0.0 0.0 4.9022 6.1390

surf 20 cuboid -5.08 5.08 -5.08 5.08 -121.76125 125.88875
surf 21 cuboid -5.08 5.08 -5.08 5.08 -250.0 125.88875

```

```

surf 40 pz 61.11875
surf 50 pz -61.11875
surf 60 cuboid -96.52 96.52 -96.52 96.52 -121.76125 125.88875
surf 70 pz 125.88875
surf 80 pz -121.76125
surf 81 pz -250.00

```

```

% universe 1 - fuel element
cell 1001 1 fuel -8 -40 50
cell 1002 1 air -9 8 -40 50
cell 1004 1 clad -10 9 -40 50
cell 1005 1 air -20 10
cell 1006 1 graphite -11 -70 40
cell 1007 1 graphite -11 -50 80
cell 1008 1 aluminum -10 11 -70 40
cell 1009 1 aluminum -10 11 -50 80
cell 1010 1 outside 20

```

```

% universe 2 - graphite element
cell 2001 2 graphite -8 -40 50
cell 2002 2 air -9 8 -40 50
cell 2004 2 clad -10 9 -40 50
cell 2005 2 air -20 10
cell 2006 2 graphite -11 -70 40
cell 2007 2 graphite -11 -50 80
cell 2008 2 aluminum -10 11 -70 40
cell 2009 2 aluminum -10 11 -50 80
cell 2010 2 outside 20

```

```

% universe 4 - movable boron carbide element
cell 4001 4 boron_carbide -8 -40 50
cell 4002 4 air -9 8 -40 50
cell 4004 4 clad -10 9 -40 50
cell 4005 4 air -21 10
cell 4006 4 graphite -11 -70 40
cell 4007 4 graphite -11 -50 81
cell 4008 4 aluminum -10 11 -70 40
cell 4009 4 aluminum -10 11 -50 81
cell 4010 4 outside 21

```

```

% universe 3 - core array
lat 3 1 0.0 0.0 19 19 10.16
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
2 2 2 2 2 2 2 2 1 2 2 2 2 2 2 2 2 2 2 2
2 2 2 2 2 2 1 1 1 1 1 1 1 2 2 2 2 2 2 2

```

```

2 2 2 2 2 1 1 1 1 1 1 1 1 1 2 2 2 2 2
2 2 2 2 1 1 1 4 1 1 1 4 1 1 1 2 2 2 2
2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2
2 2 2 1 1 4 1 1 1 1 1 1 1 4 1 1 2 2 2
2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2
2 2 2 1 1 1 1 1 1 4 1 1 1 1 1 1 2 2 2
2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2
2 2 2 1 1 4 1 1 1 1 1 1 1 4 1 1 2 2 2
2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2
2 2 2 2 1 1 1 4 1 1 1 4 1 1 1 2 2 2 2
2 2 2 2 2 1 1 1 1 1 1 1 1 1 2 2 2 2 2
2 2 2 2 2 2 1 1 1 1 1 1 1 2 2 2 2 2 2
2 2 2 2 2 2 2 2 2 1 2 2 2 2 2 2 2 2 2
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

```

```

% universe 0 - full model
cell 100 0 fill 3 -60 -70 80
cell 200 0 outside 60
cell 201 0 outside 70
cell 202 0 outside -80

```

```

% MATERIAL DEFINITIONS
therm graph gre7.00t

```

```

mat fuel sum   rgb 245 100 100 moder graph 6012
  92235.03c 10.89408E-06
  92238.03c 6.31316E-07
  6012.03c 8.62392E-02
  5010.03c 1.14290E-07
  5011.03c 4.44130E-08
  26000.03c 1.85516E-05

```

```

mat clad sum rgb 222 222 222
  50112.03c 7.53438E-07
  50114.03c 5.12648E-07
  50115.03c 2.64092E-07
  50116.03c 1.12938E-05
  50117.03c 5.96536E-06
  50118.03c 1.88126E-05
  50119.03c 6.67220E-06
  50120.03c 2.53062E-05
  50122.03c 3.59631E-06
  50124.03c 4.49732E-06
  40000.03c 4.20848E-02

```

```
mat graphite sum   rgb 175 175 175 moder graph 6012
    6012.03c 8.37491E-02
    5010.03c 4.44130E-08
    5011.03c 1.78768E-07
    26000.03c 1.80175E-05
```

```
mat boron_carbide sum   rgb 0 100 100
    6000.03c -0.217390
    5010.03c -0.15573939
    5011.03c -0.62687061
```

```
mat zirc2 sum   rgb 100 100 245
    26000.03c 9.55002E-05
    50112.03c 4.68066E-06
    50114.03c 3.18478E-06
    50115.03c 1.64064E-06
    50116.03c 7.01616E-05
    50117.03c 3.70592E-05
    50118.03c 1.16872E-04
    50119.03c 4.14504E-05
    50120.03c 1.57212E-04
    50122.03c 2.23417E-05
    50124.03c 2.79392E-05
    40000.03c 4.25479E-02
    24000.03c 7.59773E-05
    28000.03c 3.70193E-05
    72000.03c 2.21330E-06
```

```
mat air sum   rgb 10 10 10
    6000.03c 7.58114E-09
    7014.03c 3.94836E-05
    8016.03c 1.06081E-05
```

```
mat aluminum sum rgb 0 200 30
    13027.03c 6.03073E-02
```

```
% --- Link source (use point-wise precursor tracking)
```

```
set nps 5000 200 simutime
set dynsrc "/steady_state_source_excursion" 1
set savesrc "/excursion_source_end" 1
set cfe 10
set power 250e6
set cpd 1 6 -61.11875 61.11875
set pbuf 999
set nbuf 2000
```

```
% --- 30 time bins for detector
```

```
tme dettime 2 60 0 2
```

```
% --- 1 time interval for simulation (no population control)
```

```
tme simutime 2 60 0 2
```

```
% --- Detectors
```

```
det POW
```

```
du 3
```

```
dm fuel
```

```
di dettime
```

```
% --- Transformations
```

```
trans U 4 0 0 103.0
```

```
transv U 4 tlim 0.0 1 1 0 0 10.0
```

```
% --- Geometry and mesh plots:
```

```
%plot 1 1000 1000 0 -115.0 115.0 -115.0 115.0
```

```
mesh 3 5000 5000 0 -115.0 115.0 -115.0 115.0 0 100
```

```
mesh 3 5000 5000 0 -115.0 115.0 -115.0 115.0 -5 5
```

```
mesh 3 5000 5000 0 -115.0 115.0 -115.0 115.0 50 60
```

```
set bc 1
```

File: L91-60-1_steady.sss

```
%
```

```
% Ben Baker, modified by Mark Wetzel
```

```
% Idaho National Laboratory
```

```
% Jan 21 2016
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
% Surfaces
```

```
include "surfaces.sss"
```

```
include "Ex-Core-Definition.sss"
```

```
include "Ex-Core-Surfaces.sss"
```

```
include "Extra_Surfaces.sss" % Depends on the problem
```

```
% Materials
```

```

include "mat.sss"

% --- Cross section library file path:
set acelib "/hpc-common/data/serpent/xsdata/endfb71r1"

% Assemblies
include "A0.sss"
include "B0.sss"

include "CR-Type.sss"
include "C0_48inch.sss"
include "C1-C10.sss"
include "C9_Half-Slot.sss"
include "D0.sss"
include "D1-Half.sss"

include "A-s.sss"           % Depends on the problem
include "Rods0.018.sss"    % Depends on the problem
include "M8Center_wDy-22R-fuel-region.sss" % Depends on the problem

% Universe Definitions
% 11100 - A1: Sub-Universes 11101-11113
% 11200 - A2: Sub-Universes 11201-11213
% ...
% 14000 - A30: Sub-Universes 14001-14013
%
% 1100 - B1: Sub-Universes 1101 - 1113
% 1200 - B2: Sub-Universes 1201 - 1213
% ...
% 2000 - B10: Sub-Universes 2001 - 2013
%
% 5100 - C1: Sub-Universes 5101-5113
% 5150 - C2: Sub-Universes 5150-5173
% 5200 - C3: Sub-Universes 5201-5213
% ...
%
% 5900 - C-Half-Slotted Assembly:
%
% 6000 - D0: Sub-Universe 6001-6013 (ZRD - Zr clad dummy assemblies)
% 6100 - D1-Half: (Zr half clad dummy)
%
% 9000 - M8 Test Location

%

% Universe Definitions for Homogenization

```

% ##### WARNING ##### Cannot use A0 level for Homogenization. #####

% 11101 - 11113 A1

% 11x01 - 11x13 Pattern: Ax = A1-A10

% 12x01 - 12x13 A11-A20

% 13x01 - 13x13 A21-A30

%

% Largest = 13500 for A's

% Largest = 2000 for B's

%

% Dummy Zone for M8 calibration

cell 9900 9900 air_out -5999

% Rotate C & D half assemblies 180 Degrees

%trans 6100 0 0 0 0 0 180 % Flit D1-Half 180Deg (No Longer Needed)

% 6200 is the same as 6100, but faces 180 deg

trans 5900 0 0 0 0 0 180 % Flit C-Half 180Deg

%%%%%%%%%%
%%%%%%%%%

% Build 159 assembly core

%%%%%%%%%%
%%%%%%%%%

lat 101 1 0.0 0.0 19 19 10.16 % core array

6000	6000	12700	12700	12700	12700	12600	12600	12600	12600	12600	12600	12600	12600
		12700	12700	12700	12700	6000	6000						
6000	12700	12700	12700	12400	12400	11100	11100	11200	12100	11200	11100	11100	11100
		12400	12400	12700	12700	12700	6000						
12700	12700	12700	12400	11100	11100	11100	1300	11200	12100	11200	1300	11100	11100
		11100	11100	12400	12700	12700	12700						
12700	12700	12400	12400	11100	1400	11100	11100	11200	12100	11200	11100	11100	11100
		1400	11100	12400	12400	12700	12700						
12700	12400	11400	11400	11100	11100	11100	12100	12100	12100	12100	12100	12100	11100
		11100	11100	11400	11400	12400	12700						
12700	12400	11400	1900	11400	12200	12200	12100	12100	12100	12100	12100	12100	12200
		12200	11400	1900	11400	12400	12700						
12400	11400	11400	11400	11400	12000	12000	12100	11800	11800	11800	12100	12000	12000
		12000	11400	11400	11400	11400	12400						
12400	11400	2000	11400	12000	1600	12000	12100	11800	11800	11800	12100	12000	12000
		1600	12000	11400	2000	11400	12400						
12400	11400	11400	11400	12000	12000	12000	12100	11700	6100	11700	12100	12000	12000
		12000	12000	11400	11400	11400	12400						
12400	12300	12300	12300	12200	12200	12200	12100	11700	9900	11700	12100	12200	12200
		12200	12200	12300	12300	12300	12400						

```

12400 11300 11300 11300 11900 11900 11900 12100 11700 5900 11700 12100 11900
      11900 11900 11300 11300 11300 12400
12400 11300 1800 11300 11900 1500 11900 12100 11600 5100 11600 12100 11900
      1500 11900 11300 1800 11300 12400
12400 11300 11300 11300 11300 11900 11900 12100 11600 5150 11600 12100 11900
      11900 11300 11300 11300 11300 12400
12500 12400 11300 1700 11300 12200 12200 12100 11600 5200 11600 12100 12200
      12200 11300 1700 11300 12400 12500
12500 12400 11300 11300 11200 11200 11200 12100 11600 5250 11600 12100 11200
      11200 11200 11300 11300 12400 12500
12500 12500 12400 12400 11200 1200 11200 11200 11500 5300 11500 11200 11200
      1200 11200 12400 12400 12500 12500
12500 12500 12500 12400 11200 11200 11200 1100 11500 5350 11500 1100 11200
      11200 11200 12400 12500 12500 12500
6000 12500 12500 12500 12400 12400 11200 11200 11500 5400 11500 11200 11200
      12400 12400 12500 12500 12500 6000
6000 6000 12500 12500 12500 12500 12500 12500 12500 5450 12500 12500 12500
      12500 12500 12500 6000 6000

```

```

cell 8500 100 fill 9000 -9081 % Add Test Region
cell 8501 100 fill 101 9081

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
% RUN/PLOT OPTIONS
```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
% --- boundary conditions (1-black, 2-reflective , 3-periodic):
set bc 1 1 1

```

```

% estimators use (0/1 0 - collision 1- track-length)
% if 1 dt is switched off
%set tle 0

```

```

% --- Neutron population and criticality cycles:
%set pop 2000000 20000 100
set pop 2500000 4000 50
set cfe 10

```

```
set nbuf 7
```

```

% --- Fission Source Entropy
%set his 1
%set entr 5 5 5 -25.4 25.4 -25.4 25.4 0 255

```

```
% normalization to power (1 W)
```

```

set power 1.0
set U235H 182.0 %U235 Heating value Default: 202.27MeV
%set fissh <ZAI1><H1><ZAI2><H2>...

%% --- Geometry and mesh plots:
include "plots.sss" % Depends on the problem

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%      XS preparation settings
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
set micro egl
ene egl 1 1.00000E-11 2.00100E-08 4.73020E-08 7.64970E-08 2.09610E-07 6.25000E-07
8.100030E-06
1.32700E-04 3.48110E-03 1.15620E-01 2.00000E+01

% include "gcu.sss" % Depends on the problem
set gcu -1
set savesrc "/TREAT_source" 0.10 1.0 1 1 1
set impl 0 0 0

%%% Extra on GCU
%%% Detector
%%%350
%%%
%%% Air Channel w/ Det
%%%300
%%%
%%%301
%%%302
%%%303
%%%304
%%%305
%%%306
%%%307
%%%308
%%%309
%%%310
%%%311
%%%312
%%%313

set blockdt b4c_new Dy

```

```
set nfg 10 2.00100E-08 4.73020E-08 7.64970E-08 2.09610E-07 6.25000E-07 8.100030E-06
1.32700E-04 3.48110E-03 1.15620E-01
```

```
%include "Detectors.sss" % Depends on the problem
```

```
%%
```

```
%%
```

File: L91-60-1_trans.sss

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
% Transient calculation
```

```
% Mark DeHart, based on original model by Ben Baker, modified by Mark Wetzel
```

```
% Idaho National Laboratory
```

```
% Nov 17 2017
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
% transient settings
```

```
tme simutime 2 10 0 3 % --- 20 time intervals for simulation
```

```
tme dettime 2 30 0 3 % --- 50 time bins for detector
```

```
set nps 5000000 1000 simutime % --- Neutron population:
```

```
set outp 10 % --- Output after each 10 cycles
```

```
set dynsrc "/TREAT_source" 1 % --- Link source (use point-wise precursor tracking)
```

```
det 1 dr -15 void di dettime % --- Neutron population as a function of time
```

```
det 2 dr -8 void di dettime % --- Fission energy deposition as a function of time
```

```
set gcu -1
```

```
set impl 0 0 0
```

```
set nbuf 3000
```

```
set pbuf 500
```

```
%# velocity transformation on universe 802 (transient rods), between 0.0 and 0.02 seconds.
```

```
%# Motion stops (v returns to 0) at 0.02 sec.
```

```
transv U 802 tlim 0.0 0.0794 1 0.0 0.0 431.8 % transient rods travel from 67.31 cm to 101.6 cm,
fully removed.
```

```
% Surfaces
```

```
include "surfaces.sss"
```

```
include "Ex-Core-Definition.sss"
```

```
include "Ex-Core-Surfaces.sss"
```

```
include "Extra_Surfaces.sss" % Depends on the problem
```

```
% Materials
```

```

include "mat.sss"

% --- Cross section library file path:
set acelib "/hpc-common/data/serpent/xsdata/endfb71r1"

% Assemblies
include "A0.sss"
include "B0.sss"

include "CR-Type.sss"
include "C0_48inch.sss"
include "C1-C10.sss"
include "C9_Half-Slot.sss"
include "D0.sss"
include "D1-Half.sss"

include "A-s.sss"           % Depends on the problem
include "Rods0.018.sss"    % Depends on the problem
include "M8Center_wDy-22R-fuel-region.sss" % Depends on the problem

% Universe Definitions
% 11100 - A1: Sub-Universes 11101-11113
% 11200 - A2: Sub-Universes 11201-11213
% ...
% 14000 - A30: Sub-Universes 14001-14013
%
% 1100 - B1: Sub-Universes 1101 - 1113
% 1200 - B2: Sub-Universes 1201 - 1213
% ...
% 2000 - B10: Sub-Universes 2001 - 2013
%
% 5100 - C1: Sub-Universes 5101-5113
% 5150 - C2: Sub-Universes 5150-5173
% 5200 - C3: Sub-Universes 5201-5213
% ...
%
% 5900 - C-Half-Slotted Assembly:
%
% 6000 - D0: Sub-Universe 6001-6013 (ZRD - Zr clad dummy assemblies)
% 6100 - D1-Half: (Zr half clad dummy)
%
% 9000 - M8 Test Location

%

% Universe Definitions for Homogenization

```

% ##### WARNING ##### Cannot use A0 level for Homogenization. #####

% 11101 - 11113 A1

% 11x01 - 11x13 Pattern: Ax = A1-A10

% 12x01 - 12x13 A11-A20

% 13x01 - 13x13 A21-A30

%

% Largest = 13500 for A's

% Largest = 2000 for B's

%

% Dummy Zone for M8 calibration

cell 9900 9900 air_out -5999

% Rotate C & D half assemblies 180 Degrees

%trans 6100 0 0 0 0 0 180 % Flit D1-Half 180Deg (No Longer Needed)

% 6200 is the same as 6100, but faces 180 deg

trans 5900 0 0 0 0 0 180 % Flit C-Half 180Deg

%%%%%%%%%%
%%%%%%%%%

% Build 159 assembly core

%%%%%%%%%%
%%%%%%%%%

lat 101 1 0.0 0.0 19 19 10.16 % core array

6000	6000	12700	12700	12700	12700	12600	12600	12600	12600	12600	12600	12600	12600
		12700	12700	12700	12700	6000	6000						
6000	12700	12700	12700	12400	12400	11100	11100	11200	12100	11200	11100	11100	11100
		12400	12400	12700	12700	12700	6000						
12700	12700	12700	12400	11100	11100	11100	1300	11200	12100	11200	1300	11100	11100
		11100	11100	12400	12700	12700	12700						
12700	12700	12400	12400	11100	1400	11100	11100	11200	12100	11200	11100	11100	11100
		1400	11100	12400	12400	12700	12700						
12700	12400	11400	11400	11100	11100	11100	12100	12100	12100	12100	12100	12100	11100
		11100	11100	11400	11400	12400	12700						
12700	12400	11400	1900	11400	12200	12200	12100	12100	12100	12100	12100	12100	12200
		12200	11400	1900	11400	12400	12700						
12400	11400	11400	11400	11400	12000	12000	12100	11800	11800	11800	12100	12000	12000
		12000	11400	11400	11400	11400	12400						
12400	11400	2000	11400	12000	1600	12000	12100	11800	11800	11800	12100	12000	12000
		1600	12000	11400	2000	11400	12400						
12400	11400	11400	11400	12000	12000	12000	12100	11700	6100	11700	12100	12000	12000
		12000	12000	11400	11400	11400	12400						
12400	12300	12300	12300	12200	12200	12200	12100	11700	9900	11700	12100	12200	12200
		12200	12200	12300	12300	12300	12400						

```

12400 11300 11300 11300 11900 11900 11900 12100 11700 5900 11700 12100 11900
      11900 11900 11300 11300 11300 12400
12400 11300 1800 11300 11900 1500 11900 12100 11600 5100 11600 12100 11900
      1500 11900 11300 1800 11300 12400
12400 11300 11300 11300 11300 11900 11900 12100 11600 5150 11600 12100 11900
      11900 11300 11300 11300 11300 12400
12500 12400 11300 1700 11300 12200 12200 12100 11600 5200 11600 12100 12200
      12200 11300 1700 11300 12400 12500
12500 12400 11300 11300 11200 11200 11200 12100 11600 5250 11600 12100 11200
      11200 11200 11300 11300 12400 12500
12500 12500 12400 12400 11200 1200 11200 11200 11500 5300 11500 11200 11200
      1200 11200 12400 12400 12500 12500
12500 12500 12500 12400 11200 11200 11200 1100 11500 5350 11500 1100 11200
      11200 11200 12400 12500 12500 12500
6000 12500 12500 12500 12400 12400 11200 11200 11500 5400 11500 11200 11200
      12400 12400 12500 12500 12500 6000
6000 6000 12500 12500 12500 12500 12500 12500 12500 5450 12500 12500 12500
      12500 12500 12500 6000 6000

```

```

cell 8500 100 fill 9000 -9081 % Add Test Region
cell 8501 100 fill 101 9081

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
% RUN/PLOT OPTIONS
```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
% --- boundary conditions (1-black, 2-reflective , 3-periodic):
```

```
set bc 1 1 1
```

```
% estimators use (0/1 0 - collision 1- track-length)
```

```
% if 1 dt is switched off
```

```
%set tle 0
```

```
% --- Fission Source Entropy
```

```
%set his 1
```

```
%set entr 5 5 5 -25.4 25.4 -25.4 25.4 0 255
```

```
% normalization to power (1 W)
```

```
set power 1.0
```

```
set U235H 182.0 %U235 Heating value Default: 202.27MeV
```

```
%set fissh <ZAI1><H1><ZAI2><H2>...
```

```
%% --- Geometry and mesh plots:
```

```
include "plots.sss" % Depends on the problem
```

```

mesh 3 5000 5000 0 -388.059 388.059 -388.059 388.059 -194 194
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%      XS preparation settings
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%set micro eg1
%ene eg1 1 1.00000E-11 2.00100E-08 4.73020E-08 7.64970E-08 2.09610E-07 6.25000E-07
8.100030E-06
%      1.32700E-04 3.48110E-03 1.15620E-01 2.00000E+01
%
%
% include "gcu.sss"    % Depends on the problem
%%% Extra on GCU
%%% Detector
det POW du 101 dm fuel di dettime
det NPOP dr -15 fuel di dettime
det POW_test dr -8 fuel di dettime

%%%350
%%%
%%% Air Channel w/ Det
%%%300
%%%
%%%301
%%%302
%%%303
%%%304
%%%305
%%%306
%%%307
%%%308
%%%309
%%%310
%%%311
%%%312
%%%313

%set blockdt b4c_new Dy
%set nfg 10 2.00100E-08 4.73020E-08 7.64970E-08 2.09610E-07 6.25000E-07 8.100030E-06
1.32700E-04 3.48110E-03 1.15620E-01

include "Detectors.sss"    % Depends on the problem
set his 1
%%
%%

```

File: M8CAL.sss

```

% Transient Prescription
% Javier Ortensi, modified by Mark Wetzel
% Idaho National Laboratory
% March 20 2018
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

% --- Cross section library file path:
set acelib "/hpc-common/data/serpent/xsdata/endfb71r1"

% Surfaces
include "../M8_new/surfaces.sss"
include "../M8_new/Ex-Core-Surfaces.sss"

% Materials
%include "../M8_new/mat.sss"
%include "../dehart/M8_mark/mat.sss"
include "mat.sss"

% Assemblies
include "../M8_new/Assemblies_Core_Cells/A/A0.sss"
include "../M8_new/Assemblies_Core_Cells/B/B0.sss"
include "../M8_new/Assemblies_Core_Cells/C/C0_48inch.sss"
include "../M8_new/Assemblies_Core_Cells/C/C1-C10.sss"
include "../M8_new/Assemblies_Core_Cells/C/C9_Half-Slot.sss"
include "../M8_new/Assemblies_Core_Cells/D/D0.sss"
include "../M8_new/Assemblies_Core_Cells/D/D1-Half.sss"
%% include "../M8_new/M8Center_wDy-22R-fuel-region.sss"
include "../M8_new/M8Center-Transient-Prescription.sss"

include "../M8_new/Ex-Core-Definition.sss"
include "../M8_new/CR-Type_cyl.sss"
include "../M8_new/Extra_Surfaces.sss"
include "../M8_new/A-s.sss"
include "../M8_new/Rods.sss"
%include "../M8_new/plots.sss"
include "../M8_new/Detectors.sss"

% Description of Placement: C/S-1 & 4 (North) at 22" = 55.88cm
% Description of Placement: Comp-1 & 4 (North) at 58.5" = 148.59cm

```

% Description of Placement: Trans-1 & 4 (North) at 40.0" = 101.6cm
 trans 801 0 0 148.59 % compensation rods full out 58.5"
 trans 802 0 0 68.88 % safety rods 27.1"
 trans 803 0 0 70.87 % transient rods 27.9"

%Transient Data Summary Sheet for Transient 2893T on 2018.5.14
 %trans 801 0 0 148.59 % compensation rods full out 58.5 in
 %trans 802 0 0 79.934 % safety rods average raised 31.47 in
 %trans 803 0 0 59.0296 % transient rods raised 23.24 in

% Dummy Zone for M8 calibration
 cell 9900 9900 air_out -5999

% Rotate C & D half assemblies 180 Degrees
 %trans 6100 0 0 0 0 0 180 % Flit D1-Half 180Deg
 trans 5900 0 0 0 0 0 180 % Flit C-Half 180Deg
 trans 9000 0 0 0 0 0 180 % Flit M8 vehicle

%%%%%%%%%%
 %%%%%%%%%%

% Build 159 assembly core

%%%%%%%%%%
 %%%%%%%%%%

lat 101 1 0.0 0.0 19 19 10.16 % core array

6000 6000 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100
 11100 11100 11100 6000 6000
 6000 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100
 11100 11100 11100 11100 6000
 11100 11100 11100 11100 11100 11100 11100 1200 11100 11100 11100 1200 11100 11100
 11100 11100 11100 11100 11100
 11100 11100 11100 11100 11100 1200 11100 11100 11100 11100 11100 11100 11100 1200
 11100 11100 11100 11100 11100
 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100
 11100 11100 11100 11100 11100
 11100 11100 11100 1300 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100
 11100 1300 11100 11100 11100
 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100
 11100 11100 11100 11100 11100
 11100 11100 1300 11100 11100 1100 11100 11100 11100 11100 11100 11100 11100 1100 11100
 11100 1300 11100 11100
 11100 11100 11100 11100 11100 11100 11100 11100 11100 6100 11100 11100 11100 11100
 11100 11100 11100 11100 11100
 11100 11100 11100 11100 11100 11100 11100 11100 9900 11100 11100 11100 11100
 11100 11100 11100 11100 11100
 11100 11100 11100 11100 11100 11100 11100 11100 5900 11100 11100 11100 11100
 11100 11100 11100 11100 11100

```

11100 11100 1300 11100 11100 1100 11100 11100 11100 5100 11100 11100 11100 1100 11100
11100 1300 11100 11100
11100 11100 11100 11100 11100 11100 11100 11100 11100 5100 11100 11100 11100 11100
11100 11100 11100 11100 11100
11100 11100 11100 1300 11100 11100 11100 11100 11100 5100 11100 11100 11100 11100
11100 1300 11100 11100 11100
11100 11100 11100 11100 11100 11100 11100 11100 11100 5100 11100 11100 11100 11100
11100 11100 11100 11100 11100
11100 11100 11100 11100 11100 1200 11100 11100 11100 5100 11100 11100 11100 1200 11100
11100 11100 11100 11100
11100 11100 11100 11100 11100 11100 11100 1200 11100 5100 11100 1200 11100 11100 11100
11100 11100 11100 11100
6000 11100 11100 11100 11100 11100 11100 11100 11100 5100 11100 11100 11100 11100
11100 11100 11100 11100 6000
6000 6000 11100 11100 11100 11100 11100 11100 11100 5100 11100 11100 11100 11100 11100
11100 11100 6000 6000

```

```

cell 8500 100 fill 9000 -9081 % Add Test Region
cell 8501 100 fill 101 9081

```

```

cell 5590 0 fill 1 -570 571 -572
cell 5591 0 outside 570
cell 5592 0 outside -571 -570
cell 5593 0 outside 572 -570

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%   RUN/PLOT OPTIONS
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% --- boundary conditions (1-black, 2-reflective , 3-periodic):
set bc 1 1 1

```

```

% --- Neutron population and criticality cycles:
%set pop 2800000 4000 100
set pop 2000000 1000 10
%set pop 10000 100 10
set nbuf 30
set outp 10
% normalization to power (1000 W)
set power 1000.0

```

```

set U235H 182.0 %U235 Heating value Default: 202.27MeV
%set fissh <ZAI1><H1><ZAI2><H2>...

```

```

%%% Cross section regions

```

```

%% add high energy groups at 1E5 and 1E6 eV
set savesrc "./M8_1.5_source" 0.04 1.0 1 1 1
set his 1

```

File: M8CAL_100k_*.sss (* varying from values 1 to 50)

```

% Transient Prescription
% Javier Ortensi, modified by Mark Wetzel
% Idaho National Laboratory
% July 6 2018
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```

% --- Cross section library file path:
set acelib "/hpc-common/data/serpent/xsdata/endfb71r1"

```

```

% Surfaces
include "../M8_new/surfaces.sss"
include "../M8_new/Ex-Core-Surfaces.sss"

```

```

% Materials
include "mat.sss"

```

```

% Assemblies
include "../M8_new/Assemblies_Core_Cells/A/A0.sss"
include "../M8_new/Assemblies_Core_Cells/B/B0.sss"
include "../M8_new/Assemblies_Core_Cells/C/C0_48inch.sss"
include "../M8_new/Assemblies_Core_Cells/C/C1-C10.sss"
include "../M8_new/Assemblies_Core_Cells/C/C9_Half-Slot.sss"
include "../M8_new/Assemblies_Core_Cells/D/D0.sss"
include "../M8_new/Assemblies_Core_Cells/D/D1-Half.sss"
%% include "M8Center_wDy-22R-fuel-region.sss"
include "../M8_new/M8Center-Transient-Prescription.sss"

```

```

include "../M8_new/Ex-Core-Definition.sss"
include "../M8_new/CR-Type_cyl.sss"
include "../M8_new/Extra_Surfaces.sss"
include "../M8_new/A-s.sss"
include "../M8_new/Rods.sss"
%include "../M8_new/plots.sss"
%include "../M8_new/Detectors.sss"

```

```

% Description of Placement: C/S-1 & 4 (North) at 22" = 55.88cm
% Description of Placement: Comp-1 & 4 (North) at 58.5" = 148.59cm
% Description of Placement: Trans-1 & 4 (North) at 40.0" = 101.6cm

```

%Transient Data Summary Sheet for Transient 2893T on 2018.5.14

```
%trans 801 0 0 148.59 % compensation rods full out 58.5 in
```

%trans 802 0 0 79.934 % safety rods average raised 31.47 in

%trans 803 0 0 59.0296 % transient rods raised 23.24 in

trans 801 0 0 148.59 % compensation rods full out 58.5"

trans 802 0 0 68.88 % safety rods 27.1"

trans 803 0 0 70.87 % transient rods 27.9"

%transv U 802 tlim 0.0 0.09859 1 0.0 0.0 431.8 % reactivity test control rods average moved out
39.12 cm

```
%transv U 803 tlim 0.0 0.19718 1 0.0 0.0 215.9 % transient rods moved slower
```

transv U 803 tlim 0.0 0.142334 1 0.0 0.0 215.9 % transient rods moved slower

```
%trans 801 0 0 148.59 % compensation rods full out 58.5 inches
```

%trans	802	0	0	58.83	% safety rods
--------	-----	---	---	-------	---------------

```
%trans 803 0 0 65.0889 % transient rods
```

% Dummy Zone for M8 calibration

cell 9900 9900 air out -5999

% Rotate C & D half assemblies 180 Degrees

```
%trans 6100 0 0 0 0 0 180  % Flit D1-Half 180Deg
```

trans 5900 0 0 0 0 0 180 % Flit C-Half 180Deg

trans 9000 0 0 0 0 0 180 % Flit M8 vehicle

%
% %

% Build 159 assembly core

[illegible]

```
lat 101 1 0.0 0.0 19 19 10.16 % core array
```

[illegible][illegible]

11100 11100 11100 11100 11100 11100 11100 1200 11100 11100 11100 1200 11100 11100
11100 11100 11100 11100 11100

11100 11100 11100 11100 11100 1200 11100 11100 11100 11100 11100 11100 11100 1200
11100 11100 11100 11100 11100

[illegible][illegible]

11100 1200 11100 11100 11100

```

11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100 11100
11100 11100 11100 11100 11100
11100 11100 1300 11100 11100 1100 11100 11100 11100 11100 11100 11100 11100 1100 11100
11100 1300 11100 11100
11100 11100 11100 11100 11100 11100 11100 11100 11100 6100 11100 11100 11100 11100
11100 11100 11100 11100 11100
11100 11100 11100 11100 11100 11100 11100 11100 11100 9900 11100 11100 11100 11100
11100 11100 11100 11100 11100
11100 11100 11100 11100 11100 11100 11100 11100 11100 5900 11100 11100 11100 11100
11100 11100 11100 11100 11100
11100 11100 1300 11100 11100 1100 11100 11100 11100 5100 11100 11100 11100 1100 11100
11100 1300 11100 11100
11100 11100 11100 11100 11100 11100 11100 11100 11100 5100 11100 11100 11100 11100
11100 11100 11100 11100 11100
11100 11100 11100 1300 11100 11100 11100 11100 11100 5100 11100 11100 11100 11100
11100 1300 11100 11100 11100
11100 11100 11100 11100 11100 11100 11100 11100 11100 5100 11100 11100 11100 11100
11100 11100 11100 11100 11100
11100 11100 11100 11100 11100 1200 11100 11100 11100 5100 11100 11100 11100 1200 11100
11100 11100 11100 11100
11100 11100 11100 11100 11100 11100 11100 1200 11100 5100 11100 1200 11100 11100 11100
11100 11100 11100 11100
6000 11100 11100 11100 11100 11100 11100 11100 11100 5100 11100 11100 11100 11100
11100 11100 11100 11100 6000
6000 6000 11100 11100 11100 11100 11100 11100 11100 5100 11100 11100 11100 11100 11100
11100 11100 6000 6000

```

```

cell 8500 100 fill 9000 -9081 % Add Test Region
cell 8501 100 fill 101 9081

```

```

cell 5590 0 fill 1 -570 571 -572
cell 5591 0 outside 570
cell 5592 0 outside -571 -570
cell 5593 0 outside 572 -570

```

```

%%%%%%%%%%
%%%%%%%%%%
% RUN/PLOT OPTIONS
%%%%%%%%%%
%%%%%%%%%%
% --- boundary conditions (1-black, 2-reflective , 3-periodic):
set bc 1 1 1

```

```

tme simutime 2 10000 0 2 % --- 10 time interval for simulation (no population control)
tme dettime 2 40 0 2 % --- 30 time bins for detector

```

```

det 1 dr -15 void di dettime      % --- Neutron population as a function of time
det 2 dr -8 void di dettime      % --- Fission energy deposition as a function of time
det POW du 101 dm fuel di dettime
det NPOP dr -15 fuel di dettime
det POW_test dr -8 fuel di dettime

```

```
% --- Neutron population and criticality cycles:
%set pop 2800000 1000 100
%set savesrc "/M8_mark_source" 0.10 1.0 1 1 1
set dynsrc "/M8_1.5_source" 1
set nps 100000 1 simutime
set nbuf 3000
set pbuf 999
```

% normalization to power (1000 W)

```
set power 1000.0
```

```
set U235H 182.0 %U235 Heating value Default: 202.27MeV
%set fissh <ZAI1><H1><ZAI2><H2>...
```

```
%% Cross section regions
%% add high energy groups at 1E5 and 1E6 eV
set his 1
```

Subfiles:

Surfaces.sss

% TREAT - surfaces
% Javier Ortensi
% Idaho National Laboratory
% July 14 2015

```
% Ben Baker
% Added Slotted 48 inch assembly surfaces
% Modified: Changed surf 4, changed R2, R2 = 6.0207 (Was 6.0900)
%           I calculate it to be 6.02 and it was 6.02 on the original Afull 1 1.sss file as well.
```

surf 1 octa 0.0 0.0 4.82600 6.04775 % outside of fuel -- revision
 surf 2 octa 0.0 0.0 4.96570 6.25511 % outside of fuel gap
 surf 3 octa 0.0 0.0 5.02920 6.31860 % outside of fuel clad (also outside of Al clad)
 surf 4 octa 0.0 0.0 4.8006 6.0207 % outside of graphite
 % Changed surf 4, R2 = 6.0207 from 6.0900 on Jan 28, 2016
 surf 5 octa 0.0 0.0 4.9022 6.19161 % inside of Al clad
 surf 6 cuboid -4.1656 4.1656 -4.1656 4.1656 -500.0 500.0 % square graphite
 surf 7 cyl 0.0 0.0 0.36195 183.556250 190.39825 % off gas tube inner
 surf 8 cyl 0.0 0.0 0.47625 184.556250 190.51255 % off gas tube outer
 surf 9 cyl 0.0 0.0 0.9525 184.556250 206.62250 % hole in top reflector -- fuel assembly

% STD Assembly axial surfaces

surf 11 pz 3.486 % Bottom SS Grid + Al bottom fitting
 surf 12 pz 30.486 % oct graphite XS region 1
 surf 13 pz 53.1747500 % oct graphite XS region 2
 surf 14 pz 62.0647500 % square graphite bottom
 surf 15 pz 62.1917500 % Al clad
 surf 16 pz 62.5092500 % air
 surf 17 pz 62.8267500 % Zr spacer + plate
 surf 18 pz 82.8267500 % Fuel XS region 1
 surf 19 pz 163.814250 % Fuel XS region 2 - mod to match sertta
 surf 20 pz 183.794250 % Fuel XS region 1
 surf 21 pz 184.111750 % Zr spacer + plate
 surf 22 pz 184.429250 % air
 surf 23 pz 184.556250 % Al clad
 surf 24 pz 193.446250 % square graphite
 surf 25 pz 206.622500 % oct graphite w hole
 surf 26 pz 220.262500 % oct graphite XS region 2
 surf 27 pz 247.262500 % oct graphite XS region 1

% 11 Length 3.486
 % 12 Length 27
 % 13 Length 22.68875
 % 14 Length 8.89
 % 17 Length 0.762
 % 18 Length 20
 % 19 Length 80.9675
 % 20 Length 20
 % 23 Length 0.762
 % 25 Length 22.06625
 % 26 Length 13.64
 % 27 Length 27
 % upto 522 Length 8.02675

%

%

%surf 30 pz 192.643125 % end of off gas tube inner

%surf 31 pz 192.757425 % end of off gas tube outer

%%%

% CR ASSEMBLY SURFACES

%%%

% CR radial surfaces

surf 48 cyl 0.0 0.0 1.099852263 -500.0 500.0 % CR region 1

surf 49 cyl 0.0 0.0 1.555425987 -500.0 500.0 % CR region 2

surf 50 cyl 0.0 0.0 1.9050 -500.0 500.0 % CR region 3

surf 51 cyl 0.0 0.0 2.2225 -500.0 500.0 % cladding with 1.75" OD

surf 52 cyl 0.0 0.0 2.54 -500.0 500.0 % air in fuel and top oct graphite region

surf 53 cyl 0.0 0.0 2.8575 -500.0 500.0 % zirc-2 tube with 2.25" OD

surf 54 cyl 0.0 0.0 2.86893 -500.0 500.0 % air gap between zirc2 and aluminum in top sqr graphite

surf 55 cyl 0.0 0.0 2.877344 -500.0 500.0 % air gap /hole in lower short/long graphite

surf 56 cyl 0.0 0.0 2.897188 -500.0 500.0 % air gap /spacers

surf 57 cyl 0.0 0.0 2.9591 -500.0 500.0 % air gap /hole in fuel block

surf 58 cyl 0.0 0.0 3.15595 -500.0 500.0 % Al tube in upper sqr graphite region

surf 59 cyl 0.0 0.0 3.175 -500.0 500.0 % Al in upper oct graphite regions

% Slopes up from 58 to 59 as the you go up the Bearing Tube.

surf 60 cyl 0.0 0.0 3.25755 -500.0 500.0 % air gap /hole in upper short/long graphite

surf 61 cyl 0.0 0.0 2.25552 -500.0 500.0 % inside diameter for graphite bushing

surf 65 octa 0.0 0.0 4.9022 6.192348 % inside of Al clad/Base

% Un-necessary, 65 Same as 5. Only difference is if the base or end tube is used to calculate R2.

% Off-gas Tube

surf 77 cyl 3.143089642 3.143089642 0.36195 0.0 194.60195 % off gas tube inner

surf 78 cyl 3.143089642 3.143089642 0.47625 0.0 194.71625 % off gas tube outer

surf 79 cyl 3.143089642 3.143089642 0.63500 0.0 195.03375 % hole in top reflector -- CR assembly

% CR axial surfaces

surf 10 pz 2.143125 % Bottom SS Grid

surf 28 pz 198.52625 % Surf 24 (TOP square) + 2inch = x + 5.08cm [Top of Graphite Bushing for CR]

% revised CR positions - based on the transient rod position

%%
 %%%

% Control/Shutdown Specific Pz for CR at Position 0. As shown in M8-Cal report p.17

%%
 %%%

surf 851 pz	-306.64673	%Begin Graphite	-
Cronrol Rod Follower (For Shutdown Rod)			
surf 852 pz	-167.74175	%Top of Graphite	- Control Rod Follower
surf 853 pz	-163.93175	%Top of Steel plug	- Control Rod Follower
surf 854 pz	-157.89925	%Top Zr/Steel plug/Bottom Graphite	- Control Rod Follower
surf 855 pz	-120.75175	%Top of P1/P2 Graphite	- Upper Follower
surf 856 pz	-102.97175	%Top of steel plug	- Upper Follower
surf 857 pz	-96.93925	%Top of Zr/Steel plug	- Zr follower
surf 858 pz	43.39575	%Top of Graphite	- Zr follower
surf 859 pz	49.42825	%Top of Zr/Steel plug	- Zr follower
surf 860 pz	53.23825	%Top of Steel plug	-Poison Section
surf 861 pz	195.79575	%Top of B4C	-Poison Section
surf 862 pz	201.82825	%Top of grapple adaptor coupling	-Poison Section
surf 863 pz	210.08325	%Top of grapple adaptor	

%%
 %%%

% Transient Rods Specific Pz for CR at Position 0. As shown in M8-Cal report p.17

%%
 %%%

surf 871 pz	-258.38673	%Begin Graphite	-
Cronrol Rod Follower (For Shutdown Rod)			
surf 872 pz	-119.48175	%Top of Graphite	- Control Rod Follower
surf 873 pz	-115.67175	%Top of Steel plug	- Control Rod Follower
surf 874 pz	-109.63925	%Top Zr/Steel plug/Bottom Graphite	- Control Rod Follower
surf 875 pz	-86.77925	%Top of P1/P2 Graphite	- Upper Follower
surf 876 pz	-68.99925	%Top of steel plug	- Upper Follower
surf 877 pz	-62.96675	%Top of Zr/Steel plug	- Zr follower
surf 878 pz	77.36825	%Top of Graphite	- Zr follower
surf 879 pz	83.40075	%Top of Zr/Steel plug	- Zr follower
surf 880 pz	87.21075	%Top of Steel plug	-Poison Section
surf 881 pz	229.76825	%Top of B4C	-Poison Section
surf 882 pz	235.80075	%Top of grapple adaptor coupling	-Poison Section
surf 883 pz	244.05575	%Top of grapple adaptor	

%%
 %%

% Old CR - Min Critical (placed so that graphite cut out is 1.9" above core)

%%
 %%

surf 891 pz	-171.26473	%Begin Graphite	-
Cronrol Rod Follower (For Shutdown Rod)			
surf 892 pz	-32.35975	%Top of Graphite	- Control Rod Follower
surf 893 pz	-28.54975	%Top of Steel plug	- Control Rod Follower
surf 894 pz	-22.51725	%Top Zr/Steel plug/Bottom Graphite	- Control Rod Follower
surf 895 pz	14.63025	%Top of P1/P2 Graphite	- Upper Follower
surf 896 pz	32.41025	%Top of steel plug	- Upper Follower
surf 897 pz	38.44275	%Top of Zr/Steel plug	- Zr follower
surf 898 pz	178.77775	%Top of Graphite	- Zr follower
surf 899 pz	184.81025	%Top of Zr/Steel plug	- Zr follower
surf 900 pz	188.62025	%Top of Steel plug	-Poison Section
surf 901 pz	230.53025	%Origianl Section w/o B4C (Make it 16.5". It says removed 18" and 42" b4c but that isn't possible. The 1.5" is steel)	
surf 902 pz	331.17775	%Top of B4C	-Poison Section
surf 903 pz	337.21025	%Top of grapple adaptor coupling	-Poison Section
surf 904 pz	345.46525	%Top of grapple adaptor	

surf 90 inf % dummy domain

%%
 %%

% 48-inch Slotted ASSEMBLY SURFACES (H1-H-8 & H-11-H-18)

%%
 %%

% STD Slotted Radial surfaces

surf 5051 octa	0.0 0.0 5.02920 6.31860	% outside of all cladding
surf 5052 octa	0.0 0.0 4.9657 6.2551	% inside of Zr clad in Slot Region
surf 5053 octa	0.0 0.0 4.9022 6.19161	% inside of Al clad/(2x)Zr clad
surf 5054 octa	0.0 0.0 4.8006 6.02072	% outside of graphite/lead
surf 5055 cuboid	-3.4925 3.4925 -5.02920 5.02920 30.0 210.0	% Slot Region (open region x 2-3/4 in)
surf 5056 cuboid	-4.1671875 4.1671875 -4.1671875 4.1671875 30.0 210.0	% Square graphite
surf 5057 octa	-5.8954 0.0 2.1997 2.1997	% Smaller Zr support for LHS
surf 5058 octa	-5.8954 0.0 2.2632 2.2632	% Support outer surface for LHS
surf 5059 octa	5.8954 0.0 2.1997 2.1997	% Smaller Zr support for RHS

surf 5060 octa 5.8954 0.0 2.2632 2.2632

% Support outer surface for RHS

% STD Slotted axial surfaces

surf 5070 pz 1.723875 % Start HERE

surf 5071 pz 3.628875 % Al clad

surf 5072 pz 8.78825 % Top of Lead

surf 5073 pz 44.34825 % Top of Reflector #2 (14 inch)

surf 5074 pz 51.8095 % Top of Reflector #1

surf 5075 pz 59.4295 % Begin Zr (2x) Wall on Below Slot

surf 5076 pz 61.017 % Top of Square Graphite Below Slot

surf 5077 pz 61.0805 % Top of Zr Clad, End of (2x) Zr wall, begin (Zr shell + Air)

surf 5078 pz 62.3505 % Top of Zr before Slot, end (Zr shell+Air)

surf 5079 pz 184.2705 % Top of Slot Region, begin (Zr Shell + Air)

surf 5080 pz 185.5405 % Top of Zr Clad after Slot, end (Zr shell + Air), begin Zr (2x) wall

surf 5081 pz 185.604 % Top of Al Clad above Slot Region, begin square Reflector

surf 5082 pz 187.1915 % End of Zr (2x) Wall after slot

surf 5083 pz 194.8115 % Top of Square Graphite Above Slot

surf 5084 pz 206.559 % Top of Reflector #1 (above Slot)

surf 5085 pz 242.119 % Top of Reflector #2 (14 inch)

surf 5086 pz 247.2625 % Top of Lead above Slot (Really continues until 262.741 cm)

% Add Artificial pz to off-set air region in slotted assembly by a little bit

%surf 5087 pz 61.0800 % Just below air region (surf 5077)

%surf 5088 pz 185.5410 % Just above air region (surf 5080)

%%
 %%%

% outer surface

surf 5999 cyl 0. 0. 500.0 % dummy domain

% Single Assembly Definition: outside domain

surf 5900 cuboid -5.08 5.08 -5.08 5.08 -160.0 500

% M8 Cal Vehicle

surf 9099 cuboid -5.08 5.08 -10.16 10.16 0.0 500.0

%%
 %%%

% Additional Plains for half-slotted assembly (H-21) and Half-Graphite Assembly

% Additional planes

surf 5151 py -0.2667 % Outside of Zr clad on cut mark

surf 5152 py -0.3302 % inside of Zr clad on cut mark

surf 5153 py -0.3937 % Stiffener thickness on cut

surf 5154 px -4.0132 % LHS begin stiffener

surf 5155 px -3.9497 % LHS end stiffener
surf 5156 px 4.0132 % RHS end stiffener
surf 5157 px 3.9497 % RHS begin stiffener

% Radial Surfaces

surf 5158 cuboid -4.9657 -4.0132 -3.13182 -2.17932 0.0 210.0 % LHS square inner
surf 5159 cuboid 4.0132 4.9657 -3.13182 -2.17932 0.0 210.0 % RHS square inner
surf 5160 cuboid -4.9022 -3.9497 -3.19532 -2.11582 0.0 210.0 % LHS square outer
surf 5161 cuboid 3.9497 4.9022 -3.19532 -2.11582 0.0 210.0 % RHS square outer

% Additional axial surfaces

%surf 5165 pz 1.3118 % Bottom Fitting (Al-6061)
surf 5166 pz 3.2168 % P2 Extension (Al-6061)
%surf 5167 pz 23.5368 % Lead Brick
surf 5168 pz 43.8568 % Lead Brick
surf 5169 pz 59.747 % Graphite
surf 5170 pz 59.8105 % Zr Divider
surf 5171 pz 186.8105 % Air 50-inch slot
surf 5172 pz 186.874 % Zr Divider
surf 5173 pz 223.08424 % Graphite
surf 5174 pz 243.40424 % Lead Brick
surf 5175 pz 245.30924 % P1 Extension (Al-6061)
surf 5176 pz 247.2625 % Top Fitting (Al-6061)

%%
%%

% ENCLOSING BODIES FOR FULL ASSEMBLY AND CORE GEOMETRY

%%
%%

surf 500 cuboid -5.080 5.080 -5.080 5.080 0.0 255.289250 % assembly boundary
surf 520 cuboid -96.520 96.520 -96.520 96.520 0.0 255.289250 % 19x19 array boundary
surf 521 cuboid -15.24 15.24 -15.24 15.24 0.0 255.289250 % 3x3 array boundary
surf 522 cuboid -25.400 25.400 -25.400 25.400 0.0 255.289250 % 5x5 array boundary
surf 523 cuboid -15.24 15.24 -20.32 20.32 0.0 255.289250 % 3x4 array boundary

% Page 15 on ANL-6174 for dimensions of gaps and clad of PR

surf 530 cuboid -101.600 101.600 -101.600 101.600 0.0 255.289250 % 2" air gap outside core
surf 540 cuboid -102.235 102.235 -102.235 102.235 0.0 255.289250 % 0.25" thick aluminum
wall inside reflector

% Permanent Reflector (7ft-8in High - 2ft wide)

% Use 7-7/8" for the width of the PR 1 & PR 2 to match the Cavity Inserts for holes

surf 550 cuboid -122.2375 122.2375 -122.2375 122.2375 0.0 255.289250 % graphite PR 1 7-
7/8" inch wide

surf 551 cuboid -142.24 142.24 -142.24 142.24 0.0 255.289250 % graphite PR 2 7-7/8"
inch wide

surf 552 cuboid -163.195 163.195 -163.195 163.195 0.0 255.289250 % graphite PR 3 8-1/4" inch wide

surf 560 cuboid -163.83 163.83 -163.83 163.83 0.0 255.289250 % 0.25" thick aluminum wall outside reflector

surf 561 cuboid -168.91 168.91 -168.91 168.91 0.0 422.4 % 2" air gap between PR and Shield

% Shielding (Its ~ 5ft thick)

% The Walls are 15' on the long side and 4'-3" on the corners

% I'm assuming the corner angles are 45degrees which seems to be correct

% Based on the assumption the thickness of the concrete is ~5ft thick even on the corners.

%surf 570 cuboid -321.31 321.31 -321.31 321.31 0.0 350.0 % Concrete shield

%surf 570 cuboid -198.12 198.12 -198.12 198.12 0.0 350.0 % Concrete shield MAMMOTH model

% R1 ~= 10.5ft R2~= 12.73ft

surf 570 octa 0 0 320.197 388.059

surf 571 pz 0.0 % Start of Reactor

surf 572 pz 422.4 % Top of Reactor

% Air above the PR and other material to match up with the core

surf 555 pz 233.68 %Start of Air above Reflector and liners

surf 557 pz 270.0 %Approx end of air until concrete

%%%

% Core Axial CenterLine = 123.311 cm (Ref for Holes)

%%%

Ex-Core-Definition.sss

%%%

% Detector Ports

%%%

%% Startup & Steady State Det Ports

% West Wall

% Upper

% SS-DIS-Detector UPPER A Position

cell 300 300 air 710

cell 301 300 fill 350 -710

cell 302 350 SS_DIS -90

% Lower

```

cell 305 301 air      706
cell 306 301 fill 351 -706
cell 307 351 SS_RTS_A -90
% North Wall
% Upper
cell 310 302 air -90
% Lower
cell 315 303 air -90
% South Wall
% Upper
cell 320 304 air      728
cell 321 304 fill 354 -728
cell 322 354 Startup_DIS_A -90
% Lower
cell 325 305 air      729
cell 326 305 fill 355 -729
cell 327 355 SS_RTS_B -90

%% Transient Det Ports
% North-West
% Upper
cell 330 306 air      777
cell 331 306 fill 360 -776
cell 332 306 fill 361 -777 776
cell 333 360 B10TransA_up -90
cell 334 361 Cd_filter -90

% Lower
cell 335 307 air      742
cell 336 307 fill 362 -741
cell 337 307 fill 363 -742 741
cell 338 362 B10TransA_down -90
cell 339 363 Cd_filter -90

% North-East
% Upper
cell 340 308 air      779
cell 341 308 fill 364 -778
cell 342 308 fill 365 -779 778
cell 343 364 B10TransARCS_up -90
cell 344 365 Cd_filter -90

% Lower
cell 345 309 air      744
cell 346 309 fill 366 -743
cell 347 309 fill 367 -744 743

```

cell 348 366 B10TransARCS_down -90
 cell 349 367 Cd_filter -90

% South-West

% Upper

cell 350 310 air 781
 cell 351 310 fill 368 -780
 cell 352 310 fill 369 -781 780
 cell 353 368 B10TransB_up -90
 cell 354 369 Cd_filter -90

% Lower

cell 355 311 air 746
 cell 356 311 fill 370 -745
 cell 357 311 fill 371 -746 745
 cell 358 370 B10TransB_down -90
 cell 359 371 Cd_filter -90

% South-East

% Upper

cell 360 312 air 783
 cell 361 312 fill 372 -782
 cell 362 312 fill 373 -783 782
 cell 363 372 B10TransC_up -90
 cell 364 373 Cd_filter -90

% Lower

cell 365 313 air 748
 cell 366 313 fill 374 -747
 cell 367 313 fill 375 -748 747
 cell 368 374 B10TransC_down -90
 cell 369 375 Cd_filter -90

%%%

% Full Core

%%%

% Air Gap & Al Liner

cell 400 401 air -530:-610:-650:-660:-700:-702:-720:-722:-724:-726 % 2" air gap and
 opening in liner for North Face
 cell 401 401 aluminum 530 610 650 660 700 702 720 722 724 726 % Al clad PR liner
 inside

%%% REFLECTOR %%%%%%%%%%%%%%%%%%%%%%%%%%

% PR 1

% North Cavity

cell 405 402 air -620 % First part of first Insert

cell 406 402 air	-623	% First part of second Insert
cell 407 402 air	-625	% First part of third Insert
% West Cavity		
cell 408 402 graphite	-650	% First part of Insert
% South Cavity		
cell 409 402 graphite	-660	% First part of Insert

% Reflector PR1 Graphite

cell 416 402 graphite 620 623 625 650 660

% PR 2

% North Cavity		
cell 421 403 air	-621	% Second part of first Insert
cell 422 403 air	-624	% Second part of second Insert
cell 423 403 air	-626	% Second part of third Insert
% West Cavity		
cell 425 403 graphite	-651	% Second Part of Insert
% South Cavity		
cell 426 403 graphite	-661	% Second Part of Insert

% Reflector PR2 Graphite

cell 435 403 graphite 621 624 626 651 661

% PR 3

% North Cavity		
cell 440 404 air	-628	% Hodoscope Air Hole
% West Cavity		
cell 441 404 graphite	-651	% Extension after Second Part
% South Cavity		
cell 442 404 graphite	-661	% Extension after Second Part

% Reflector PR3 Graphite

cell 449 404 graphite 628 651 661

%%%%%%%%%%%% Air Gap %%%%%%%%%%

% Al Liner and Air Gap

cell 450 405 air 560:-628:-651:-661

cell 451 405 aluminum -560 628 651 661

%%%%%%%%%%%% SHIELD %%%%%%%%%%

% ThermoColumn

cell 460 406 graphite -680:-681

cell 461 406 concrete 680 681

%%%%%%%%%%%% Build Whole CORE --- COMBINE IT %%%%%%%%%%

cell 550 150 fill 100	-520	% 19x19 array region	
cell 551 150 fill 401	-540 520 -555	% 2" air gap with Al liner (Limit on Height)	
cell 552 150 fill 402	-550 540 -555	700 701 702 703 720 721 722 723 724 725 726 727	%
PR 1	(Limit on Height)		
cell 553 150 fill 403	-551 550 -555	700 701 702 703 720 721 722 723 724 725 726 727	%
PR 2	(Limit on Height)		
cell 554 150 fill 404	-552 551 -555	700 701 702 703 720 721 722 723 724 725 726 727	%
PR 3	(Limit on Height)		
cell 555 150 fill 405	-561 552 -555	700 701 702 703 720 721 722 723 724 725 726 727	
	750 752 754 756 760 762 764 766	% 2" air gap with Al	
liner (Limit on Height)			

cell 556 150 air	520 -561 555 -557	% Air above PR
regions and liners (Adds Height)		

cell 559 150 fill 406	(561:557) (700 701 702 703 720 721 722 723 724 725 726 727	
	750 751 752 753 754 755 756 757	
	760 761 762 763 764 765 766 767)	% Shield

% Instr. Holes

cell 560 150 fill 300	(-700:-701) 540	% Fill West Upper Inst. Hole
cell 561 150 fill 301	(-702:-703) 540	% Fill West Lower Inst. Hole
cell 562 150 fill 302	(-720:-721) 540	% Fill North Upper Inst. Hole
cell 563 150 fill 303	(-724:-725) 540	% Fill North Lower Inst. Hole
cell 564 150 fill 304	(-722:-723) 540	% Fill South Upper Inst. Hole
cell 565 150 fill 305	(-726:-727) 540	% Fill South Lower Inst. Hole

% Trans. Holes

%%%%%%%%%

% Upper

%%%%%%%%%

cell 566 150 fill 306	(-750:-751) 552	% Fill North-West Inst. Hole
cell 567 150 fill 308	(-752:-753) 552	% Fill North-East Inst. Hole
cell 568 150 fill 310	(-754:-755) 552	% Fill South-West Inst. Hole
cell 569 150 fill 312	(-756:-757) 552	% Fill South-East Inst. Hole

%%%%%%%%%

% Lower

%%%%%%%%%

cell 570 150 fill 307	(-760:-761) 552	% Fill North-West Inst. Hole
cell 571 150 fill 309	(-762:-763) 552	% Fill North-East Inst. Hole
cell 572 150 fill 311	(-764:-765) 552	% Fill South-West Inst. Hole
cell 573 150 fill 313	(-766:-767) 552	% Fill South-East Inst. Hole

```

%%%%%%%%%
%%%%%%%%%
%%%%%%%%%
%%%%%%%%%
%%%%%%%%%
%%%%%%%%%
%%%%%%%%%
%%%%%%%%%
%%%%%%%%%
%%%%%%%%%
%
% Generate cross section regions beyond the 19x19
cell 580 4000 fill 150 -1000 % 19x19
% zone PR1
cell 581 4101 fill 150 (-1022:-1023:-1024:-1025) -265 % air,liner,pr corner
cell 582 4102 fill 150 (-1022:-1023:-1024:-1025) 265 % air,liner,pr corner
cell 583 4401 fill 150 1000 -1001 (-1030:-1031:-1032:-1033:-1034:-1035) % det penetrations
cell 584 4201 fill 150 1000 -1001 -1036 % hodoscope
cell 585 4001 fill 150 (1000 -1001) (#581) (#583) (#584) -265 %air, liner, pr
cell 586 4002 fill 150 (1000 -1001) (#582) 265 %air, liner, pr
% zone PR2-6
cell 590 4302 fill 150 1001 -1005 -1036 % hodoscope hole
cell 591 4602 fill 150 1002 -1003 -729 %detector S lower
cell 592 4603 fill 150 1002 -1003 -728 %detector S upper
cell 593 4604 fill 150 1002 -1003 -706 %detector W lower
cell 594 4605 fill 150 1002 -1003 -710 %detector W upper
cell 595 4601 fill 150 1001 -1004 (-1030:-1031:-1032:-1033:-1034:-1035) (#591) (#592) (#593)
(#594) %detector hole empty
cell 596 4301 fill 150 1001 -1004 (#590) (#591) (#592) (#593) (#594) (#595) -265 %solid
cell 597 4303 fill 150 1001 -1004 265 %solid pr with top air
% zone PR7
cell 600 4703 fill 150 (-1026:-1027:-1028:-1029) -265 % out air,liner,pr corner
cell 601 4704 fill 150 (-1026:-1027:-1028:-1029) 265 % out air,liner,pr,top air corner
cell 603 4701 fill 150 1004 -1005 (#590) (#595) (#600) -265 % out air,liner,pr
cell 604 4702 fill 150 1004 -1005 (#601) 265 % out air,liner,pr,top air
% zone PR8-10
cell 610 4706 fill 150 -1037 % air TC
cell 611 4707 fill 150 1005 -1007 (-1030:-1031:-1032:-1033:-1034:-1035) % air concrete in
detector hole
cell 612 4705 fill 150 1005 -1007 1042 1043 1044 1045 (#610) (#611)
cell 613 4901 fill 150 -743 % detector lower NE
cell 614 4902 fill 150 -778 % detector upper NE
cell 615 4903 fill 150 -747 % detector lower SE
cell 616 4904 fill 150 -782 % detector upper SE
cell 617 4905 fill 150 -745 % detector lower SW
cell 618 4906 fill 150 -780 % detector upper SW
cell 619 4907 fill 150 -741 % detector lower NW

```

cell 620 4908 fill 150 -776 % detector upper NW
 cell 621 4802 fill 150 (-1046:-1047:-1048:-1049:-1050:-1051:-1052:-1053)
 (#600) (#601) (#613) (#614) (#615) (#616) (#617) (#618) (#619) (#620) %
 concrete w detector hole
 cell 622 4801 fill 150 (-1042:-1043:-1044:-1045) 1046 1047 1048 1049 1050 1051 1052 1053
 (#600) (#601) % concrete in corner outside holes
 cell 623 4999 fill 150 1007

 %
 % rebuild core
 cell 630 1 fill 4000 -1000 % 19x19
 % zone PR1
 cell 631 1 fill 4101 (-1022:-1023:-1024:-1025) -265 % air,liner,pr corner
 cell 632 1 fill 4102 (-1022:-1023:-1024:-1025) 265% air,liner,pr corner
 cell 633 1 fill 4401 1000 -1001 (-1030:-1031:-1032:-1033:-1034:-1035) % det penetrations
 cell 634 1 fill 4201 1000 -1001 -1036 % hodoscope
 cell 635 1 fill 4001 (1000 -1001) (#581) (#583) (#584) -265 %air, liner, pr
 cell 636 1 fill 4002 (1000 -1001) (#582) 265 %air, liner, pr
 % zone PR2-6
 cell 640 1 fill 4302 1001 -1005 -1036 % hodoscope hole
 cell 641 1 fill 4602 1002 -1003 -729 %detector S lower
 cell 642 1 fill 4603 1002 -1003 -728 %detector S upper
 cell 643 1 fill 4604 1002 -1003 -706 %detector W lower
 cell 644 1 fill 4605 1002 -1003 -710 %detector W upper
 cell 645 1 fill 4601 1001 -1004 (-1030:-1031:-1032:-1033:-1034:-1035) (#591) (#592) (#593)
 (#594) %detector hole empty
 cell 646 1 fill 4301 1001 -1004 (#590) (#591) (#592) (#593) (#594) (#595) -265 %solid
 cell 647 1 fill 4303 1001 -1004 265 %solid pr with top air
 % zone PR7
 cell 650 1 fill 4703 (-1026:-1027:-1028:-1029) -265 % out air,liner,pr corner
 cell 651 1 fill 4704 (-1026:-1027:-1028:-1029) 265 % out air,liner,pr corner
 cell 652 1 fill 4701 1004 -1005 (#590) (#595) (#600) -265 % out air,liner,pr
 cell 653 1 fill 4702 1004 -1005 (#601) 265 % out air,liner,pr,top air
 % zone PR8-10
 cell 660 1 fill 4706 -1037 % air TC
 cell 661 1 fill 4707 1005 -1007 (-1030:-1031:-1032:-1033:-1034:-1035) % air concrete in
 detector hole
 cell 662 1 fill 4705 1005 -1007 1042 1043 1044 1045 (#610) (#611)
 cell 663 1 fill 4901 -743 % detector lower NE
 cell 664 1 fill 4902 -778 % detector upper NE
 cell 665 1 fill 4903 -747 % detector lower SE
 cell 666 1 fill 4904 -782 % detector upper SE
 cell 667 1 fill 4905 -745 % detector lower SW
 cell 668 1 fill 4906 -780 % detector upper SW
 cell 669 1 fill 4907 -741 % detector lower NW
 cell 670 1 fill 4908 -776 % detector upper NW

cell 671 1 fill 4802 (-1046:-1047:-1048:-1049:-1050:-1051:-1052:-1053)
 (#600) (#601) (#613) (#614) (#615) (#616) (#617) (#618) (#619) (#620) %
 concrete w detector hole
 cell 672 1 fill 4801 (-1042:-1043:-1044:-1045) 1046 1047 1048 1049 1050 1051 1052 1053
 (#600) (#601) % concrete in corner outside holes
 cell 673 1 fill 4999 1007

Ex-Core-Surfaces.sss

%%
 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

% Core Axial CenterLine = 123.3105 cm (Ref for Holes)

%%
 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

%%

% Hodoscope (North Wall) - 600's

%%

% Long Cavity Insert (PR) Part

%%

% Real Dimensions (see Drawing 23201 - Reflector) 1st part 5-13/16" wide x 7-7/8" long x 60-3/4" height

% 2nd part 4-1/8" wide x 7-7/8" long same height

%% Liner on North Wall (12" above/below Axial Centerline and 7-1/8" right/left of Centerline)

% (x left) (x right) (y start) (y end) (z bottom) (z top)

% Actual

% surf 610 cuboid -18.0975 18.0975 101.600 102.235 82.6705 163.9505 % Al liner hole on North Wall (14-1/4" wide x 32" High)

% INF version

surf 610 cuboid -18.0975 18.0975 0.0 500.0 82.6705 163.9505 % Al liner hole on North Wall (14-1/4" wide x 32" High)

%% North Cavity

% y-axis starts after Al liner for Inserts. Assume Cavity is also 32" high.

% PR 1 & PR 2 lineup with the 1st and 2nd parts of the cavity

% Left Cavity (x left) (x right) (y start) (y end) (z bottom) (z top)

% Actual Size

% surf 620 cuboid -20.0025 -5.23875 102.235 122.2375 82.6705 163.9505 % 1st part of first Insert

% surf 621 cuboid -17.859375 -7.381875 122.2375 142.24 82.6705 163.9505 % 2nd part of first Insert

% INF Size
surf 620 cuboid -20.0025 -5.23875 50.0 500.0 82.6705 163.9505 % 1st part
of first Insert
surf 621 cuboid -17.859375 -7.381875 50.0 500.0 82.6705 163.9505 % 2nd
part of first Insert

% Center Cavity (x left) (x right) (y start) (y end) (z bottom) (z top)
% Actual Size
% surf 623 cuboid -5.23875 5.23875 102.235 122.2375 82.6705 163.9505 % 1st
part of second Insert
% surf 624 cuboid -7.381875 7.381875 122.2375 142.24 82.6705 163.9505 % 2nd
part of second Insert
% INF Size
surf 623 cuboid -5.23875 5.23875 50.0 500.0 82.6705 163.9505 % 1st part of
second Insert
surf 624 cuboid -7.381875 7.381875 50.0 500.0 82.6705 163.9505 % 2nd part
of second Insert

% Right Cavity (x left) (x right) (y start) (y end) (z bottom) (z top)
% Actual Size
% surf 625 cuboid 5.23875 20.0025 102.235 122.2375 82.6705 163.9505 % 1st
part of third Insert
% surf 626 cuboid 7.381875 17.859375 122.2375 142.24 82.6705 163.9505 % 2nd
part of third Insert
% INF Size
surf 625 cuboid 5.23875 20.0025 50.0 500.0 82.6705 163.9505 % 1st part of
third Insert
surf 626 cuboid 7.381875 17.859375 50.0 500.0 82.6705 163.9505 % 2nd part
of third Insert

% I have no record for the Tapper after the Inserts. I'm assuming air for now.
% Air after Inserts (x left) (x right) (y start) (y end) (z bottom) (z top)
% INF Size
surf 628 cuboid -17.859375 17.859375 0.0 500.0 82.6705 163.9505 % Air
after Inserts in Cavity
% (Extended it all the way to the concrete to cut through Al-outside + 2" air gap)

% Concrete Part
%%%%%%%%%%
% First hodoscope hole starts 12" below centerline and is 2ft high x 2ft wide x (~2.5'depth)
% Second hole is 3ft high x (2'=LHS of Centerline, 1'-4"=RHS of CL := 3'-4" wide) x 2.5'
depth

% Additional pyramids can be added to be an aperture for the beam. I will leave it open for now.

```
% First hole   (x left) (x right) (y start) (y end) (z bottom) (z top)
surf 630 cuboid -30.48  30.48  168.91  245.11  92.8305  153.7905 % First Hole in
Concrete (NORTH)
surf 631 cuboid -60.96  40.64  245.11  321.31  92.8305  153.7905 % Second Hole
in Concrete (NORTH)
```

```
%%%%%%%%%%%%%
% West Wall Cavity - 650's
%%%%%%%%%%%%%
% Size: First part=~5-7/8" wide x 7-15/16 long x 24" high, Second Part=~4.25" wide x 7.9" long
x 24" high
% Centered on Centerline
% West Wall Cavity (x left) (x right) (y start) (y end) (z bottom) (z top)
% INF Size
surf 650 cuboid -500.0 -50.0 -7.46125 7.46125 92.8305 153.7905 % 1st part of
Insert
surf 651 cuboid -500.0 -50.0 -5.3975 5.3975 92.8305 153.7905 % 2nd part of
Insert
% The second part can extend through the reflector and Al liner.
```

```
%%%%%%%%%%%%%
% South Wall Cavity - 660's
%%%%%%%%%%%%%
% Size: First part=~5-7/8" wide x 7-15/16 long x 24" high, Second Part=~4.25" wide x 7.9" long
x 24" high
% Centered on Centerline
% West Wall Cavity (x left) (x right) (y start) (y end) (z bottom) (z top)
% INF Size
surf 660 cuboid -7.46125 7.46125 -500.0 -50.0 92.8305 153.7905 % 1st part of
Insert
surf 661 cuboid -5.3975 5.3975 -500.0 -50.0 92.8305 153.7905 % 2nd part of
Insert
% The second part can extend through the reflector and Al liner.
% Note there is a retrofit block that is a wedge 2" high
```

```
%%%%%%%%%%%%%
% Thermo-column - 680's
%%%%%%%%%%%%%
%
% Thermocolumn liner is 32" wide x 4'-8" tall
% The graphite is actually 5'x 5' until 1/2 way through the concrete (ie. 2.5ft) then it's 5'-8" x 5'-
8"
%          Start (x) End (x) Start(y) End(y)   z1    z2
```

% Actual Size

% surf 680 cuboid 168.91 245.11 -76.2 76.2 47.1105 199.5105 % First Graphite Blocks

% surf 681 cuboid 245.11 321.31 -86.36 86.36 36.9505 209.6705 % Second Graphite Blocks

% Inf Size

surf 680 cuboid 0.0 500.0 -76.2 76.2 47.1105 199.5105 % First Graphite Blocks

surf 681 cuboid 245.11 500.0 -86.36 86.36 36.9505 209.6705 % Second Graphite Blocks

%%%

%%%

% West Instrument Holes - 700's

%%%

% This applies to all the holes that go through the permeant reflector

% Instrument Holes are located 1Ft above and below core CenterLine and 2ft from the core x-y center lines

% The holes are R=3.25" with a sleeve of 6" OD in the Reflector.

% The sleeve is 55-3/8" long which travels from the reflector into the shield.

% The hole changes to 8" dia for the last 2'-6.75" of the Shield.

%%%

% Upper Hole (DIS-SS in Upper A)

%%%

% y0 z0 r start(x1) End(x2)

% Actual Location

% surf 700 cylx 60.96 153.7905 7.62 -243.205 -102.235 % 6" Hole

% surf 701 cylx 60.96 153.7905 10.16 -321.31 -243.205 % 8" Hole

% INF Location

% surf 700 cylx 60.96 153.7905 7.62 -500 -60 % 6" Hole

% surf 701 cylx 60.96 153.7905 10.16 -500 -243.205 % 8" Hole

% replace with rectangular hole with same volume

surf 700 cuboid -500 -60 55.88 66.04 144.813399 162.767601 % 6" Hole

surf 701 cuboid -500 -243.205 55.38 66.54 139.2612533 168.3197467 % 8" Hole

%%%

% Lower Hole

%%%

% y0 z0 r start(x1) End(x2)

% Actual Location

% surf 702 cylx 60.96 92.8305 7.62 -243.205 -102.235 % 6" Hole

% surf 703 cylx 60.96 92.8305 10.16 -321.31 -243.205 % 8" Hole

% surf 702 cylx 60.96 92.8305 7.62 -500 -60 % 6" Hole

% surf 703 cylx 60.96 92.8305 10.16 -500 -243.205 % 8" Hole

```

% replace with rectangular hole with same volume
surf 702 cuboid -500 -60 55.88 66.04 83.85339899 101.807601 % 6" Hole
surf 703 cuboid -500 -243.205 55.38 66.54 78.30125329 107.3597467 % 8" Hole

%surf 706 cylx 60.96 92.8305 2.54 -145.733 -122.2375 % West-Lower Det
surf 706 cuboid -137.08380 -127.07620 55.95620 65.96380 87.28695
97.13455 % lower square detector
%%%%%%%%%%%%
% Interface
%%%%%%%%%%%%
surf 705 px -243.205 % 8" to 6" interface

% Cylinder for Detector
% Using the 8" to 6" dia holes and the det drawings the 6" dia region for the SS chamber
% is up to ~47.5" this means the closest to the core the detector can be is ~16" into the
reflector
% or 8" into the reflector from the core side. This is the end of the detector. Det Length =
12.94"
% The furthest away (ref being bottom of detector) is ~16.3" from the start of the concrete.
%
% Det Specs
% Active length = 9.25"
% Dia = 1.99", Fill Gas = N2, B-10 Lined.
%%%%%%%%
% DIS-SS Chamber
%%%%%%%%
%
% y0 z0 r start(x1) End(x2)
%surf 710 cylx 60.96 153.7905 2.54 -145.733 -122.2375
%surf 712 cylx 60.96 153.791 3.04 -146.233 -121.7375 % 1st Filter 0.5 cm thick

surf 710 cuboid -137.08380 -127.07620 55.95620 65.96380 147.28695
157.13455 % upper square detector
%%%%%%%%
surf 711 cylx 60.96 153.791 7.62 -103.235 -102.235 % puck in front of DIS-SS
Upper A hole
surf 713 cylx 60.96 153.791 7.62 -163.195 -102.235 % dummy upper hole

%%%%%%%%
% North & South Instrument Holes - 720's
%%%%%%%%
%%%%%%%%
% Upper Hole
%%%%%%%%
%
% x0 z0 r start(y1) End(y2)

```

% INF Location

% surf 720 cyly	60.96	153.7905	7.62	60	500	% 6" Hole (North)
% surf 721 cyly	60.96	153.7905	10.16	243.205	500	% 8" Hole (North)
% surf 722 cyly	-60.96	153.7905	7.62	-500	-60	% 6" Hole (South)
% surf 723 cyly	-60.96	153.7905	10.16	-500	-243.205	% 8" Hole (South)

% replace with rectangular hole with same volume

surf 720 cuboid	55.88	66.04	60	500.0	144.813399	162.767601	% 6" Hole
(North)							
surf 721 cuboid	55.88	66.04	243.205	500.0	139.2612533	168.3197467	% 8" Hole
(North)							
surf 722 cuboid	-66.04	-55.88	-500	-60.0	144.813399	162.767601	% 6" Hole
(South)							
surf 723 cuboid	-66.04	-55.88	-500	-243.205	139.2612533	168.3197467	% 8" Hole
(South)							

%surf 728 cyly -60.96 153.7905 2.54 -145.733 -122.2375 % South-Upper Det

surf 728 cuboid -65.96380 -55.95620 -137.08380 -127.07620 147.28695

157.13455 % upper square detector

%%%%%%%%%

% Lower Hole

%%%%%%%%%

% x0 z0 r start(y1) End(y2)

% INF Location

% surf 724 cyly	60.96	92.8305	7.62	60	500	% 6" Hole (North)
% surf 725 cyly	60.96	92.8305	10.16	243.205	500	% 8" Hole (North)
% surf 726 cyly	-60.96	92.8305	7.62	-500	-60	% 6" Hole (South)
% surf 727 cyly	-60.96	92.8305	10.16	-500	-243.205	% 8" Hole (South)

% replace with rectangular hole with same volume

surf 724 cuboid	55.88	66.04	60	500.0	83.85339899	101.807601	% 6" Hole
(North)							
surf 725 cuboid	55.88	66.04	243.205	500.0	78.30125329	107.3597467	% 8" Hole
(North)							
surf 726 cuboid	-66.04	-55.88	-500	-60.0	83.85339899	101.807601	% 6" Hole
(South)							
surf 727 cuboid	-66.04	-55.88	-500	-243.205	78.30125329	107.3597467	% 8" Hole
(South)							

%surf 729 cyly -60.96 92.8305 2.54 -145.733 -122.2375 % South-Lower Det

surf 729 cuboid -65.96380 -55.95620 -137.08380 -127.07620 87.28695

97.13455 % lower square detector

%%%%%%%%%

% Interface

%%%%%%%%%

% x0 z0 r start(y1) End(y2)

surf 730 py 243.205 % 8" to 6" interface (North)

surf 731 py -243.205 % 8" to 6" interface (South)

%%%%%%%%%

%%%%%%%%%

% North-West & South-East Instrument Holes - 750-760's

%%%%%%%%%

%%%%%%%%%

% Upper Hole

%%%%%%%%%

% x0 y0 r start(y1) End(y2)

% INF Location

surf 750 cyl 0.0 0.0 7.62 -320.0 -30.0 % 6" Hole (North-West)

surf 751 cyl 0.0 0.0 10.16 -500.0 -309.905 % 8" Hole (North-West)

surf 752 cyl 0.0 0.0 7.62 -320.0 -30.0 % 6" Hole (North-East)

surf 753 cyl 0.0 0.0 10.16 -500.0 -309.905 % 8" Hole (North-East)

surf 754 cyl 0.0 0.0 7.62 30.0 320.0 % 6" Hole (South-West)

surf 755 cyl 0.0 0.0 10.16 309.905 500.0 % 8" Hole (South-West)

surf 756 cyl 0.0 0.0 7.62 30.0 309.905 % 6" Hole (South-East)

surf 757 cyl 0.0 0.0 10.16 309.905 500.0 % 8" Hole (South-East)

% Translate up 153.7905 on z-axis then rotate about x-axis -90 Deg (sends to x-y plane)

% then +/- 45 deg about y-axis which is really z-axis after rotating on x-axis

trans S 750 0 0 153.7905 -90 -45 0 1

trans S 751 0 0 153.7905 -90 -45 0 1

trans S 752 0 0 153.7905 -90 45 0 1

trans S 753 0 0 153.7905 -90 45 0 1

trans S 754 0 0 153.7905 -90 45 0 1

trans S 755 0 0 153.7905 -90 45 0 1

trans S 756 0 0 153.7905 -90 -45 0 1

trans S 757 0 0 153.7905 -90 -45 0 1

%%%%%%%%% ADDED For Tallies For the Air Chamber (Starts = ~239cm, Ends = ~309.905cm Length ~27.9")

surf 770 cyl 0.0 0.0 7.62 -309.905 -239.0 % NW-up Air Chamber

surf 771 cyl 0.0 0.0 7.62 -240.0 -239.0 % NW-up puck

surf 772 cyl 0.0 0.0 7.62 239.0 309.905 % SW-up Air Chamber

surf 773 cyl 0.0 0.0 7.62 239.0 240.0 % SW-up puck

surf 774 cyl 0.0 0.0 7.62 -309.905 -239.0 % NE-up Air Chamber

surf 775 cyl 0.0 0.0 7.62 239.0 309.905 % SE-up Air Chamber

trans S 770 0 0 153.7905 -90 -45 0 1 % NW Air

```

trans S 771 0 0 153.7905 -90 -45 0 1 % NW-puck
trans S 772 0 0 153.7905 -90 45 0 1 % SW Air
trans S 773 0 0 153.7905 -90 45 0 1 % SW-puck
trans S 774 0 0 153.7905 -90 45 0 1 % NE Air
trans S 775 0 0 153.7905 -90 -45 0 1 % SE Air

surf 776 cuboid -187.8838 -177.8762 177.8762 187.8838 147.28695
157.13455 % NW upper square detector - det
surf 777 cuboid -187.96 -177.8 177.8 187.96 147.21075
157.21075 % NW upper square detector - Cd
surf 778 cuboid 177.8762 187.8838 177.8762 187.8838 147.28695
157.13455 % NE upper square detector - det
surf 779 cuboid 177.8 187.96 177.8 187.96 147.21075 157.21075 %
NE upper square detector - Cd
surf 780 cuboid -187.8838 -177.8762 -187.8838 -177.8762 147.21075
157.13455 % SW upper square detector - det
surf 781 cuboid -187.96 -177.8 -187.96 -177.8 147.21075
157.21075 % SW upper square detector - Cd
surf 782 cuboid 177.8762 187.8838 -187.8838 -177.8762 147.28695
157.13455 % SE upper square detector - det
surf 783 cuboid 177.8 187.96 -187.96 -177.8 147.21075
157.21075 % SE upper square detector - Cd

```

```

%%%%%%%%%%

```

```

% Lower Hole

```

```

%%%%%%%%%%

```

```

% x0 y0 r start(y1) End(y2)

```

```

% INF Location

```

surf 760 cyl	0.0	0.0	7.62	-320.0	-30.0	% 6" Hole (North-West)
surf 761 cyl	0.0	0.0	10.16	-500.0	-309.905	% 8" Hole (North-West)
surf 762 cyl	0.0	0.0	7.62	-320.0	-30.0	% 6" Hole (North-East)
surf 763 cyl	0.0	0.0	10.16	-500.0	-309.905	% 8" Hole (North-East)
surf 764 cyl	0.0	0.0	7.62	30.0	320.0	% 6" Hole (South-West)
surf 765 cyl	0.0	0.0	10.16	309.905	500.0	% 8" Hole (South-West)
surf 766 cyl	0.0	0.0	7.62	30.0	309.905	% 6" Hole (South-East)
surf 767 cyl	0.0	0.0	10.16	309.905	500.0	% 8" Hole (South-East)

```

% Rotate surface -90 deg around y-axis, -45 deg about z-axis then translate up 153.7905 on
z-axis (2=Rotation before Translation)

```

```

trans S 760 0 0 92.8305 -90 -45 0 1

```

```

trans S 761 0 0 92.8305 -90 -45 0 1

```

```

trans S 762 0 0 92.8305 -90 45 0 1

```

trans S 763 0 0 92.8305 -90 45 0 1
trans S 764 0 0 92.8305 -90 45 0 1
trans S 765 0 0 92.8305 -90 45 0 1
trans S 766 0 0 92.8305 -90 -45 0 1
trans S 767 0 0 92.8305 -90 -45 0 1

%%%%%%%%% ADDED For Tallies For the Air Chamber (Starts = ~239cm, Ends = ~309.905cm Length ~27.9")

surf 735 cyl 0.0 0.0 7.62 -309.905 -239.0 % NW-down Air Chamber
surf 736 cyl 0.0 0.0 7.62 -240.0 -239.0 % NW-down puck
surf 737 cyl 0.0 0.0 7.62 239.0 309.905 % SW-down Air Chamber
surf 738 cyl 0.0 0.0 7.62 239.0 240.0 % SW-down puck
surf 739 cyl 0.0 0.0 7.62 -309.905 -239.0 % NE-down Air Chamber
surf 740 cyl 0.0 0.0 7.62 239.0 309.905 % SE-down Air Chamber

trans S 735 0 0 92.8305 -90 -45 0 1 % NW Air
trans S 736 0 0 92.8305 -90 -45 0 1 % NW-puck
trans S 737 0 0 92.8305 -90 45 0 1 % SW Air
trans S 738 0 0 92.8305 -90 45 0 1 % SW-puck
trans S 739 0 0 92.8305 -90 45 0 1 % NE Air
trans S 740 0 0 92.8305 -90 -45 0 1 % SE Air

%%%%%%%%% ADDED For Chamber and Cd Filter (nominal=30mills = 0.0762cm)
%%%%%%%%% Choose Close or Far From the Reflector

surf 741 cuboid -187.8838 -177.8762 177.8762 187.8838 87.21075
97.21075 % NW lower square detector - det
surf 742 cuboid -187.96 -177.8 177.8 187.96 87.21075 97.21075 %
NW lower square detector - Cd
surf 743 cuboid 177.8762 187.8838 177.8762 187.8838 87.21075
97.21075 % NE lower square detector - det
surf 744 cuboid 177.8 187.96 177.8 187.96 87.21075 97.21075 %
NE lower square detector - Cd
surf 745 cuboid -187.8838 -177.8762 -187.8838 -177.8762 87.21075
97.21075 % SW lower square detector - det
surf 746 cuboid -187.96 -177.8 -187.96 -177.8 87.21075 97.21075 %
SW lower square detector - Cd
surf 747 cuboid 177.8762 187.8838 -187.8838 -177.8762 87.21075
97.21075 % SE lower square detector - det
surf 748 cuboid 177.8 187.96 -187.96 -177.8 87.21075 97.21075 %
SE lower square detector - Cd

%%%%%%%%%
% Diagonal Cuts for PR to make North/South/East/West sides
%%%%%%%%%

surf 790 plane -1 -1 0 0
surf 791 plane 1 -1 0 0

% Planes for axial cuts in PR & Liner

surf 792 pz 85.2105
surf 793 pz 100.4505
surf 794 pz 146.1705
surf 795 pz 161.4105

% surfaces to define cross section regions beyond the 19x19

surf 1000 cuboid -96.52 96.52 -96.52 96.52 -100.0 400 % 19x19
surf 1001 cuboid -106.68 106.68 -106.68 106.68 -100.0 400 % PR1
surf 1002 cuboid -127.0 127.0 -127.0 127.0 -100.0 400 % PR3
surf 1003 cuboid -137.16 137.16 -137.16 137.16 -100.0 400 % PR4
surf 1004 cuboid -157.48 157.48 -157.48 157.48 -100.0 400 % PR6
surf 1005 cuboid -167.64 167.64 -167.64 167.64 -100.0 400 % PR7
surf 1006 cuboid -177.8 177.8 -177.8 177.8 -100.0 400 % PR8
surf 1007 cuboid -198.12 198.12 -198.12 198.12 -100.0 400 % PR10

surf 1022 cuboid 96.52 106.68 96.52 106.68 -100.0 400 % NE corner air pr liner
surf 1023 cuboid 96.52 106.68 -106.68 -96.52 -100.0 400 % SE corner air pr liner
surf 1024 cuboid -106.68 -96.52 -106.68 -96.52 -100.0 400 % SW corner air pr liner
surf 1025 cuboid -106.68 -96.52 96.52 106.68 -100.0 400 % NW corner air pr liner

surf 1026 cuboid 157.48 167.64 157.48 167.64 -100.0 400 % NE corner outer air pr liner
surf 1027 cuboid 157.48 167.64 -167.64 -157.48 -100.0 400 % SE corner outer air pr liner
surf 1028 cuboid -167.64 -157.48 -167.64 -157.48 -100.0 400 % SW corner outer air pr liner
surf 1029 cuboid -167.64 -157.48 157.48 167.64 -100.0 400 % NW corner outer air pr liner

surf 1030 cuboid 55.88 66.04 96.52 200.0 137.21075 163.79425 % N upper penetration
surf 1031 cuboid 55.88 66.04 96.52 200.0 82.82675 107.21075 % N lower penetration
surf 1032 cuboid -200.0 -96.52 55.88 66.04 137.21075 163.79425 % W upper penetration
surf 1033 cuboid -200.0 -96.52 55.88 66.04 82.82675 107.21075 % W lower penetration
surf 1034 cuboid -66.04 -55.88 -200.0 -96.52 137.21075 163.79425 % S upper penetration
surf 1035 cuboid -66.04 -55.88 -200.0 -96.52 82.82675 107.21075 % S lower penetration

surf 1036 cuboid -25.4 25.4 96.52 167.64 82.82675 163.79425 % hodoscope hole
surf 1037 cuboid 167.64 198.12 -66.04 66.04 41.830375 206.6225 % Thermal column

surf 1042 cuboid 157.48 198.12 157.48 198.12 -100.0 400 % 4x4 NE corner
surf 1043 cuboid 157.48 198.12 -198.12 -157.48 -100.0 400 % 4x4 SE corner
surf 1044 cuboid -198.12 -157.48 -198.12 -157.48 -100.0 400 % 4x4 SW corner
surf 1045 cuboid -198.12 -157.48 157.48 198.12 -100.0 400 % 4x4 NW corner

```

surf 1046 cuboid 157.48 198.12 157.48 198.12 137.21075 163.79425 % 4x4 NE corner
upper hole region only
surf 1047 cuboid 157.48 198.12 -198.12 -157.48 137.21075 163.79425 % 4x4 SE corner
upper hole region only
surf 1048 cuboid -198.12 -157.48 -198.12 -157.48 137.21075 163.79425 % 4x4 SW corner
upper hole region only
surf 1049 cuboid -198.12 -157.48 157.48 198.12 137.21075 163.79425 % 4x4 NW corner
upper hole region only

surf 1050 cuboid 157.48 198.12 157.48 198.12 82.82675 107.21075 % 4x4 NE corner
lower hole region only
surf 1051 cuboid 157.48 198.12 -198.12 -157.48 82.82675 107.21075 % 4x4 SE corner
lower hole region only
surf 1052 cuboid -198.12 -157.48 -198.12 -157.48 82.82675 107.21075 % 4x4 SW corner
lower hole region only
surf 1053 cuboid -198.12 -157.48 157.48 198.12 82.82675 107.21075 % 4x4 NW corner
lower hole region only

```

mat.sss

```

%% Fuel at 293.6K
%% all other materials at 293.6K
%% low boron

```

```

% Boron Detectors
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```

% Boron Detectors
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%% Startup & Steady-State %
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% West-Upper: A = SS-DIS-Linear (Linear Oper.), B = Startup-DIS-A (Startup A)
mat SS_DIS sum tmp 294.0 rgb 15 29 200 %% DIS-SS (West-Upper)

```

```

5010.80c 1.5616E-06 % Based on B4c

```

```

% West-Lower: A = SS-RTS-A-Linear (Linear A), B = SS-RTS-A-Log/Period (Log/Period A)
mat SS_RTS_A sum tmp 294.0 rgb 15 29 200 %% (West-Lower)
5010.80c 1.5616E-06 % Based on B4c

```

```

% South-Upper: A = Startup-DIS-B (Startup B), B = No INFO.
mat Startup_DIS_A sum tmp 294.0 rgb 15 29 200 %% (South-Upper)
5010.80c 1.5616E-06 % Based on B4c

```

```

% South-Lower: A = SS-RTS-B-Linear (Linear B), B = SS-RTS-B-Log/Period (Log/Period B)

```

```
mat SS_RTS_B sum tmp 294.0 rgb 15 29 200  %% (South-Lower)
5010.80c 1.5616E-06  % Based on B4c
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%% Transient B-10 Detectors %%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
% NW-Upper: A = Trans-RTS-A-Linear (Linear A), B = Trans-RTS-A-Energy (Energy A)
mat B10TransA_up sum tmp 294.0 rgb 15 29 200
5010.80c 1.5616E-06  % Based on B4c
```

```
% NW-Lower: A = , B = Trans-RTS-A-Log/Period (Log/Period A) (Could be A)
mat B10TransA_down sum tmp 294.0 rgb 15 29 200
5010.80c 1.5616E-06  % Based on B4c
```

```
% SW-Upper: A = Trans-RTS-B-Linear (Linear B), B = Trans-RTS-B-Energy (Energy B)
mat B10TransB_up sum tmp 294.0 rgb 15 29 200
5010.80c 1.5616E-06  % Based on B4c
```

```
% SW-Lower: A = , B = Trans-RTS-B-Log/Period (Log/Period B) (Could be A)
mat B10TransB_down sum tmp 294.0 rgb 15 29 200
5010.80c 1.5616E-06  % Based on B4c
```

```
% SE-Upper: A = Trans-RTS-C-Linear (Linear C), C = Trans-RTS-C-Energy (Energy C)
mat B10TransC_up sum tmp 294.0 rgb 15 29 200
5010.80c 1.5616E-06  % Based on B4c
```

```
% SE-Lower: A = , B = Trans-RTS-C-Log/Period (Log/Period C) (Could be A)
mat B10TransC_down sum tmp 294.0 rgb 15 29 200
5010.80c 1.5616E-06  % Based on B4c
```

```
% NE-Upper: A = ARCS-Linear, B = ARCS-Log/Period
mat B10TransARCS_up sum tmp 294.0 rgb 15 29 200
5010.80c 1.5616E-06  % Based on B4c
```

```
% NE-Lower: A = No INFO., B = No INFO.
mat B10TransARCS_down sum tmp 294.0 rgb 15 29 200
5010.80c 1.5616E-06  % Based on B4c
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
%%%%%%%% Cd Filter on Detectors
mat Cd_filter sum tmp 294.0 rgb 255 5 10
48106.80c 5.8259E-04
48108.80c 4.1480E-04
48110.80c 5.8305E-03
```

48111.80c 5.9704E-03
 48112.80c 1.1246E-02
 48113.80c 5.6954E-03
 48114.80c 1.3386E-02
 48116.80c 3.4815E-03

% Boron Filter on Detectors

mat B_filter sum tmp 294.0 rgb 215 229 200
 5010.80c 1.5616E-02 % Based on B4c

% Indium Filter

mat In_filter sum tmp 294.0 rgb 200 129 100
 49113.80c 1.6448E-03
 49115.80c 3.6695E-02

% Hafnium

mat Hafnium_filter sum tmp 294.0 rgb 100 229 50
 72174.80c 7.05541E-05
 72176.80c 0.002319467
 72177.80c 0.008201917
 72178.80c 0.012029479
 72179.80c 0.00600592
 72180.80c 0.015468993

% Silver

mat Silver_filter sum tmp 294.0 rgb 50 220 150
 47107.80c 3.0387E-02
 47109.80c 2.8231E-02

% --- Materials:

%mat fuel sum tmp 294.0 moder gra_300 6000 rgb 238 59 59
 %6000.80c 5.0874E-02
 %6002.80c 3.5353E-02
 %% NOT 5.9 ppm but 7.6 ppm boron
 %5010.80c 1.4495E-07
 %5011.80c 5.8343E-07
 %% 7.6 ppm boron
 %%5010.80c 1.8672E-07
 %%5011.80c 7.5154E-07
 %92235.80c 8.6849E-06
 %92238.80c 6.2967E-07
 %26054.80c 6.5286E-07
 %26056.80c 1.0239E-05
 %26057.80c 2.3659E-07

%26058.80c 3.1248E-08

%8016.80c 1.8623E-05

% -- Michigan fuel

mat fuel sum tmp 294.0 moder gra_300 6000 rgb 238 59 59

6000.80c 5.1039E-02

6002.80c 3.5468E-02

5010.80c 1.4440E-07

5011.80c 5.8124E-07

8016.80c 1.8685E-05

23050.80c 1.5339E-09

23051.80c 6.1201E-07

26054.80c 2.9114E-07

26056.80c 4.5703E-06

26057.80c 1.0555E-07

26058.80c 1.4047E-08

92234.80c 8.5472E-08

92235.80c 8.7202E-06

92236.80c 4.0790E-08

92238.80c 4.9986E-07

% 900 ppm hydrogen impurity

1001.80c 9.3015E-04

1002.80c 1.0698E-07

%%%%%%%%%%

% Experiment

%%%%%%%%%%

% Transient Prescription

% wire: Dia=1.59 mm or 1.82 mm (not sure)

% actual heights are set to be 5 mm. But I am using 2cm for better stats.

%

% U235 is 0.36 wt% and 0.36 at%

% Assuming density = 19.1 g/cm³ for DU then

% U238 = 4.815E22 at/cm³ = 0.04815 at/b-cm

% U235 = 1.739E20 at/cm³ = 0.0001739 at/b-cm

% If we homogenize the wire with the air for larger volume (use area's lengths are equal)

% Area of Wire = $\pi \cdot (0.159\text{cm}/2)^2 = 0.019856 \text{ cm}^2$

% Area of Titanium Tube = $\pi \cdot (0.3175\text{cm}^2 - 0.2286\text{cm}^2) = 0.1525 \text{ cm}^2$

% Total Area = $\pi \cdot (1.4224\text{cm})^2 = 6.356 \text{ cm}^2$

% Area of Air = $\pi \cdot ((1.4224\text{cm})^2 - \text{Area of Titanium} - \text{Area of Wire}) = 6.18376 \text{ cm}^2$

% Ratio of Areas: Air/Total = 0.97288, Wire/Total = 3.12E-3, Ti/Total = 0.023995

%

mat FissionWire sum tmp 294.0 rgb 135 29 48

% U (only ballpark numbers)

92238.80c 1.504254E-04

92235.80c 5.433401E-07

% Air

6000.80c 7.375505E-09

7014.80c 3.841322E-05

8016.80c 1.032032E-05

% Titanium

%22000.80c 1.3605E-04

22046.80c 1.12241E-05

22047.80c 1.01221E-05

22048.80c 1.00296E-04

22049.80c 7.36030E-06

22050.80c 7.04739E-06

mat WireHolder sum tmp 294.0 rgb 0 120 120

% Titanium - Actual 5.6698E-03 at/b-cm (total)

%22000.80c 1.99405E-04 % Homogenized with Air

22046.80c 1.64509E-05

22047.80c 1.48357E-05

22048.80c 1.47002E-04

22049.80c 1.07878E-05

22050.80c 1.03292E-05

% Air

6000.80c 7.31448E-09

7014.80c 3.80954E-05

8016.80c 1.02349E-05

% Flux Wires

mat FeWire sum tmp 294.0 rgb 20 29 20

% Iron Fe54 (n,p) Reaction

26054.80c 6.14E-06

mat TiWire sum tmp 294.0 rgb 30 30 30

% Ti46(n,p) Reaction

22046.80c 5.77905E-06

mat NbWire sum tmp 294.0 rgb 50 50 50

% Nb93(n,gamma) and (n,n') Reactions

41093.80c 6.86411E-05

mat CoWire sum tmp 294.0 rgb 60 60 60

% Co59(n,gamma) Reaction

27059.80c 1.12377E-7

%13027.80c 7.43892e-5

mat PerDuWire sum tmp 294.0 rgb 135 29 48 %% Peripheral Du Wires

% U (only ballpark numbers)

92238.80c 3.116038E-03

92235.80c 1.125520E-05

% Air

6000.80c 3.321630E-09

7014.80c 1.729976E-05

8016.80c 4.647854E-06

% Titanium

22046.80c 2.32506E-04

22047.80c 2.09678E-04

22048.80c 2.07762E-03

22049.80c 1.52467E-04

22050.80c 1.45985E-04

% FROM M8

%%% Test Sample: U-Zr: 19.8wt % U-235 and 6.0 wt. % Uranium (About 2mg/inch)

%%% mat test_pin sum tmp 294.0 rgb 238 59 59

%%% % U

%%% 92235.80c 2.488346E-04

%%% 92238.80c 9.951746E-04

%%% % Zr

%%% 40090.80c 2.610042E-02

%%% 40091.80c 5.691869E-03

%%% 40092.80c 8.700138E-03

%%% 40094.80c 8.816817E-03

%%% 40096.80c 1.420431E-03

%% mat air_fuel1 sum tmp 294.0 rgb 238 59 59 %rgb 204 255 255

%% % U (See the Test-Assembly.xlsx file inside of the T-TestCenter folder on my desktop)

%% 92235.80c 3.173910E-07

%% 92238.80c 1.269355E-06

%% % Zr

%% 40090.80c 3.329135E-05

%% 40091.80c 7.260037E-06

%% 40092.80c 1.109712E-05

%% 40094.80c 1.124594E-05

%% 40096.80c 1.811774E-06

%% % air

%% 6000.80c 7.59330E-09

%% 7014.80c 3.95476E-05

%% 8016.80c 1.06251E-05

%%

%% %mat fuel2 sum tmp 294.0 moder gra_300 6000 rgb 238 59 59

%% %6000.80c 5.0874E-02

%% %6002.80c 3.5353E-02

%% %92235.80c 1.1000E-04

```
%%%%%%%%%%
%
%%%%%%%%%
```

```
mat air_fuel1 sum tmp 294.0 rgb 238 59 59 %rgb 204 255 255
% U (See the Test-Assembly.xlsx file inside of the T-TestCenter folder on my desktop)
92235.80c 3.173910E-07
92238.80c 1.269355E-06
% Zr
40090.80c 3.329135E-05
40091.80c 7.260037E-06
40092.80c 1.109712E-05
40094.80c 1.124594E-05
40096.80c 1.811774E-06
% air
6000.80c 7.59330E-09
7014.80c 3.95476E-05
8016.80c 1.06251E-05
```

```
%mat fuel2 sum tmp 294.0 moder gra_300 6000 rgb 238 59 59
%6000.80c 5.0874E-02
%6002.80c 3.5353E-02
%92235.80c 1.1000E-04
```

```
mat zr sum tmp 294.0 rgb 160 160 160
% B
5010.80c 1.3751E-07
5011.80c 5.9006E-07
% Cr
24050.80c 9.8706E-08
24052.80c 1.9013E-06
24053.80c 2.1556E-07
24054.80c 5.3551E-08
% Fe
26054.80c 1.1659E-05
26056.80c 1.8285E-04
26057.80c 4.2252E-06
26058.80c 5.5804E-07
% Ni
28058.80c 2.2803E-07
28060.80c 8.7821E-08
28061.80c 3.8183E-09
```

28062.80c 2.2207E-08

28064.80c 3.1149E-09

% Zr

40090.80c 2.2054E-02

40091.80c 4.8095E-03

40092.80c 7.3513E-03

40094.80c 7.4499E-03

40096.80c 1.2002E-03

% Cd

48106.80c 8.7468E-11

48108.80c 6.2277E-11

48110.80c 8.7398E-10

48111.80c 8.9567E-10

48112.80c 1.6885E-09

48113.80c 8.5508E-10

48114.80c 2.0104E-09

48116.80c 5.2411E-10

% Sn

50112.80c 8.9997E-07

50114.80c 6.1235E-07

50115.80c 3.1545E-07

50116.80c 1.3490E-05

50117.80c 7.1255E-06

50118.80c 2.2471E-05

50119.80c 7.9698E-06

50120.80c 3.0228E-05

50122.80c 4.2957E-06

50124.80c 5.3720E-06

% Hf

72174.80c 3.5695E-09

72176.80c 1.1471E-07

72177.80c 4.0996E-07

72178.80c 6.0146E-07

72179.80c 3.0030E-07

72180.80c 7.7339E-07

mat air_sal sum tmp 294.0 rgb 255 160 122

6000.80c 7.5811E-09

mat air sum tmp 294.0 rgb 204 255 255

6000.80c 7.5811E-09

7014.80c 3.9484E-05

8016.80c 1.0608E-05

```
% add absorber to prevent problem with XS
mat airCR sum tmp 294.0 rgb 204 255 255
6000.80c 7.5811E-09
7014.80c 3.9484E-05
8016.80c 1.0608E-05
5010.80c 5.0000E-07
```

```
mat air_out sum tmp 294.0 rgb 0 0 128
6000.80c 7.5811E-09
7014.80c 3.9484E-05
8016.80c 1.0608E-05
```

```
mat air_Test sum tmp 294.0 rgb 245 96 197
6000.80c 7.5811E-09
7014.80c 3.9484E-05
8016.80c 1.0608E-05
```

```
mat air_hmg sum tmp 294.0 rgb 204 255 255
6000.80c 7.5811E-09
7014.80c 3.9484E-05
8016.80c 1.0608E-05
```

```
mat reflector sum tmp 294.0 moder gra_300 6000 rgb 199 199 199
5010.80c 3.517E-08
5011.80c 1.509E-07
6000.80c 4.9360E-02
6002.80c 3.4300E-02
26054.80c 1.054E-06
26056.80c 1.652E-05
26057.80c 3.818E-07
26058.80c 5.043E-08
```

```
mat graphite sum tmp 294.0 moder gra_300 6000 rgb 203 203 203
5010.80c 3.517E-08
5011.80c 1.509E-07
6000.80c 4.9360E-02
6002.80c 3.4300E-02
26054.80c 1.054E-06
26056.80c 1.652E-05
26057.80c 3.818E-07
26058.80c 5.043E-08
```

```
mat aluminum sum rgb 50 250 50 tmp 294.0 rgb 204 0 204
13027.80c 5.9477E-02
26054.80c 2.5591E-05
26056.80c 4.0136E-04
```

26057.80c 9.2739E-06
 26058.80c 1.2249E-06

mat aluminum_TF sum rgb 50 250 50 tmp 294.0 rgb 204 0 204
 13027.80c 5.9477E-02
 26054.80c 2.5591E-05
 26056.80c 4.0136E-04
 26057.80c 9.2739E-06
 26058.80c 1.2249E-06

mat aluminum_BF sum rgb 50 250 50 tmp 294.0 rgb 204 0 204
 13027.80c 5.9477E-02
 26054.80c 2.5591E-05
 26056.80c 4.0136E-04
 26057.80c 9.2739E-06
 26058.80c 1.2249E-06

%#####

% Old Control Rod 1.6 g/cc

%#####

mat b4c sum tmp 294.0 rgb 255 130 171

5010.80c 1.3881E-02

5011.80c 5.5872E-02

6000.80c 1.7438E-02

%#####

% New Control Rod 1.8 g/cc

%#####

mat b4c_new sum tmp 294.0 rgb 255 130 171

5010.80c 1.5616E-02

5011.80c 6.2854E-02

6000.80c 2.3562E-01

%#####

mat steel sum tmp 294.0 rgb 133 99 99

26054.80c 5.0819E-03

26056.80c 7.6860E-02

26057.80c 1.7447E-03

26058.80c 2.2647E-04

42092.80c 8.11748E-05

42094.80c 5.05975E-05

42095.80c 8.70824E-05

42096.80c 9.12396E-05

42097.80c 5.22385E-05

42098.80c 1.31991E-04

42100.80c 5.26761E-05

6000.80c 1.4000E-03

mat zirc2 sum tmp 294.0 rgb 160 160 160

26054.80c 5.5868E-06
 26056.80c 8.7621E-05
 26057.80c 2.0246E-06
 26058.80c 2.6740E-07
 24050.80c 3.3050E-06
 24052.80c 6.3661E-05
 24053.80c 7.2178E-06
 24054.80c 1.7931E-06
 28058.80c 2.5203E-05
 28060.80c 9.7065E-06
 28061.80c 4.2202E-07
 28062.80c 1.3438E-06
 28064.80c 3.4428E-07
 40090.80c 2.18909E-02
 40091.80c 4.77387E-03
 40092.80c 7.29696E-03
 40094.80c 7.39483E-03
 40096.80c 1.19134E-03
 50112.80c 4.68066E-06
 50114.80c 3.18478E-06
 50115.80c 1.64064E-06
 50116.80c 7.01616E-05
 50117.80c 3.70592E-05
 50118.80c 1.16872E-04
 50119.80c 4.14504E-05
 50120.80c 1.57212E-04
 50122.80c 2.23417E-05
 50124.80c 2.79392E-05
 72174.80c 3.58555E-09
 72176.80c 1.15224E-07
 72177.80c 4.11807E-07
 72178.80c 6.04165E-07
 72179.80c 3.01651E-07
 72180.80c 7.76868E-07

% mixture of aluminum and steel for all assemblies except CR

% to model steel grid and bottom fitting area

mat Al_steel sum tmp 294.0 rgb 165 165 165

6000.80c 6.956295E-04
 13027.80c 2.209049E-02
 26054.80c 2.534587E-03
 26056.80c 3.833907E-02
 26057.80c 8.703466E-04
 26058.80c 1.129828E-04

42092.80c 4.033393E-05
 42094.80c 2.514076E-05
 42095.80c 4.326928E-05
 42096.80c 4.533490E-05
 42097.80c 2.595614E-05
 42098.80c 6.558336E-05
 42100.80c 2.617357E-05
 7014.80c 5.200443E-06
 8016.80c 1.397181E-06

% mixture of aluminum and air
 % to model the top fitting area
 mat Al_air sum tmp 294.0 rgb 165 165 165
 6000.80c 4.082824E-09
 13027.80c 2.744548E-02
 26054.80c 1.180889E-05
 26056.80c 1.852064E-04
 26057.80c 4.279413E-06
 26058.80c 5.652264E-07
 7014.80c 2.126423E-05
 8016.80c 5.712970E-06

% mixture of zr-3 and steel for the Zr follower plugs
 mat zr_steel sum tmp 294.0 rgb 160 160 160
 5010.80c 9.4717E-08
 5011.80c 4.0643E-07
 6000.80c 4.3568E-04
 24050.80c 6.7988E-08
 24052.80c 1.3096E-06
 24053.80c 1.4848E-07
 24054.80c 3.6886E-08
 26054.80c 1.5895E-03
 26056.80c 2.4045E-02
 26057.80c 5.4587E-04
 26058.80c 7.0862E-05
 28058.80c 1.5707E-07
 28060.80c 6.0491E-08
 28061.80c 2.6300E-09
 28062.80c 1.5296E-08
 28064.80c 2.1455E-09
 40090.80c 1.5191E-02
 40091.80c 3.3128E-03
 40092.80c 5.0636E-03
 40094.80c 5.1315E-03
 40096.80c 8.2669E-04
 42092.80c 2.5262E-05

42094.80c 1.5746E-05
 42095.80c 2.7100E-05
 42096.80c 2.8394E-05
 42097.80c 1.6257E-05
 42098.80c 4.1076E-05
 42100.80c 1.6393E-05
 48106.80c 6.0248E-11
 48108.80c 4.2896E-11
 48110.80c 6.0200E-10
 48111.80c 6.1694E-10
 48112.80c 1.1630E-09
 48113.80c 5.8898E-10
 48114.80c 1.3848E-09
 48116.80c 3.6101E-10
 50112.80c 6.1990E-07
 50114.80c 4.2179E-07
 50115.80c 2.1728E-07
 50116.80c 9.2919E-06
 50117.80c 4.9080E-06
 50118.80c 1.5478E-05
 50119.80c 5.4896E-06
 50120.80c 2.0821E-05
 50122.80c 2.9589E-06
 50124.80c 3.7002E-06
 72174.80c 2.4587E-09
 72176.80c 7.9012E-08
 72177.80c 2.8238E-07
 72178.80c 4.1428E-07
 72179.80c 2.0685E-07
 72180.80c 5.3271E-07

% to modle the top graple in the CR

mat Air_steel sum tmp 294.0 rgb 165 162 165

6000.80c 3.249E-04
 7014.80c 3.032E-05
 8016.80c 8.146E-06
 26054.80c 1.179E-03
 26056.80c 1.783E-02
 26057.80c 4.048E-04
 26058.80c 5.255E-05
 42092.80c 1.884E-05
 42094.80c 1.174E-05
 42095.80c 2.021E-05
 42096.80c 2.117E-05
 42097.80c 1.212E-05
 42098.80c 3.063E-05

42100.80c 1.222E-05

mat lead sum tmp 294.0 rgb 100 100 100
83209.51c 3.2964E-02

mat Dy sum tmp 294.0 rgb 0 255 0
68162.80c 2.1370E-08
68164.80c 2.4614E-07
68166.80c 5.1507E-06
68167.80c 3.5159E-06
68168.80c 4.1476E-06
68170.80c 2.2923E-06
67165.80c 1.5591E-05
66156.80c 1.7705E-05
66158.80c 3.0036E-05
66160.80c 7.3636E-04
66161.80c 5.9721E-03
66162.80c 8.0544E-03
66163.80c 7.8713E-03
66164.80c 8.9349E-03

% From Connie

mat concrete sum moder lwtr 1001 moder hwtr 1002 rgb 0 102 0
20040.80c 2.5914E-03
20042.80c 1.7296E-05
20043.80c 3.6088E-06
20044.80c 5.5763E-05
20046.80c 1.0693E-07
20048.80c 4.9989E-06
14028.80c 1.5236E-03
14029.80c 7.7399E-05
14030.80c 5.1082E-05
13027.80c 1.1921E-03
26054.80c 1.0360E-03
26056.80c 1.6262E-02
26057.80c 3.7557E-04
26058.80c 4.9981E-05
12024.80c 9.5284E-04
12025.80c 1.2063E-04
12026.80c 1.3281E-04
16032.80c 4.8069E-05
16033.80c 3.7953E-07
16034.80c 2.1507E-06
16036.80c 5.0604E-09
19039.80c 2.0056E-05
19040.80c 2.5162E-09

19041.80c 1.4474E-06
 11023.80c 3.2685E-05
 25055.80c 2.8557E-05
 23050.80c 4.0548E-08
 23051.80c 1.6178E-05
 24050.80c 1.1582E-07
 24052.80c 2.2335E-06
 24053.80c 2.5326E-07
 24054.80c 6.3043E-08
 22046.80c 5.9935E-05
 22047.80c 5.4050E-05
 22048.80c 5.3556E-04
 22049.80c 3.9303E-05
 22050.80c 3.7632E-05
 8016.80c 4.7228E-02
 8017.80c 1.7953E-05
 1001.80c 2.3634E-02
 1002.80c 2.7182E-06
 % Total 9.6208E-02

% new homogenized mixtures for CR
 mat HS1 sum tmp 294.0 rgb 165 162 165

24050.80c 1.928821E-08
 24052.80c 3.715340E-07
 24053.80c 4.212344E-08
 24054.80c 1.046452E-08
 26054.80c 4.091111E-03
 26056.80c 6.187640E-02
 26057.80c 1.404592E-03
 26058.80c 1.823241E-04
 28058.80c 4.456035E-08
 28060.80c 1.716126E-08
 28061.80c 7.461334E-10
 28062.80c 4.339481E-09
 28064.80c 6.086809E-10
 40090.80c 4.309655E-03
 40091.80c 9.398372E-04
 40092.80c 1.436537E-03
 40094.80c 1.455802E-03
 40096.80c 2.345321E-04
 42092.80c 6.531234E-05
 42094.80c 4.071015E-05
 42095.80c 7.006544E-05
 42096.80c 7.341033E-05
 42097.80c 4.203054E-05
 42098.80c 1.061984E-04

42100.80c 4.238259E-05
 48106.80c 1.709231E-11
 48108.80c 1.216960E-11
 48110.80c 1.707867E-10
 48111.80c 1.750252E-10
 48112.80c 3.299460E-10
 48113.80c 1.670931E-10
 48114.80c 3.928631E-10
 48116.80c 1.024180E-10
 5010.80c 2.687113E-08
 5011.80c 1.153042E-07
 50112.80c 1.758651E-07
 50114.80c 1.196612E-07
 50115.80c 6.164236E-08
 50116.80c 2.636106E-06
 50117.80c 1.392400E-06
 50118.80c 4.391099E-06
 50119.80c 1.557395E-06
 50120.80c 5.906906E-06
 50122.80c 8.394355E-07
 50124.80c 1.049747E-06
 6000.80c 1.126423E-03
 72174.80c 6.975285E-10
 72176.80c 2.241567E-08
 72177.80c 8.011103E-08
 72178.80c 1.175315E-07
 72179.80c 5.868286E-08
 72180.80c 1.511295E-07

mat HS2 sum tmp 294.0 rgb 165 162 165

24050.80c 4.666503E-08
 24052.80c 8.988726E-07
 24053.80c 1.019115E-07
 24054.80c 2.531739E-08
 26054.80c 2.684829E-03
 26056.80c 4.060936E-02
 26057.80c 9.218580E-04
 26058.80c 1.196654E-04
 28058.80c 1.078073E-07
 28060.80c 4.151918E-08
 28061.80c 1.805161E-09
 28062.80c 1.049874E-08
 28064.80c 1.472615E-09
 40090.80c 1.042658E-02
 40091.80c 2.273800E-03
 40092.80c 3.475493E-03

40094.80c 3.522101E-03
 40096.80c 5.674163E-04
 42092.80c 4.279789E-05
 42094.80c 2.667649E-05
 42095.80c 4.591234E-05
 42096.80c 4.810427E-05
 42097.80c 2.754182E-05
 42098.80c 6.958966E-05
 42100.80c 2.777245E-05
 48106.80c 4.135236E-11
 48108.80c 2.944258E-11
 48110.80c 4.131936E-10
 48111.80c 4.234480E-10
 48112.80c 7.982564E-10
 48113.80c 4.042575E-10
 48114.80c 9.504753E-10
 48116.80c 2.477854E-10
 5010.80c 6.501080E-08
 5011.80c 2.789618E-07
 50112.80c 4.254800E-07
 50114.80c 2.895028E-07
 50115.80c 1.491347E-07
 50116.80c 6.377676E-06
 50117.80c 3.368710E-06
 50118.80c 1.062363E-05
 50119.80c 3.767891E-06
 50120.80c 1.429090E-05
 50122.80c 2.030892E-06
 50124.80c 2.539711E-06
 6000.80c 7.381206E-04
 72174.80c 1.687569E-09
 72176.80c 5.423145E-08
 72177.80c 1.938170E-07
 72178.80c 2.843503E-07
 72179.80c 1.419747E-07
 72180.80c 3.656359E-07

mat HS3 sum tmp 294.0 rgb 165 162 165

26054.80c 2.82689E-03
 26056.80c 4.27538E-02
 26057.80c 9.70536E-04
 26058.80c 1.25983E-04
 42092.80c 4.51591E-05
 42094.80c 2.81465E-05
 42095.80c 4.84450E-05
 42096.80c 5.07549E-05

```

42097.80c 2.90589E-05
42098.80c 7.34269E-05
42100.80c 2.93015E-05
6000.80c 7.78831E-04

```

```

% s alpha betas
therm lwtr lwtr.10t
therm hwtr hwtr.10t

```

```

therm gra_300 grph.10t
therm gra_350 350.0 grph.10t grph.11t
therm gra_400 grph.11t
therm gra_450 450.0 grph.11t grph.12t
therm gra_500 grph.12t
therm gra_550 550.0 grph.12t grph.13t
therm gra_600 grph.13t
therm gra_650 650.0 grph.13t grph.14t

```

mat.sss (modifications done for M8CAL 1.5% run)

```

% -- Michigan fuel
mat fuel sum tmp 294.0 moder gra_300 6000 rgb 238 59 59
6000.80c 5.1039E-02
6002.80c 3.5468E-02
5010.80c 1.9240E-07
5011.80c 8.8524E-07
8016.80c 1.8685E-05
23050.80c 1.5339E-09
23051.80c 6.1201E-07
26054.80c 2.9114E-07
26056.80c 4.5703E-06
26057.80c 1.0555E-07
26058.80c 1.4047E-08
92234.80c 8.5472E-08
92235.80c 8.7202E-06
92236.80c 4.0790E-08
92238.80c 4.9986E-07

```

A0.sss

```

% TREAT std assembly, HEU fuel
% Model for cross section preparation
%
% Combines most homogenization models:
% - Full no channels
% - Full w channels
%

```

% Javier Ortensi
 % Idaho National Laboratory
 % August 18 2015
 %
 % Modified: 20 Jan 2015 by Ben Baker
 % -Changed the total length of the graphite in the bottom of the core to be 19.5625inch = $([14 - 3/8] + [8 - 11/16] - [3 - 1/2])$ inch
 % I had to modify most of the pz locates.
 % -Extended the off gas hole in the graphite to (8-11/16 inch) which is all the way through the square and the oct graphite piece.
 % -Modified surfaces 7,8, and 9 to reflect changes in heights because of the graphite change.
 % And I saw the Al off-gas shell had a 3/8 inch inside diameter when it was the outside. The lengths were kept the same.
 %
 % Modified: 25 Jan 2015 by Ben Baker
 % - Changed the model to do only a homogenized and homogenized with air channels models

%%
 % for cross section preparation we have the following regions
 %%%
 % universe material
 % 11001 Steel Grid Plate + Aluminum bottom fitting
 % 11013 Al top fitting
 %
 % full homogenization universes (not including air channel)
 %
 % 11030 Oct graphite XS region 1 + air gap + Al clad - bot
 % 11031 Oct graphite XS region 2 + air gap + Al clad - bot
 % 11032 square graphite + air gap + Al clad - bot
 % 11033 axial interface
 % 11034 Fuel XS region 1 + air gap + Zr clad
 % 11035 Fuel XS region 2 + air gap + Zr clad
 % 11036 Fuel XS region 3 + air gap + Zr clad
 % 11037 axial interface
 % 11038 square graphite w hole + Oct graphite with hole + air + Al clad - top
 % 11039 Oct graphite XS region 2 + air gap + Al clad - top
 % 11040 Oct graphite XS region 1 + air gap + Al clad - top
 %
 % full homogenization universes (with air channel)
 %
 % 11001 Oct graphite XS region 1 + air gap + Al clad + air channel - bot
 % 11002 Oct graphite XS region 2 + air gap + Al clad + air chan31nel - bot

```

% 11003    square graphite + air gap + Al clad + air channel - bot
% 11004    axial interface + air channel - bot
% 11005    Fuel XS region 1 + air gap + Zr clad + air channel
% 11006    Fuel XS region 2 + air gap + Zr clad + air channel
% 11007    Fuel XS region 3 + air gap + Zr clad + air channel
% 11008    axial interface + air channel - top
% 11009    square graphite w hole + Oct graphite with hole + air + Al clad + air channel -
top
% 11010    Oct graphite XS region 2 + air gap + Al clad + air channel - top
% 11011    Oct graphite XS region 1 + air gap + Al clad + air channel - top
%#####
##
%#####
##
% Reserve
% Universe [11000-11013, 11030-11040] [Final 11000]
% Cells [11000-11077]
% Surf [1-27]
%#####
##
%#####
##
% Full homogenization with air channel separated
%#####
##
%#####
##
% Reflector Oct graphite XS region 1
cell 11000 11030 reflector -4 % graphite
cell 11001 11030 air -5 4 % air gap
cell 11002 11030 aluminum -90 5 % INF Al clad
%%%%%%%%%
% Reflector Oct graphite XS region 2
cell 11003 11031 reflector -4 % graphite
cell 11004 11031 air -5 4 % air gap
cell 11005 11031 aluminum -90 5 % INF Al clad
%%%%%%%%%
% Bottom reflector square graphite XS region
cell 11006 11032 reflector -6 % graphite
cell 11007 11032 air -5 6 % air gap
cell 11008 11032 aluminum -90 5 % INF Al clad
%%%%%%%%%
% Zr and Air in spacers + Al clad before axial interface
cell 11009 11033 aluminum -90 -15 % Al cap before axial interface
cell 11010 11033 air -2 15 -16 % air in Zr spacer region axially --bottom
cell 11011 11033 zr -2 16 % Zr

```



```

%#####
##
% Full homogenization with homogenized channels
%#####
##
%#####
##

%%%%%%%%%
% steel grid plate + bottom fitting
cell 11041 11001 Al_steel -90 % steel grid + partial Al fitting
%%%%%%%%%
% Reflector Oct graphite XS region 1
cell 11042 11002 fill 11030 -3 % graphite + air gap + clad
cell 11043 11002 air_out 3 % air out
%%%%%%%%%
% Reflector Oct graphite XS region 2
cell 11044 11003 fill 11031 -3 % graphite + air gap + clad
cell 11045 11003 air_out 3 % air out
%%%%%%%%%
% Bottom reflector square graphite XS region
cell 11046 11004 fill 11032 -3 % graphite + air gap + clad
cell 11047 11004 air_out 3 % air out
%%%%%%%%%
% Axial interface
cell 11048 11005 fill 11033 -3 % AI
cell 11049 11005 air_out 3 % air out
%%%%%%%%%
% Fuel region 1
cell 11050 11006 fill 11034 -3 % fuel1 + air gap + clad
cell 11051 11006 air_out 3 % air out
%%%%%%%%%
% Fuel region 2
cell 11052 11007 fill 11035 -3 % fuel 2 + air gap + clad
cell 11053 11007 air_out 3 % air out
%%%%%%%%%
% Fuel region 3
cell 11054 11008 fill 11036 -3 % fuel 3 + air gap + clad
cell 11055 11008 air_out 3 % air out
%%%%%%%%%
% Axial interface
cell 11056 11009 fill 11037 -3 % AI
cell 11057 11009 air_out 3 % air out
%%%%%%%%%
% Top reflector square graphite XS region
cell 11058 11010 fill 11038 -3 % top sq graphite + air gap + clad

```

```

cell 11059 11010 air_out    3    % air out
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%   Reflector Oct graphite XS region 2
cell 11060 11011 fill 11039  -3    % graphite + air gap + clad
cell 11061 11011 air_out    3    % air out
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%   Reflector Oct graphite XS region 1
cell 11062 11012 fill 11040  -3    % graphite + air gap + clad
cell 11063 11012 air_out    3    % air out
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%   Al top fitting
cell 11064 11013 Al_air    -90    % Al at top end cap up to fuel surface
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

%#####
##
%#####
##
% Build std assembly
%#####
##
%#####
##
%%% start at bottom then from the center out
%%cell 11065 11000 fill 11001    -11 % Steel Grid Plate + Aluminum bottom fitting
%%cell 11066 11000 fill 11002    11 -12 % Oct graphite XS region 1 -- bottom
%%cell 11067 11000 fill 11003    12 -13 % Oct graphite XS region 2 -- bottom
%%cell 11068 11000 fill 11004    13 -14 % square graphite bottom + air gap + Al clad
%%cell 11069 11000 fill 11005    14 -17 % axial interface
%%cell 11070 11000 fill 11006    17 -18 % Fuel1 bottom
%%cell 11071 11000 fill 11007    18 -19 % Fuel2
%%cell 11072 11000 fill 11008    19 -20 % Fuel1 top
%%cell 11073 11000 fill 11009    20 -23 % aixal interface
%%cell 11074 11000 fill 11010    23 -25 % square graphite w hole top + Oct graphite with
hole + air + Al clad
%%cell 11075 11000 fill 11011    25 -26 % Oct graphite XS region 2 -- top
%%cell 11076 11000 fill 11012    26 -27 % Oct graphite XS region 1 -- top
%%cell 11077 11000 fill 11013    27    % top fitting

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Debug Assembly
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%
%include "/Users/bakeba/Desktop/HPC-Serpent/Assemblies/DebugAssembly.i"
%cell 3 1 fill 11000 -5900
%
%----- Geometry and mesh plots:
%plot 3 1000 1000 1.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 5.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 31.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 54.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 62.1 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 62.3 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 62.6 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 70.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 90.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 170.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 183.9 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 184.2 -5.08 5.08 -5.08 5.08 % xy-plot %21
%plot 3 1000 1000 184.5 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 185.0 -5.08 5.08 -5.08 5.08 % xy-plot above al plat (al hole and
pin)
%plot 3 1000 1000 190.4 -5.08 5.08 -5.08 5.08 % xy-plot (Inside pin clad)
%plot 3 1000 1000 191.0 -5.08 5.08 -5.08 5.08 % xy-plot (square + air, no pin)
%plot 3 1000 1000 194.0 -5.08 5.08 -5.08 5.08 % xy-plot (hex + air hole)
%plot 3 1000 1000 207.0 -5.08 5.08 -5.08 5.08 % xy-plot (hex + no hole)
%plot 3 1000 1000 222.0 -5.08 5.08 -5.08 5.08 % xy-plot (hex + no hole)
%plot 3 1000 1000 249.0 -5.08 5.08 -5.08 5.08 % xy-plot (hex + no hole)
%
%plot 2 800 4000 0.0 -5.08 5.08 -3.0 260.65 % xz-plot
%
%plot 1 800 4000 -5.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 -4.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 -3.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 -2.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 -1.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 0.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 1.0 -5.08 5.08 0.0 247.65 % yz-plot

```

```
%plot 1 800 4000 2.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 3.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 4.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 5.0 -5.08 5.08 0.0 247.65 % yz-plot
```

B0.sss

```
% TREAT CR assembly, HEU fuel -- OLD SHORT ROD
```

```
% Model for cross section preparation
```

```
%
```

```
%
```

```
%
```

```
%
```

```
% Ben Baker derived from Javi Ortensi's model
```

```
% Feb 11, 2016
```

```
%%%%%%%%%%%
```

```
%%%%%%%%%%%
```

```
% for cross section preparation we have the following regions
```

```
%%%%%%%%%%%
```

```
%%%%%%%%%%%
```

```
% universe material
```

```
% 1001 Steel Grid Plate + Aluminum bottom fitting
```

```
% 1013 Al top fitting
```

```
%
```

```
% full homogenization universes (not including air channel)
```

```
%
```

```
% 1030 Oct graphite XS region 1 + air gap + Al clad - bot
```

```
% 1031 Oct graphite XS region 2 + air gap + Al clad - bot
```

```
% 1032 square graphite + air gap + Al clad - bot
```

```
% 1033 axial interface
```

```
% 1034 Fuel XS region 1 + air gap + Zr clad
```

```
% 1035 Fuel XS region 2 + air gap + Zr clad
```

```
% 1036 Fuel XS region 3 + air gap + Zr clad
```

```
% 1037 axial interface
```

```
% 1038 square graphite w hole + Oct graphite with hole + air + Al clad - top
```

```
% 1039 Oct graphite XS region 2 + air gap + Al clad - top
```

```
% 1040 Oct graphite XS region 1 + air gap + Al clad - top
```

```
%
```

```
% full homogenization universes (with air channel)
```

```
%
```

```
% 1001 Oct graphite XS region 1 + air gap + Al clad + air channel - bot
```

```
% 1002 Oct graphite XS region 2 + air gap + Al clad + air channel - bot
```

```
% 1003 square graphite + air gap + Al clad + air channel - bot
```

```
% 1004 axial interface + air channel - bot
```

```
% 1005 Fuel XS region 1 + air gap + Zr clad + air channel
```

```
% 1006 Fuel XS region 2 + air gap + Zr clad + air channel
```

```

% 1007    Fuel XS region 3 + air gap + Zr clad + air channel
% 1008    axial interface + air channel - top
% 1009    square graphite w hole + Oct graphite with hole + air + Al clad + air channel - top
% 1010    Oct graphite XS region 2 + air gap + Al clad + air channel - top
% 1011    Oct graphite XS region 1 + air gap + Al clad + air channel - top
%#####
##
%#####
##
% Reserve
% Universe [1000-1013, 1030-1040] [Final 1000]
% Cells [900-944,1000-1083]
% Surf [10,28, 48-61, 65, 77-79]
%#####
##
%
%#####
##
% Bottom long lower graphite plug
cell 1000 1030 air -52 % air gap between CR and Zirc2 tube
      **(Removed Surf 51)**
cell 1001 1030 zirc2 -53 52 % Zirc2 tubing
cell 1002 1030 air -55 53 % air gap between Zirc2 tube and Bottom Oct Plug
cell 1003 1030 reflector -4 55 % Oct graphite long lower plug
cell 1004 1030 air -5 4 % air gap between graphite and clad
cell 1005 1030 aluminum -90 5 % aluminum clad
%%%%%%%%%%
%%%%%%%%%%
%%%%%%%%%%
%%%%%%%%%%
% Bottom short lower graphite plug - Oct region
cell 1006 1031 air -52 % air gap between CR and Zirc2 tube
      **(Removed Surf 51)**
cell 1007 1031 zirc2 -53 52 % Zirc2 tubing
cell 1008 1031 air -55 53 % air gap between Zirc2 tube and Bottom Oct Plug
cell 1009 1031 reflector -4 55 % Oct graphite long lower plug
cell 1010 1031 air -5 4 % air gap between graphite and clad
cell 1011 1031 aluminum -90 5 % aluminum clad
%%%%%%%%%%
%%%%%%%%%%
%%%%%%%%%%
%%%%%%%%%%
% Square graphite Bottom
cell 1012 1032 air -52 % air gap between CR and Zirc2 tube
      **(Removed Surf 51)**
cell 1013 1032 zirc2 -53 52 % Zirc2 tubing

```

cell 1014 1032 air -55 53 % air gap between Zirc2 tube and Bottom square graphite
 cell 1015 1032 reflector -6 55 % Square graphite bottom
 cell 1016 1032 air -5 6 % air gap between graphite and clad
 cell 1017 1032 aluminum -90 5 % aluminum clad
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 % Bottom Axial Interface
 cell 1018 1033 air -52 % air gap between CR and Zirc2 tube **(Removed Surf 51)**
 cell 1019 1033 zirc2 -53 52 % Zirc2 tubing
 % Al clad before axial interface
 % Pz
 cell 1020 1033 air -55 53 -15 % Air gap between CR tube and aluminum cap
 cell 1021 1033 aluminum 55 -15 % Aluminum cap
 % Zr clad
 cell 1022 1033 air -2 53 15 -16 % Air gap between CR tube and Zr clad
 cell 1023 1033 zr 2 15 -16 % Zr clad
 %
 cell 1024 1033 air -56 53 16 % Air gap between CR tube and Zr bacon strips
 cell 1025 1033 zr 56 16 % Zr bacon strip until clad
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 % Fuel Region 1
 cell 1026 1034 air -52 % air gap between CR and Zirc2 tube **(Removed Surf 51)**
 cell 1027 1034 zirc2 -53 52 % Zirc2 tubing
 cell 1028 1034 air -57 53 % air gap between zirc2 tube and fuel
 cell 1029 1034 fuel -1 57 % fuel
 cell 1030 1034 air -2 1 % air gap between fuel and clad
 cell 1031 1034 zr -90 2 % zr clad
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 % Fuel Region 2
 cell 1032 1035 air -52 % air gap between CR and Zirc2 tube **(Removed Surf 51)**
 cell 1033 1035 zirc2 -53 52 % Zirc2 tubing
 cell 1034 1035 air -57 53 % air gap between zirc2 tube and fuel
 cell 1035 1035 fuel -1 57 % fuel
 cell 1036 1035 air -2 1 % air gap between fuel and clad
 cell 1037 1035 zr -90 2 % zr clad

%%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%

% Fuel Region 3

cell 1038 1036 air -52 % air gap between CR and Zirc2 tube **(Removed Surf 51)**

cell 1039 1036 zirc2 -53 52 % Zirc2 tubing

cell 1040 1036 air -57 53 % air gap between zirc2 tube and fuel

cell 1041 1036 fuel -1 57 % fuel

cell 1042 1036 air -2 1 % air gap between fuel and clad

cell 1043 1036 zr -90 2 % zr clad

%%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%

% Top axial interface region

cell 1044 1037 air -52 % air gap between CR and Zirc2 tubing **(Removed Surf 51)**

cell 1045 1037 zirc2 -53 52 % Zirc2 tubing -- bottom ref

% Zr clad and bacon strips - before axial interface

cell 1046 1037 air -56 53 -21 % air between CR tube and Zr bacon strips

cell 1047 1037 zr 56 -21 % Zr bacon strips until clad top

% Zr clad and air

cell 1048 1037 air 53 -2 21 -22 % air between CR tube and zr clad

cell 1049 1037 zr 2 21 -22 % side Zr clad

% hole for outgas tube

cell 1050 1037 air -77 22 % hole Al clad top

% Al clad - after axial interface

cell 1051 1037 air -55 53 22 % air between Zirc2 clad and Al clad cap

cell 1052 1037 aluminum 55 77 22 % Al clad cap

%%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%

% Square graphite and oct Top

cell 1053 1038 air -52 -24 % air gap between CR and Zirc2 tube stop at end of square **(Removed Surf 51)**

cell 1054 1038 zirc2 -53 52 -24 % Zirc2 tubing stop at top of square graphite

% hole for outgas

cell 1055 1038 air -77 % Inside off gas tube

cell 1056 1038 aluminum -78 77 % aluminum off gas tube

cell 1057 1038 air -79 78 % air outside of Al tube upto graphite

% Square graphite

cell 1058 1038 air -54 53 -24 % air gap between Al and zirc2 tube

cell 1059 1038 aluminum -58 54 -24 % aluminum after zirc2 tube

cell 1060 1038 air -60 58 -24 % air gap between Al and graphite
 cell 1061 1038 reflector 60 79 -6 -24 % square graphite minus off gas hole and center hole
 cell 1062 1038 air -5 6 -24 % air up to Al clad
 % Oct-region Added 61 for bushing I.D.
 % bushing region until aluminum
 cell 1063 1038 air -61 24 -28 % air gap between CR clad and graphite bushing
 (Removed Surf 51)
 cell 1064 1038 reflector -54 61 24 -28 % graphite bushing
 % all other in Oct-region
 cell 1065 1038 air -52 28 % air between CR clad and aluminum tube above
 bushing **(Removed Surf 51)**
 cell 1066 1038 aluminum -54 52 28 % aluminum tube after gap and until aluminum
 tube where bushing ends radially
 cell 1067 1038 aluminum -59 54 24 % aluminum after bushing radially
 cell 1068 1038 air -60 59 24 % air gap between aluminum tube and graphite oct
 cell 1069 1038 reflector 60 79 -4 24 % Oct-reflector minus CR hole and Off-gas hole
 cell 1070 1038 air -5 4 24 % air gap up to aluminum clad
 % Cladding
 cell 1071 1038 aluminum -90 5 % aluminum clad
 %%%%%%%%%%%
 %%%%%%%%%%%
 %%%%%%%%%%%
 %%%%%%%%%%%
 % Short upper graphite plug - Oct region (No OFF-Gas hole)
 cell 1072 1039 air -52 % air gap between CR and Zirc2 tube
 (Removed Surf 51)
 cell 1073 1039 aluminum -59 52 % Aluminum bearing tube
 cell 1074 1039 air -60 59 % air gap between Al bearing tube and Oct Plug
 cell 1075 1039 reflector -4 60 % Oct graphite long lower plug
 cell 1076 1039 air -5 4 % air gap between graphite and clad
 cell 1077 1039 aluminum -90 5 % aluminum clad
 %%%%%%%%%%%
 %%%%%%%%%%%
 %%%%%%%%%%%
 %%%%%%%%%%%
 % Short upper graphite plug - Oct region (No OFF-Gas hole)
 cell 1078 1040 air -52 % air gap between CR and Zirc2 tube
 (Removed Surf 51)
 cell 1079 1040 aluminum -59 52 % Aluminum bearing tube
 cell 1080 1040 air -60 59 % air gap between Al bearing tube and Oct Plug
 cell 1081 1040 reflector -4 60 % Oct graphite long lower plug
 cell 1082 1040 air -5 4 % air gap between graphite and clad
 cell 1083 1040 aluminum -90 5 % aluminum clad
 %%%%%%%%%%%
 %%%%%%%%%%%

%%%%%%%%%
 %%%%%%%%%

%%%%%%%%%
 %%%%%%%%%

% full homogenization universes (w air channel)

%%%%%%%%%
 %%%%%%%%%

% Steel Grid Plate + Aluminum base (Bottom)

cell 900 1001 air -52 % air between CR clad and Zirc2 tubing -- bottom ref

** (Removed Surf 51) **

cell 901 1001 zirc2 -53 52 % Zirc2 tubing -- bottom ref

cell 902 1001 air -55 53 % air between zirc2 and core grid & aluminum base

cell 903 1001 steel 55 -10 % steel grid

cell 904 1001 aluminum 55 -3 10 % Al base

cell 905 1001 air_out 3 10 % air around base

%%%%%%%%%

% Oct graphite XS region 1 + air gap + Al clad - bot

cell 906 1002 fill 1030 -3 % graphite

cell 907 1002 air_out 3 % air channel

%%%%%%%%%

% Oct graphite XS region 2 + air gap + Al clad - bot

cell 908 1003 fill 1031 -3 % air gap before Al clad

cell 909 1003 air_out 3 % air channel

%%%%%%%%%

% square graphite + air gap + Al clad - bot

cell 910 1004 fill 1032 -3 % air gap before Al clad

cell 911 1004 air_out 3 % air channel

%%%%%%%%%

% Axial Interface Bottom

cell 912 1005 fill 1033 -3 % air outside fuel region

cell 913 1005 air_out 3 % air channel

%%%%%%%%%

% Fuel XS region 1 + air gap + Zr clad

cell 914 1006 fill 1034 -3 % air outside fuel region

cell 915 1006 air_out 3 % air channel

%%%%%%%%%

% Fuel XS region 2 + air gap + Zr clad

cell 916 1007 fill 1035 -3 % air outside fuel region

cell 917 1007 air_out 3 % air channel

%%%%%%%%%

% Fuel XS region 3 + air gap + Zr clad

```

cell 918 1008 fill 1036    -3      % air outside fuel region
cell 919 1008 air_out      3      % air channel
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% AI
cell 920 1009 fill 1037    -3      % air outside fuel region
cell 921 1009 air_out      3      % air channel
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% square graphite w hole + Oct graphite with hole + air + Al clad - top
cell 922 1010 fill 1038    -3      % air gap before Al clad
cell 923 1010 air_out      3      % air channel
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Oct graphite XS region 2 + air gap + Al clad - top
cell 924 1011 fill 1039    -3      % air gap before Al clad
cell 925 1011 air_out      3      % air channel
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Oct graphite XS region 1 + air gap + Al clad - top
cell 926 1012 fill 1040    -3      % air gap before Al clad
cell 927 1012 air_out      3      % air channel
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%   Al top fitting
cell 928 1013 air          -52      % air between CR clad and Al tubing -- top oct region
      **(Removed Surf 51)**
cell 929 1013 aluminum     -59  52   % Al tubing -- top oct region
cell 930 1013 air          -60  59   % air after Al tubing -- top ref
cell 931 1013 aluminum      60      % Al top fitting

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Build CR assembly
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% start at bottom of assembly with regions outside CR
%%cell 932 1000 fill 1001    -11   % Steel Grid Plate + Aluminum bottom fitting
%%cell 933 1000 fill 1002    11 -12 % Oct graphite XS region 1 -- bot
%%cell 934 1000 fill 1003    12 -13 % Oct graphite XS region 2 -- bot
%%cell 935 1000 fill 1004    13 -14 % square graphite bottom + air gap + Al clad - bot
%%cell 936 1000 fill 1005    14 -17 % axial interface - bot
%%cell 937 1000 fill 1006    17 -18 % Fuel1
%%cell 938 1000 fill 1007    18 -19 % Fuel2
%%cell 939 1000 fill 1008    19 -20 % Fuel3
%%cell 940 1000 fill 1009    20 -23 % axial interface - top
%%cell 941 1000 fill 1010    23 -25 % square graphite w hole top + Oct graphite with hole -
top
%%cell 942 1000 fill 1011    25 -26 % Oct graphite XS region 2 -- top

```

```
%%cell 943 1000 fill 1012    26 -27 % Oct graphite XS region 1 -- top
%%cell 944 1000 fill 1013    27    % top Al fitting
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
% Debug Assembly
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
%
```

```
%include "/Users/bakeba/Desktop/HPC-Serpent/Assemblies/DebugAssembly.i"
```

```
%cell 3 1 fill 1000 -5900
```

```
%
```

```
%%%%%%%%% --- Geometry and mesh plots:
```

```
%plot 2 800 4000 0.0 -5.08 5.08 -160.0 250.00 % xz-plot
```

```
%plot 1 800 4000 0.0 -5.08 5.08 -160.0 250.00 % yz-plot
```

```
%
```

```
%plot 3 1000 1000 1.0 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 5.0 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 31.0 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 54.0 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 62.1 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 62.3 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 62.6 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 70.0 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 90.0 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 170.0 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 183.9 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 184.2 -5.08 5.08 -5.08 5.08 % xy-plot %21
```

```
%plot 3 1000 1000 184.5 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 185.0 -5.08 5.08 -5.08 5.08 % xy-plot square w/ everything
```

```
%plot 3 1000 1000 193.5 -5.08 5.08 -5.08 5.08 % xy-plot oct w/ everything
```

```
%plot 3 1000 1000 194.7 -5.08 5.08 -5.08 5.08 % xy-plot oct in-between Al off-gas
tube
```

```
%plot 3 1000 1000 194.8 -5.08 5.08 -5.08 5.08 % xy-plot oct w/o Al off-gas
```

```
%plot 3 1000 1000 195.1 -5.08 5.08 -5.08 5.08 % xy-plot oct No off-gas
```

```
%plot 3 1000 1000 198.6 -5.08 5.08 -5.08 5.08 % xy-plot oct No Bushing
```

```
%plot 3 1000 1000 207.0 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 222.0 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 3 1000 1000 249.0 -5.08 5.08 -5.08 5.08 % xy-plot
```

```
%plot 1 800 4000 -5.0 -5.08 5.08 0.0 247.65 % yz-plot
```

```
%plot 1 800 4000 -4.0 -5.08 5.08 0.0 247.65 % yz-plot
```

```
%plot 1 800 4000 -3.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 -2.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 -1.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 0.0 -5.08 5.08 -160.0 247.65 % yz-plot
%plot 1 800 4000 1.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 2.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 3.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 4.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 1 800 4000 5.0 -5.08 5.08 0.0 247.65 % yz-plot
```

CR-Type.sss

```
%#####
##
% Reserve
% Universe [C/S = 800, Comp = 801, Trans. = 802]
% Cells [800-853]
% Surf [50, 851-863, 871-883]
%#####
##

%#####
##
% CONTROL ROD REGIONS (Control/Shutdown Rods)
%#####
##
% Dynamic Control Rod
cell 800 800 steel -50 -851 % Bottom Adaptor - Control Rod Follower
cell 801 800 graphite -50 851 -852 % Graphite - Control Rod Follower
cell 802 800 steel -50 852 -853 % Steel plug - Control Rod Follower
cell 803 800 zr_steel -50 853 -854 % Zr/Steel plug - Control Rod Follower
cell 804 800 graphite -50 854 -855 % Graphite - Upper follower
cell 805 800 steel -50 855 -856 % Steel plug - Upper follower
cell 806 800 zr_steel -50 856 -857 % Zr/Steel plug - Zr follower
cell 807 800 graphite -50 857 -858 % Graphite - Zr follower
cell 808 800 zr_steel -50 858 -859 % Zr/Steel plug - Zr follower
cell 809 800 steel -50 859 -860 % Steel plug - poison section
cell 810 800 b4c_new -50 860 -861 % B4C - poison section
cell 811 800 steel -50 861 -862 % steel plug | grapple adaptor

cell 812 800 steel 50 -856 % lower carbon steel clad
cell 813 800 zr 50 856 -859 % zirc-3 clad (zirc follower)
cell 814 800 steel 50 859 -861 % upper carbon steel clad
cell 815 800 steel 50 861 -862 % steel plug | grapple adaptor
cell 816 800 Air_steel 862 -863 % grapple and air
cell 817 800 air 863 % air above CR
```

```
%#####
##
```

```
%#####
##
```

```
% CONTROL ROD REGIONS (Compensation Rods)
```

```
%#####
##
```

```
% Dynamic Control Rod
```

```
cell 818 801 steel    -50      -851    % Bottom Adaptor - Control Rod Follower
cell 819 801 graphite -50    851 -852    % Graphite    - Control Rod Follower
cell 820 801 steel    -50    852 -853    % Steel plug   - Control Rod Follower
cell 821 801 zr_steel -50    853 -854    % Zr/Steel plug - Control Rod Follower
cell 822 801 graphite -50    854 -855    % Graphite    - Upper follower
cell 823 801 steel    -50    855 -856    % Steel plug   - Upper follower
cell 824 801 zr_steel -50    856 -857    % Zr/Steel plug - Zr follower
cell 825 801 graphite -50    857 -858    % Graphite    - Zr follower
cell 826 801 zr_steel -50    858 -859    % Zr/Steel plug - Zr follower
cell 827 801 steel    -50    859 -860    % Steel plug   - poison section
cell 828 801 b4c_new  -50    860 -861    % B4C         - poison section
cell 829 801 steel    -50    861 -862    % steel plug | grapple adaptor
```

```
cell 830 801 steel    50      -856    % lower carbon steel clad
cell 831 801 zr       50    856 -859    % zirc-3 clad (zirc follower)
cell 832 801 steel    50    859 -861    % upper carbon steel clad
cell 833 801 steel    50    861 -862    % steel plug | grapple adaptor
cell 834 801 Air_steel      862 -863    % grapple and air
cell 835 801 air       863          % air above CR
```

```
%#####
##
```

```
%#####
##
```

```
% CONTROL ROD REGIONS (Transient Rods)
```

```
%#####
##
```

```
% Dynamic Control Rod
```

```
cell 836 802 steel    -50      -871    % Bottom Adaptor - Control Rod Follower
cell 837 802 graphite -50    871 -872    % Graphite    - Control Rod Follower
cell 838 802 steel    -50    872 -873    % Steel plug   - Control Rod Follower
cell 839 802 zr_steel -50    873 -874    % Zr/Steel plug - Control Rod Follower
cell 840 802 graphite -50    874 -875    % Graphite    - Upper follower
```

```

cell 841 802 steel      -50  875 -876  % Steel plug  - Upper follower
cell 842 802 zr_steel  -50  876 -877  % Zr/Steel plug - Zr follower
cell 843 802 graphite  -50  877 -878  % Graphite    - Zr follower
cell 844 802 zr_steel  -50  878 -879  % Zr/Steel plug - Zr follower
cell 845 802 steel     -50  879 -880  % Steel plug   - poison section
cell 846 802 b4c_new   -50  880 -881  % B4C          - poison section
cell 847 802 steel     -50  881 -882  % steel plug | grapple adaptor

```

```

cell 848 802 steel     50      -876  % lower carbon steel clad
cell 849 802 zr        50  876 -879  % zirc-3 clad (zirc follower)
cell 850 802 steel     50  879 -881  % upper carbon steel clad
cell 851 802 steel     50  881 -882  % steel plug | grapple adaptor
cell 852 802 Air_steel      882 -883  % grapple and air
cell 853 802 air        883          % air above CR

```

```

%#####
##

```

```

%%%#####
#####

```

%%% OLD CONTROL ROD REGIONS (Old Rods-MinCritical)

```

%%%#####
#####

```

%%% Dynamic Control Rod

```

%%cell 854 803 steel    -50      -891  % Bottom Adaptor - Control Rod Follower
%%cell 855 803 graphite -50  891 -892  % Graphite      - Control Rod Follower
%%cell 856 803 steel    -50  892 -893  % Steel plug    - Control Rod Follower
%%cell 857 803 zr_steel -50  893 -894  % Zr/Steel plug - Control Rod Follower
%%cell 858 803 graphite -50  894 -895  % Graphite      - Upper follower
%%cell 859 803 steel    -50  895 -896  % Steel plug    - Upper follower
%%cell 860 803 zr_steel -50  896 -897  % Zr/Steel plug - Zr follower
%%cell 861 803 graphite -50  897 -898  % Graphite      - Zr follower
%%cell 862 803 zr_steel -50  898 -899  % Zr/Steel plug - Zr follower
%%cell 863 803 steel    -50  899 -900  % Steel plug    - poison section
%%cell 864 803 b4c      -50  900 -901
%%cell 865 803 b4c      -50  901 -902  % B4C           - poison section
%%cell 866 803 steel    -50  902 -903  % steel plug | grapple adaptor

```

%%

```

%%cell 867 803 steel    50      -896  % lower carbon steel clad
%%cell 868 803 zr        50  896 -899  % zirc-3 clad (zirc follower)
%%cell 869 803 steel    50  899 -902  % upper carbon steel clad
%%cell 870 803 steel    50  902 -903  % steel plug | grapple adaptor
%%cell 871 803 Air_steel      903 -904  % grapple and air
%%cell 872 803 air        904          % air above CR

```

```

%%%#####
#####

```

C0 48inch.sss

% TREAT 48 inch Slotted Assembly (H1-H8 and H11-H18)

% Ben Baker

% Idaho National Laboratory

% Jan 20, 2016

[illegible][illegible]

% for cross section preparation we have the following regions

[illegible][illegible]

	% universe	material
1	100	100
2	100	100
3	100	100
4	100	100
5	100	100
6	100	100
7	100	100
8	100	100
9	100	100
10	100	100
11	100	100
12	100	100
13	100	100
14	100	100
15	100	100
16	100	100
17	100	100
18	100	100
19	100	100
20	100	100
21	100	100
22	100	100
23	100	100
24	100	100
25	100	100
26	100	100
27	100	100
28	100	100
29	100	100
30	100	100
31	100	100
32	100	100
33	100	100
34	100	100
35	100	100
36	100	100
37	100	100
38	100	100
39	100	100
40	100	100
41	100	100
42	100	100
43	100	100
44	100	100
45	100	100
46	100	100
47	100	100
48	100	100
49	100	100
50	100	100
51	100	100
52	100	100
53	100	100
54	100	100
55	100	100
56	100	100
57	100	100
58	100	100
59	100	100
60	100	100
61	100	100
62	100	100
63	100	100
64	100	100
65	100	100
66	100	100
67	100	100
68	100	100
69	100	100
70	100	100
71	100	100
72	100	100
73	100	100
74	100	100
75	100	100
76	100	100
77	100	100
78	100	100
79	100	100
80	100	100
81	100	100
82	100	100
83	100	100
84	100	100
85	100	100
86	100	100
87	100	100
88	100	100
89	100	100
90	100	100
91	100	100
92	100	100
93	100	100
94	100	100
95	100	100
96	100	100
97	100	100
98	100	100
99	100	100
100	100	100

%

%

% 5021 Aluminum base

% 5022 Lead

% 5023 Oct Graphite Reflector

% 5024 Square Graphite Reflector

% 5025 Zr caps

% 5026 Zr complete shell + Air

%	5027	Zr cut shell + supports + Air
---	------	-------------------------------

%

%	5028	Al-steel for baseplate
---	------	------------------------

% 5029 Al top fitting (The slotted assembly has lead all the way up)

%

% 5020 Build Assembly

% 5001-5013 Copy Assembly

% 5000 Reconstruct with Homogenized zones

%

[illegible][illegible]

% Universe 5000 - 5029

% Surfaces 5051 - 5086 (Reserve 5900 & 5999 for outside definitions)

% Cells 5000 - 5099

```
% Building in order from bottom
```

[illegible][illegible]

% Aluminum & air at end caps (Cells 4650-4659)

[illegible][illegible]

cell 5001 5021 aluminum -5051 % Aluminum Bottom, Artificially Long
 cell 5002 5021 air_out -5999 5051 % Air outside of clad

%%%%%%%%%%
 %%%%%%%%%%

% Lead (Bottom to Top) (Cells 4660-4669)

%%%%%%%%%%
 %%%%%%%%%%

cell 5003 5022 lead -5054 % lead base or top
 cell 5004 5022 air -5053 5054 % air between clad and contents
 cell 5005 5022 aluminum -5051 5053 % aluminum clad
 cell 5006 5022 air_out -5999 5051 % Air outside of clad

% Notes: Cut at 5071 -5072 and 5085 -5086

%%%%%%%%%%
 %%%%%%%%%%

% Graphite Reflector #1,#2 (Bottom to Top) (Cells 4670-4679)

%%%%%%%%%%
 %%%%%%%%%%

cell 5007 5023 reflector -5054 % reflector graphite
 cell 5008 5023 air -5053 5054 % air between clad and contents
 cell 5009 5023 aluminum -5051 5053 % aluminum clad
 cell 5010 5023 air_out -5999 5051 % Air outside of clad

% Notes: Cut at 5072 -5074 and 5083 -5085

%%%%%%%%%%
 %%%%%%%%%%

% Square Graphite Reflector (Bottom to Top) (Cells 4680-4689)

%%%%%%%%%%
 %%%%%%%%%%

cell 5011 5024 reflector -5056 % square Graphite reflector
 cell 5012 5024 air -5053 5056 % air between clad and contents
 cell 5013 5024 aluminum -5051 5053 -5075 % Aluminum clad
 cell 5014 5024 zr -5051 5053 5075 -5082 % 2x thick Zr clad
 cell 5015 5024 aluminum -5051 5053 5082 % Aluminum clad
 cell 5016 5024 air_out -5999 5051 % Air outside of clad

% Notes: Cut at 5074 -5076 and 5081 -5083

%%%%%%%%%%
 %%%%%%%%%%

% Zr Cap (Bottom to Top) (Cells 4690-4699)

%%%%%%%%%%
 %%%%%%%%%%

% Infinite Aluminum base

cell 5050 5028 Al_steel -5999

% Solid base - INF down and INF across

cell 5051 5029 Al_air -5999

% Solid base - INF down and INF across

% Notes: Used below 5070 and above 5086

%%%

% Build H1-H8, H11-H18 Slotted assembly (Cells 4600-4649)

%%%

% start at bottom then from the center out

cell 5060 5020 fill 5028 -5070 % Fill Area below

cell 5061 5020 fill 5021 5070 -5071 % Aluminum at bottom

cell 5062 5020 fill 5022 5071 -5072 % Lead at bottom

cell 5063 5020 fill 5023 5072 -5074 % Octa Graphite Reflector (Bottom)

cell 5064 5020 fill 5024 5074 -5076 % Square Graphite Reflector (Bottom)

cell 5065 5020 fill 5025 5076 -5077 % Zr solid base (Bottom)

cell 5066 5020 fill 5026 5077 -5078 % Zr + air base region (Bottom)

cell 5067 5020 fill 5027 5078 -5079 % Air + Zr cut shell (48 inch)

cell 5068 5020 fill 5026 5079 -5080 % Zr + air base region (Top)

cell 5069 5020 fill 5025 5080 -5081 % Zr solid base (Top)

cell 5070 5020 fill 5024 5081 -5083 % Square Graphite Reflector (Top)

cell 5071 5020 fill 5023 5083 -5085 % Octa Graphite Reflector (Top)

cell 5072 5020 fill 5022 5085 -5086 % Lead at top

cell 5073 5020 fill 5029 5086 % Fill Area above

%%%

% Copy Assembly to multiple universes to match STD assembly (Cells 4650-4669)

%%%

cell 5074 5001 fill 5020 -90

cell 5075 5002 fill 5020 -90

cell 5076 5003 fill 5020 -90

cell 5077 5004 fill 5020 -90

cell 5078 5005 fill 5020 -90

cell 5079 5006 fill 5020 -90

cell 5080 5007 fill 5020 -90

cell 5081 5008 fill 5020 -90

cell 5082 5009 fill 5020 -90

cell 5083 5010 fill 5020 -90

cell 5084 5011 fill 5020 -90

cell 5085 5012 fill 5020 -90

cell 5086 5013 fill 5020 -90

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Build Assembly to match universe sizes in STD assembly (Cells 4670-4689)
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
cell 5087 5000 fill 5001      -11 % Steel Grid Plate + Aluminum bottom fitting
cell 5088 5000 fill 5002      11 -12 % Oct graphite XS region 1 -- bottom
cell 5089 5000 fill 5003      12 -13 % Oct graphite XS region 2 -- bottom
cell 5090 5000 fill 5004      13 -14 % square graphite bottom + air gap + Al clad
cell 5091 5000 fill 5005      14 -17 % axial interface
cell 5092 5000 fill 5006      17 -18 % Fuel1 bottom
cell 5093 5000 fill 5007      18 -19 % Fuel2
cell 5094 5000 fill 5008      19 -20 % Fuel1 top
cell 5095 5000 fill 5009      20 -23 % aixal interface
cell 5096 5000 fill 5010      23 -25 % square graphite w hole top + Oct graphite with hole +
air + Al clad
cell 5097 5000 fill 5011      25 -26 % Oct graphite XS region 2 -- top
cell 5098 5000 fill 5012      26 -27 % Oct graphite XS region 1 -- top
cell 5099 5000 fill 5013      27    % top fitting

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Debug Assembly
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%
%include "/Users/bakeba/Desktop/HPC-Serpent/Assemblies/DebugAssembly.i"
%cell 3 1 fill 5000 -5900

```

```

%
%
%%%%%%%%% --- Geometry and mesh plots:
%plot 3 1000 1000 2.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 7.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 42.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 50.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 57.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 59.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 59.48 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 62.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 184.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 187.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 187.18 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 188.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 196.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 208.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 243.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 247.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 248.0 -5.08 5.08 -5.08 5.08 % xy-plot
%
%plot 2 800 4000 0.0 -5.08 5.08 0.0 247.65 % xz-plot
%
%plot 2 800 4000 -5.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 -4.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 -3.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 -2.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 -1.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 0.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 1.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 2.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 3.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 4.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 5.0 -5.08 5.08 0.0 247.65 % yz-plot
%
C1-C10.sss
% TREAT 50 inch Half-Slotted Assembly (H-21)

% Ben Baker
% Idaho National Laboratory
% Feb 12, 2016

%#####
##
% Reserve
% Universe [5100-5563] where base-level is every 50. 5100,5150,5200 ...

```

% and homogenization universes are XX01-XX13.
 % Cells [5YXX-5YXX] where XX is 01-26 (C1,C3,...C9) and 50-76 for (C2,C4..C10) and Y
 is 1-5

% Surf Same as C0

%#####
 ##

%%%%%%%%%%
 %%%%%%%%%%

% Define C1

% Description of placement:

% COPY UNIVERSES

cell 5101 5101 fill 5020 -90
 cell 5102 5102 fill 5020 -90
 cell 5103 5103 fill 5020 -90
 cell 5104 5104 fill 5020 -90
 cell 5105 5105 fill 5020 -90
 cell 5106 5106 fill 5020 -90
 cell 5107 5107 fill 5020 -90
 cell 5108 5108 fill 5020 -90
 cell 5109 5109 fill 5020 -90
 cell 5110 5110 fill 5020 -90
 cell 5111 5111 fill 5020 -90
 cell 5112 5112 fill 5020 -90
 cell 5113 5113 fill 5020 -90

%% BUILD C1

cell 5114 5100 fill 5101 -11 % Steel Grid Plate + Aluminum bottom fitting
 cell 5115 5100 fill 5102 11 -12 % Oct graphite XS region 1 -- bottom
 cell 5116 5100 fill 5103 12 -13 % Oct graphite XS region 2 -- bottom
 cell 5117 5100 fill 5104 13 -14 % square graphite bottom + air gap + Al clad
 cell 5118 5100 fill 5105 14 -17 % axial interface
 cell 5119 5100 fill 5106 17 -18 % Fuel1 bottom
 cell 5120 5100 fill 5107 18 -19 % Fuel2
 cell 5121 5100 fill 5108 19 -20 % Fuel1 top
 cell 5122 5100 fill 5109 20 -23 % axial interface
 cell 5123 5100 fill 5110 23 -25 % square graphite w hole top + Oct graphite with hole + air
 + Al clad
 cell 5124 5100 fill 5111 25 -26 % Oct graphite XS region 2 -- top
 cell 5125 5100 fill 5112 26 -27 % Oct graphite XS region 1 -- top
 cell 5126 5100 fill 5113 27 % top fitting

%%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%

% Define C2

% Description of placement:

% COPY UNIVERSES

cell 5151 5151 fill 5020 -90
 cell 5152 5152 fill 5020 -90
 cell 5153 5153 fill 5020 -90
 cell 5154 5154 fill 5020 -90
 cell 5155 5155 fill 5020 -90
 cell 5156 5156 fill 5020 -90
 cell 5157 5157 fill 5020 -90
 cell 5158 5158 fill 5020 -90
 cell 5159 5159 fill 5020 -90
 cell 5160 5160 fill 5020 -90
 cell 5161 5161 fill 5020 -90
 cell 5162 5162 fill 5020 -90
 cell 5163 5163 fill 5020 -90

%% BUILD C2

cell 5164 5150 fill 5151 -11 % Steel Grid Plate + Aluminum bottom fitting
 cell 5165 5150 fill 5152 11 -12 % Oct graphite XS region 1 -- bottom
 cell 5166 5150 fill 5153 12 -13 % Oct graphite XS region 2 -- bottom
 cell 5167 5150 fill 5154 13 -14 % square graphite bottom + air gap + Al clad
 cell 5168 5150 fill 5155 14 -17 % axial interface
 cell 5169 5150 fill 5156 17 -18 % Fuel1 bottom
 cell 5170 5150 fill 5157 18 -19 % Fuel2
 cell 5171 5150 fill 5158 19 -20 % Fuel1 top
 cell 5172 5150 fill 5159 20 -23 % axial interface
 cell 5173 5150 fill 5160 23 -25 % square graphite w hole top + Oct graphite with hole + air
 + Al clad
 cell 5174 5150 fill 5161 25 -26 % Oct graphite XS region 2 -- top
 cell 5175 5150 fill 5162 26 -27 % Oct graphite XS region 1 -- top
 cell 5176 5150 fill 5163 27 % top fitting

%%%%%%%%%%

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%%%%%%%%%%

% Define C3

% Description of placement:

% COPY UNIVERSES

cell 5201 5201 fill 5020 -90
 cell 5202 5202 fill 5020 -90
 cell 5203 5203 fill 5020 -90
 cell 5204 5204 fill 5020 -90
 cell 5205 5205 fill 5020 -90

cell 5206 5206 fill 5020 -90
 cell 5207 5207 fill 5020 -90
 cell 5208 5208 fill 5020 -90
 cell 5209 5209 fill 5020 -90
 cell 5210 5210 fill 5020 -90
 cell 5211 5211 fill 5020 -90
 cell 5212 5212 fill 5020 -90
 cell 5213 5213 fill 5020 -90

%% BUILD C3

cell 5214 5200 fill 5201 -11 % Steel Grid Plate + Aluminum bottom fitting
 cell 5215 5200 fill 5202 11 -12 % Oct graphite XS region 1 -- bottom
 cell 5216 5200 fill 5203 12 -13 % Oct graphite XS region 2 -- bottom
 cell 5217 5200 fill 5204 13 -14 % square graphite bottom + air gap + Al clad
 cell 5218 5200 fill 5205 14 -17 % axial interface
 cell 5219 5200 fill 5206 17 -18 % Fuel1 bottom
 cell 5220 5200 fill 5207 18 -19 % Fuel2
 cell 5221 5200 fill 5208 19 -20 % Fuel1 top
 cell 5222 5200 fill 5209 20 -23 % axial interface
 cell 5223 5200 fill 5210 23 -25 % square graphite w hole top + Oct graphite with hole + air
 + Al clad
 cell 5224 5200 fill 5211 25 -26 % Oct graphite XS region 2 -- top
 cell 5225 5200 fill 5212 26 -27 % Oct graphite XS region 1 -- top
 cell 5226 5200 fill 5213 27 % top fitting
 %%%%%%%%%%%
 %%%%%%%%%%%
 %%%%%%%%%%%
 %%%%%%%%%%%

% Define C4

% Description of placement:

% COPY UNIVERSES

cell 5251 5251 fill 5020 -90
 cell 5252 5252 fill 5020 -90
 cell 5253 5253 fill 5020 -90
 cell 5254 5254 fill 5020 -90
 cell 5255 5255 fill 5020 -90
 cell 5256 5256 fill 5020 -90
 cell 5257 5257 fill 5020 -90
 cell 5258 5258 fill 5020 -90
 cell 5259 5259 fill 5020 -90
 cell 5260 5260 fill 5020 -90
 cell 5261 5261 fill 5020 -90
 cell 5262 5262 fill 5020 -90
 cell 5263 5263 fill 5020 -90

%% BUILD C4

cell 5264 5250 fill 5251	-11	% Steel Grid Plate + Aluminum bottom fitting
cell 5265 5250 fill 5252	11 -12	% Oct graphite XS region 1 -- bottom
cell 5266 5250 fill 5253	12 -13	% Oct graphite XS region 2 -- bottom
cell 5267 5250 fill 5254	13 -14	% square graphite bottom + air gap + Al clad
cell 5268 5250 fill 5255	14 -17	% axial interface
cell 5269 5250 fill 5256	17 -18	% Fuel1 bottom
cell 5270 5250 fill 5257	18 -19	% Fuel2
cell 5271 5250 fill 5258	19 -20	% Fuel1 top
cell 5272 5250 fill 5259	20 -23	% axial interface
cell 5273 5250 fill 5260	23 -25	% square graphite w hole top + Oct graphite with hole + air
+ Al clad		
cell 5274 5250 fill 5261	25 -26	% Oct graphite XS region 2 -- top
cell 5275 5250 fill 5262	26 -27	% Oct graphite XS region 1 -- top
cell 5276 5250 fill 5263	27	% top fitting

%%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 %%%%%%%%%%
 % Define C5
 % Description of placement:

% COPY UNIVERSES

cell 5301 5301 fill 5020	-90
cell 5302 5302 fill 5020	-90
cell 5303 5303 fill 5020	-90
cell 5304 5304 fill 5020	-90
cell 5305 5305 fill 5020	-90
cell 5306 5306 fill 5020	-90
cell 5307 5307 fill 5020	-90
cell 5308 5308 fill 5020	-90
cell 5309 5309 fill 5020	-90
cell 5310 5310 fill 5020	-90
cell 5311 5311 fill 5020	-90
cell 5312 5312 fill 5020	-90
cell 5313 5313 fill 5020	-90

%% BUILD C5

cell 5314 5300 fill 5301	-11	% Steel Grid Plate + Aluminum bottom fitting
cell 5315 5300 fill 5302	11 -12	% Oct graphite XS region 1 -- bottom
cell 5316 5300 fill 5303	12 -13	% Oct graphite XS region 2 -- bottom
cell 5317 5300 fill 5304	13 -14	% square graphite bottom + air gap + Al clad
cell 5318 5300 fill 5305	14 -17	% axial interface
cell 5319 5300 fill 5306	17 -18	% Fuel1 bottom
cell 5320 5300 fill 5307	18 -19	% Fuel2
cell 5321 5300 fill 5308	19 -20	% Fuel1 top


```

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```
% Define C7
```

```
% Description of placement:
```

```
% COPY UNIVERSES
```

```

cell 5401 5401 fill 5020 -90
cell 5402 5402 fill 5020 -90
cell 5403 5403 fill 5020 -90
cell 5404 5404 fill 5020 -90
cell 5405 5405 fill 5020 -90
cell 5406 5406 fill 5020 -90
cell 5407 5407 fill 5020 -90
cell 5408 5408 fill 5020 -90
cell 5409 5409 fill 5020 -90
cell 5410 5410 fill 5020 -90
cell 5411 5411 fill 5020 -90
cell 5412 5412 fill 5020 -90
cell 5413 5413 fill 5020 -90

```

```
%% BUILD C7
```

```

cell 5414 5400 fill 5401 -11 % Steel Grid Plate + Aluminum bottom fitting
cell 5415 5400 fill 5402 11 -12 % Oct graphite XS region 1 -- bottom
cell 5416 5400 fill 5403 12 -13 % Oct graphite XS region 2 -- bottom
cell 5417 5400 fill 5404 13 -14 % square graphite bottom + air gap + Al clad
cell 5418 5400 fill 5405 14 -17 % axial interface
cell 5419 5400 fill 5406 17 -18 % Fuel1 bottom
cell 5420 5400 fill 5407 18 -19 % Fuel2
cell 5421 5400 fill 5408 19 -20 % Fuel1 top
cell 5422 5400 fill 5409 20 -23 % axial interface
cell 5423 5400 fill 5410 23 -25 % square graphite w hole top + Oct graphite with hole + air
+ Al clad
cell 5424 5400 fill 5411 25 -26 % Oct graphite XS region 2 -- top
cell 5425 5400 fill 5412 26 -27 % Oct graphite XS region 1 -- top
cell 5426 5400 fill 5413 27 % top fitting

```

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```
% Define C8
```

```
% Description of placement:
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```
% COPY UNIVERSES
```

```

cell 5451 5451 fill 5020 -90
cell 5452 5452 fill 5020 -90
cell 5453 5453 fill 5020 -90

```

cell 5454 5454 fill 5020 -90
 cell 5455 5455 fill 5020 -90
 cell 5456 5456 fill 5020 -90
 cell 5457 5457 fill 5020 -90
 cell 5458 5458 fill 5020 -90
 cell 5459 5459 fill 5020 -90
 cell 5460 5460 fill 5020 -90
 cell 5461 5461 fill 5020 -90
 cell 5462 5462 fill 5020 -90
 cell 5463 5463 fill 5020 -90

%% BUILD C8

cell 5464 5450 fill 5451 -11 % Steel Grid Plate + Aluminum bottom fitting
 cell 5465 5450 fill 5452 11 -12 % Oct graphite XS region 1 -- bottom
 cell 5466 5450 fill 5453 12 -13 % Oct graphite XS region 2 -- bottom
 cell 5467 5450 fill 5454 13 -14 % square graphite bottom + air gap + Al clad
 cell 5468 5450 fill 5455 14 -17 % axial interface
 cell 5469 5450 fill 5456 17 -18 % Fuel1 bottom
 cell 5470 5450 fill 5457 18 -19 % Fuel2
 cell 5471 5450 fill 5458 19 -20 % Fuel1 top
 cell 5472 5450 fill 5459 20 -23 % axial interface
 cell 5473 5450 fill 5460 23 -25 % square graphite w hole top + Oct graphite with hole + air
 + Al clad
 cell 5474 5450 fill 5461 25 -26 % Oct graphite XS region 2 -- top
 cell 5475 5450 fill 5462 26 -27 % Oct graphite XS region 1 -- top
 cell 5476 5450 fill 5463 27 % top fitting

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 %%%%%%%%%

% Define C9

% Description of placement:

% COPY UNIVERSES

cell 5501 5501 fill 5020 -90
 cell 5502 5502 fill 5020 -90
 cell 5503 5503 fill 5020 -90
 cell 5504 5504 fill 5020 -90
 cell 5505 5505 fill 5020 -90
 cell 5506 5506 fill 5020 -90
 cell 5507 5507 fill 5020 -90
 cell 5508 5508 fill 5020 -90
 cell 5509 5509 fill 5020 -90
 cell 5510 5510 fill 5020 -90
 cell 5511 5511 fill 5020 -90
 cell 5512 5512 fill 5020 -90

cell 5513 5513 fill 5020 -90

%% BUILD C9

cell 5514 5500 fill 5501 -11 % Steel Grid Plate + Aluminum bottom fitting
 cell 5515 5500 fill 5502 11 -12 % Oct graphite XS region 1 -- bottom
 cell 5516 5500 fill 5503 12 -13 % Oct graphite XS region 2 -- bottom
 cell 5517 5500 fill 5504 13 -14 % square graphite bottom + air gap + Al clad
 cell 5518 5500 fill 5505 14 -17 % axial interface
 cell 5519 5500 fill 5506 17 -18 % Fuel1 bottom
 cell 5520 5500 fill 5507 18 -19 % Fuel2
 cell 5521 5500 fill 5508 19 -20 % Fuel1 top
 cell 5522 5500 fill 5509 20 -23 % axial interface
 cell 5523 5500 fill 5510 23 -25 % square graphite w hole top + Oct graphite with hole + air
 + Al clad
 cell 5524 5500 fill 5511 25 -26 % Oct graphite XS region 2 -- top
 cell 5525 5500 fill 5512 26 -27 % Oct graphite XS region 1 -- top
 cell 5526 5500 fill 5513 27 % top fitting

%%%%%%%%%%
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% Define C10

% Description of placement:

% COPY UNIVERSES

cell 5551 5551 fill 5020 -90
 cell 5552 5552 fill 5020 -90
 cell 5553 5553 fill 5020 -90
 cell 5554 5554 fill 5020 -90
 cell 5555 5555 fill 5020 -90
 cell 5556 5556 fill 5020 -90
 cell 5557 5557 fill 5020 -90
 cell 5558 5558 fill 5020 -90
 cell 5559 5559 fill 5020 -90
 cell 5560 5560 fill 5020 -90
 cell 5561 5561 fill 5020 -90
 cell 5562 5562 fill 5020 -90
 cell 5563 5563 fill 5020 -90

%% BUILD C10

cell 5564 5550 fill 5551 -11 % Steel Grid Plate + Aluminum bottom fitting
 cell 5565 5550 fill 5552 11 -12 % Oct graphite XS region 1 -- bottom
 cell 5566 5550 fill 5553 12 -13 % Oct graphite XS region 2 -- bottom
 cell 5567 5550 fill 5554 13 -14 % square graphite bottom + air gap + Al clad
 cell 5568 5550 fill 5555 14 -17 % axial interface
 cell 5569 5550 fill 5556 17 -18 % Fuel1 bottom

```

cell 5570 5550 fill 5557    18 -19 % Fuel2
cell 5571 5550 fill 5558    19 -20 % Fuel1 top
cell 5572 5550 fill 5559    20 -23 % axial interface
cell 5573 5550 fill 5560    23 -25 % square graphite w hole top + Oct graphite with hole + air
+ Al clad
cell 5574 5550 fill 5561    25 -26 % Oct graphite XS region 2 -- top
cell 5575 5550 fill 5562    26 -27 % Oct graphite XS region 1 -- top
cell 5576 5550 fill 5563    27      % top fitting
%%%%%%%%%%
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%%%%%%%%%%
%%%%%%%%%%

```

```
% Define C11
```

```
% Description of placement:
```

```
% COPY UNIVERSES
```

```

cell 5601 5601 fill 5020    -90
cell 5602 5602 fill 5020    -90
cell 5603 5603 fill 5020    -90
cell 5604 5604 fill 5020    -90
cell 5605 5605 fill 5020    -90
cell 5606 5606 fill 5020    -90
cell 5607 5607 fill 5020    -90
cell 5608 5608 fill 5020    -90
cell 5609 5609 fill 5020    -90
cell 5610 5610 fill 5020    -90
cell 5611 5611 fill 5020    -90
cell 5612 5612 fill 5020    -90
cell 5613 5613 fill 5020    -90

```

```
%% BUILD C11
```

```

cell 5614 5600 fill 5601    -11 % Steel Grid Plate + Aluminum bottom fitting
cell 5615 5600 fill 5602    11 -12 % Oct graphite XS region 1 -- bottom
cell 5616 5600 fill 5603    12 -13 % Oct graphite XS region 2 -- bottom
cell 5617 5600 fill 5604    13 -14 % square graphite bottom + air gap + Al clad
cell 5618 5600 fill 5605    14 -17 % axial interface
cell 5619 5600 fill 5606    17 -18 % Fuel1 bottom
cell 5620 5600 fill 5607    18 -19 % Fuel2
cell 5621 5600 fill 5608    19 -20 % Fuel1 top
cell 5622 5600 fill 5609    20 -23 % axial interface
cell 5623 5600 fill 5610    23 -25 % square graphite w hole top + Oct graphite with hole + air
+ Al clad
cell 5624 5600 fill 5611    25 -26 % Oct graphite XS region 2 -- top
cell 5625 5600 fill 5612    26 -27 % Oct graphite XS region 1 -- top
cell 5626 5600 fill 5613    27      % top fitting

```

```

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```

```
% Define C12
```

```
% Description of placement:
```

```
% COPY UNIVERSES
```

```

cell 5651 5651 fill 5020 -90
cell 5652 5652 fill 5020 -90
cell 5653 5653 fill 5020 -90
cell 5654 5654 fill 5020 -90
cell 5655 5655 fill 5020 -90
cell 5656 5656 fill 5020 -90
cell 5657 5657 fill 5020 -90
cell 5658 5658 fill 5020 -90
cell 5659 5659 fill 5020 -90
cell 5660 5660 fill 5020 -90
cell 5661 5661 fill 5020 -90
cell 5662 5662 fill 5020 -90
cell 5663 5663 fill 5020 -90

```

```
%% BUILD C12
```

```

cell 5664 5650 fill 5651 -11 % Steel Grid Plate + Aluminum bottom fitting
cell 5665 5650 fill 5652 11 -12 % Oct graphite XS region 1 -- bottom
cell 5666 5650 fill 5653 12 -13 % Oct graphite XS region 2 -- bottom
cell 5667 5650 fill 5654 13 -14 % square graphite bottom + air gap + Al clad
cell 5668 5650 fill 5655 14 -17 % axial interface
cell 5669 5650 fill 5656 17 -18 % Fuel1 bottom
cell 5670 5650 fill 5657 18 -19 % Fuel2
cell 5671 5650 fill 5658 19 -20 % Fuel1 top
cell 5672 5650 fill 5659 20 -23 % axial interface
cell 5673 5650 fill 5660 23 -25 % square graphite w hole top + Oct graphite with hole + air
+ Al clad
cell 5674 5650 fill 5661 25 -26 % Oct graphite XS region 2 -- top
cell 5675 5650 fill 5662 26 -27 % Oct graphite XS region 1 -- top
cell 5676 5650 fill 5663 27 % top fitting

```

```

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```

```
% Define C13
```

```
% Description of placement:
```

```
% COPY UNIVERSES
```

```
cell 5701 5701 fill 5020 -90
```

cell 5702 5702 fill 5020 -90
 cell 5703 5703 fill 5020 -90
 cell 5704 5704 fill 5020 -90
 cell 5705 5705 fill 5020 -90
 cell 5706 5706 fill 5020 -90
 cell 5707 5707 fill 5020 -90
 cell 5708 5708 fill 5020 -90
 cell 5709 5709 fill 5020 -90
 cell 5710 5710 fill 5020 -90
 cell 5711 5711 fill 5020 -90
 cell 5712 5712 fill 5020 -90
 cell 5713 5713 fill 5020 -90

%% BUILD C13

cell 5714 5700 fill 5701 -11 % Steel Grid Plate + Aluminum bottom fitting
 cell 5715 5700 fill 5702 11 -12 % Oct graphite XS region 1 -- bottom
 cell 5716 5700 fill 5703 12 -13 % Oct graphite XS region 2 -- bottom
 cell 5717 5700 fill 5704 13 -14 % square graphite bottom + air gap + Al clad
 cell 5718 5700 fill 5705 14 -17 % axial interface
 cell 5719 5700 fill 5706 17 -18 % Fuel1 bottom
 cell 5720 5700 fill 5707 18 -19 % Fuel2
 cell 5721 5700 fill 5708 19 -20 % Fuel1 top
 cell 5722 5700 fill 5709 20 -23 % axial interface
 cell 5723 5700 fill 5710 23 -25 % square graphite w hole top + Oct graphite with hole + air
 + Al clad
 cell 5724 5700 fill 5711 25 -26 % Oct graphite XS region 2 -- top
 cell 5725 5700 fill 5712 26 -27 % Oct graphite XS region 1 -- top
 cell 5726 5700 fill 5713 27 % top fitting
 %%%%%%%%%%%
 %%%%%%%%%%%
 %%%%%%%%%%%
 %%%%%%%%%%%

% Define C14

% Description of placement:

% COPY UNIVERSES

cell 5751 5751 fill 5020 -90
 cell 5752 5752 fill 5020 -90
 cell 5753 5753 fill 5020 -90
 cell 5754 5754 fill 5020 -90
 cell 5755 5755 fill 5020 -90
 cell 5756 5756 fill 5020 -90
 cell 5757 5757 fill 5020 -90
 cell 5758 5758 fill 5020 -90
 cell 5759 5759 fill 5020 -90
 cell 5760 5760 fill 5020 -90

cell 5761 5761 fill 5020 -90
 cell 5762 5762 fill 5020 -90
 cell 5763 5763 fill 5020 -90

%% BUILD C14

cell 5764 5750 fill 5751 -11 % Steel Grid Plate + Aluminum bottom fitting
 cell 5765 5750 fill 5752 11 -12 % Oct graphite XS region 1 -- bottom
 cell 5766 5750 fill 5753 12 -13 % Oct graphite XS region 2 -- bottom
 cell 5767 5750 fill 5754 13 -14 % square graphite bottom + air gap + Al clad
 cell 5768 5750 fill 5755 14 -17 % axial interface
 cell 5769 5750 fill 5756 17 -18 % Fuel1 bottom
 cell 5770 5750 fill 5757 18 -19 % Fuel2
 cell 5771 5750 fill 5758 19 -20 % Fuel1 top
 cell 5772 5750 fill 5759 20 -23 % axial interface
 cell 5773 5750 fill 5760 23 -25 % square graphite w hole top + Oct graphite with hole + air
 + Al clad
 cell 5774 5750 fill 5761 25 -26 % Oct graphite XS region 2 -- top
 cell 5775 5750 fill 5762 26 -27 % Oct graphite XS region 1 -- top
 cell 5776 5750 fill 5763 27 % top fitting

%%%%%%%%%%
 %%%%%%%%%
 %%%%%%%%%
 %%%%%%%%%

% Define C15

% Description of placement:

% COPY UNIVERSES

cell 5801 5801 fill 5020 -90
 cell 5802 5802 fill 5020 -90
 cell 5803 5803 fill 5020 -90
 cell 5804 5804 fill 5020 -90
 cell 5805 5805 fill 5020 -90
 cell 5806 5806 fill 5020 -90
 cell 5807 5807 fill 5020 -90
 cell 5808 5808 fill 5020 -90
 cell 5809 5809 fill 5020 -90
 cell 5810 5810 fill 5020 -90
 cell 5811 5811 fill 5020 -90
 cell 5812 5812 fill 5020 -90
 cell 5813 5813 fill 5020 -90

%% BUILD C15

cell 5814 5800 fill 5801 -11 % Steel Grid Plate + Aluminum bottom fitting
 cell 5815 5800 fill 5802 11 -12 % Oct graphite XS region 1 -- bottom
 cell 5816 5800 fill 5803 12 -13 % Oct graphite XS region 2 -- bottom
 cell 5817 5800 fill 5804 13 -14 % square graphite bottom + air gap + Al clad

```

cell 5818 5800 fill 5805    14 -17  % axial interface
cell 5819 5800 fill 5806    17 -18  % Fuel1 bottom
cell 5820 5800 fill 5807    18 -19  % Fuel2
cell 5821 5800 fill 5808    19 -20  % Fuel1 top
cell 5822 5800 fill 5809    20 -23  % aixal interface
cell 5823 5800 fill 5810    23 -25  % square graphite w hole top + Oct graphite with hole + air
+ Al clad
cell 5824 5800 fill 5811    25 -26  % Oct graphite XS region 2 -- top
cell 5825 5800 fill 5812    26 -27  % Oct graphite XS region 1 -- top
cell 5826 5800 fill 5813    27      % top fitting

```

```

%%%%%%%%%
%%%%%%%%%
%%%%%%%%%
%%%%%%%%%

```

```
% Define C16
```

```
% Description of placement:
```

```
% COPY UNIVERSES
```

```

cell 5851 5851 fill 5020    -90
cell 5852 5852 fill 5020    -90
cell 5853 5853 fill 5020    -90
cell 5854 5854 fill 5020    -90
cell 5855 5855 fill 5020    -90
cell 5856 5856 fill 5020    -90
cell 5857 5857 fill 5020    -90
cell 5858 5858 fill 5020    -90
cell 5859 5859 fill 5020    -90
cell 5860 5860 fill 5020    -90
cell 5861 5861 fill 5020    -90
cell 5862 5862 fill 5020    -90
cell 5863 5863 fill 5020    -90

```

```
%% BUILD C16
```

```

cell 5864 5850 fill 5851    -11  % Steel Grid Plate + Aluminum bottom fitting
cell 5865 5850 fill 5852    11 -12  % Oct graphite XS region 1 -- bottom
cell 5866 5850 fill 5853    12 -13  % Oct graphite XS region 2 -- bottom
cell 5867 5850 fill 5854    13 -14  % square graphite bottom + air gap + Al clad
cell 5868 5850 fill 5855    14 -17  % axial interface
cell 5869 5850 fill 5856    17 -18  % Fuel1 bottom
cell 5870 5850 fill 5857    18 -19  % Fuel2
cell 5871 5850 fill 5858    19 -20  % Fuel1 top
cell 5872 5850 fill 5859    20 -23  % aixal interface
cell 5873 5850 fill 5860    23 -25  % square graphite w hole top + Oct graphite with hole + air
+ Al clad
cell 5874 5850 fill 5861    25 -26  % Oct graphite XS region 2 -- top
cell 5875 5850 fill 5862    26 -27  % Oct graphite XS region 1 -- top

```

```

cell 5876 5850 fill 5863    27    % top fitting
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
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%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%   Debug Assembly
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%
%include "/Users/bakeba/Desktop/HPC-Serpent/Assemblies/C/C0_48inch.i"
%include "/Users/bakeba/Desktop/HPC-Serpent/Assemblies/DebugAssembly.i"
%cell 3 1 fill 5550 -5900
%
%
%%%%%%%%%% --- Geometry and mesh plots:
%plot 3 1000 1000  2.0  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000  7.0  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 42.0  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 50.0  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 57.0  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 59.0  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 59.48 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 62.0  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 184.0 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 187.0 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 187.18 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 188.0 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 196.0 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 208.0 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 243.0 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 247.0 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 248.0 -5.08 5.08  -5.08  5.08    % xy-plot
%
%plot 2 800 4000  0.0  -5.08 5.08  0.0  247.65    % xz-plot
%
%plot 2 800 4000 -5.0  -5.08 5.08  0.0  247.65    % yz-plot
%plot 2 800 4000 -4.0  -5.08 5.08  0.0  247.65    % yz-plot
%plot 2 800 4000 -3.0  -5.08 5.08  0.0  247.65    % yz-plot

```

```
%plot 2 800 4000 -2.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 -1.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 0.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 1.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 2.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 3.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 4.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 5.0 -5.08 5.08 0.0 247.65 % yz-plot
```

C9_Half-Slot.sss

% TREAT 50 inch Half-Slotted Assembly (H-21)

% Ben Baker

% Idaho National Laboratory

% Feb 2, 2016

```
%%%%%%%%%%
%%%%%%%%%
```

% Half-Slotted Assembly

```
%%%%%%%%%%
%%%%%%%%%
```

%

%

```
%%%%%%%%%%
%%%%%%%%%
```

% for cross section preparation we have the following regions

```
%%%%%%%%%%
%%%%%%%%%
```

% universe material

%

%

% 5921 Aluminum base

% 5922 Lead

% 5923 Oct Graphite Reflector

% 5924 Zr caps

% 5925 Zr cut shell + supports + Air

%

% 5926 Al-steel for baseplate

% 5927 Al top fitting (The slotted assembly has lead all the way up)

%

% 5920 Build Assembly

% 5901-5913 Copy Assembly

% 5900 Reconstruct with Homogenized zones

%

```
%%%%%%%%%%
%%%%%%%%%
```

% Reserve
 % Universe [5900, 5920-5927] [Final 5900]
 % Cells [5900-5986]
 % Surf [5151-5176] Also dependent on full-48inch slotted surfaces
 %
 % Aluminum & Zr Clad (Bottom, Top Fittings, P1 & P2 Extensions)
 % Aluminum is filling to Zr clad
 % y-axis-cuts
 cell 5900 5921 aluminum -5052 -5152 % Fittings and Extensions
 cell 5901 5921 zr -5051 5052 -5152 % Zr clad except cut
 cell 5902 5921 zr -5051 5152 -5151 % Zr clad at cut
 cell 5903 5921 air_out -5999 5051 -5151 % Air outside of clad until cut
 cell 5904 5921 air_out -5999 5151 % Air outside of clad above cut
 % Lead (Bottom to Top)
 % Lead is filling to Zr clad
 cell 5905 5922 lead -5052 -5152 % Lead
 cell 5906 5922 zr -5051 5052 -5152 % Zr clad except cut
 cell 5907 5922 zr -5051 5152 -5151 % Zr clad at cut
 cell 5908 5922 air_out -5999 5051 -5151 % Air outside of clad until cut
 cell 5909 5922 air_out -5999 5151 % Air outside of clad above cut
 % Graphite Reflector (Bottom to Top)
 % Graphite filling to Zr clad
 cell 5910 5923 reflector -5052 -5152 % Graphite
 cell 5911 5923 zr -5051 5052 -5152 % Zr clad except cut
 cell 5912 5923 zr -5051 5152 -5151 % Zr clad at cut
 cell 5913 5923 air_out -5999 5051 -5151 % Air outside of clad until cut
 cell 5914 5923 air_out -5999 5151 % Air outside of clad above cut
 % Zr Cap/Divider (Bottom to Top)

%%
 %%

cell 5915 5924 zr -5051 -5151 % Zr divider
 cell 5916 5924 air_out -5999 5051 -5151 % Air outside of clad until cut
 cell 5917 5924 air_out -5999 5151 % Air outside of clad above cut

%%
 %%

% Cut Zr Shell + Large Air Slot
 %%
 %%

% Use surf 5053 (2x-Zr or Al octa) for part of stiffener

cell 5918 5925 zr -5051 5052 5055 -5152 % Zr shell for Large Void Region
 cell 5919 5925 zr -5051 5055 -5151 5152
 cell 5920 5925 zr -5052 5053 5055 -5152 5158 5159 % Stiffener on wall (minus square)
 cell 5921 5925 zr -5053 5055 -5152 5153 % Stiffener up by cut
 cell 5922 5925 zr -5160 5158 % Stiffener square
 cell 5923 5925 zr -5161 5159 % Stiffener square
 cell 5924 5925 air -5158 % Air inside square
 cell 5925 5925 air -5159 % Air inside square
 cell 5926 5925 zr -5053 5154 -5155 -5153 5160 % Flat stiffener on LHS
 cell 5927 5925 zr -5053 5157 -5156 -5153 5161 % Flat stiffener on RHS
 cell 5928 5925 air -5053 -5154 -5153 5160 % Air on LHS
 cell 5929 5925 air -5053 5156 -5153 5161 % Air on RHS
 cell 5930 5925 air -5055 -5151 % Large Void Region
 cell 5931 5925 air -5053 5055 5155 -5157 -5153 % Air between Large void and stiffener flat sides
 cell 5932 5925 air_out -5999 5051 -5151 % Air outside of clad until cut
 cell 5933 5925 air_out -5999 5151 % Air outside of clad above cut

%%
 %%

% INF top and bottom (Cells 4720-4725)
 %%
 %%

% Infinite Aluminum base

cell 5934 5926 Al_steel -5999 % Solid base - INF down and INF across
 cell 5935 5927 Al_air -5999 % Solid base - INF down and INF across
 %%
 %%

% Build Assembly

%%
 %%

cell 5950	5920	fill 5926	-5070	% Al-steel outside
cell 5951	5920	fill 5921	5070 -5166	% Al Fitting & P2
cell 5952	5920	fill 5922	5166 -5168	% Lead bottom
cell 5953	5920	fill 5923	5168 -5169	% Graphite bottom
cell 5954	5920	fill 5924	5169 -5170	% Zr divider
cell 5955	5920	fill 5925	5170 -5171	% Air Slot
cell 5956	5920	fill 5924	5171 -5172	% Zr divider
cell 5957	5920	fill 5923	5172 -5173	% Graphite top
cell 5958	5920	fill 5922	5173 -5174	% Lead top
cell 5959	5920	fill 5921	5174 -5176	% Al Fitting & P1
cell 5960	5920	fill 5927	5086	% Fill Area above

%%
 %%%

% Copy Assembly to multiple universes to match STD assembly

%%
 %%%

cell 5961	5901	fill 5920	-90
cell 5962	5902	fill 5920	-90
cell 5963	5903	fill 5920	-90
cell 5964	5904	fill 5920	-90
cell 5965	5905	fill 5920	-90
cell 5966	5906	fill 5920	-90
cell 5967	5907	fill 5920	-90
cell 5968	5908	fill 5920	-90
cell 5969	5909	fill 5920	-90
cell 5970	5910	fill 5920	-90
cell 5971	5911	fill 5920	-90
cell 5972	5912	fill 5920	-90
cell 5973	5913	fill 5920	-90

%%
 %%%

% Build Assembly to match universe sizes in STD assembly (North-Side)

%%
 %%%

cell 5974	5900	fill 5901	-11	% Steel Grid Plate + Aluminum bottom fitting
cell 5975	5900	fill 5902	11 -12	% Oct graphite XS region 1 -- bottom
cell 5976	5900	fill 5903	12 -13	% Oct graphite XS region 2 -- bottom
cell 5977	5900	fill 5904	13 -14	% square graphite bottom + air gap + Al clad
cell 5978	5900	fill 5905	14 -17	% axial interface
cell 5979	5900	fill 5906	17 -18	% Fuel1 bottom
cell 5980	5900	fill 5907	18 -19	% Fuel2
cell 5981	5900	fill 5908	19 -20	% Fuel1 top
cell 5982	5900	fill 5909	20 -23	% aixal interface

cell 5983 5900 fill 5910	23 -25	% square graphite w hole top + Oct graphite with hole + air + Al clad
cell 5984 5900 fill 5911	25 -26	% Oct graphite XS region 2 -- top
cell 5985 5900 fill 5912	26 -27	% Oct graphite XS region 1 -- top
cell 5986 5900 fill 5913	27	% top fitting

%%%

% 1/2 Slotted Assembly South Facing

%%%

cell 5987 5951 fill 5920	-90
cell 5988 5952 fill 5920	-90
cell 5989 5953 fill 5920	-90
cell 5990 5954 fill 5920	-90
cell 5991 5955 fill 5920	-90
cell 5992 5956 fill 5920	-90
cell 5993 5957 fill 5920	-90
cell 5994 5958 fill 5920	-90
cell 5995 5959 fill 5920	-90
cell 5996 5960 fill 5920	-90
cell 5997 5961 fill 5920	-90
cell 5998 5962 fill 5920	-90
cell 5999 5963 fill 5920	-90

trans 5951 0 0 0 0 0 180
trans 5952 0 0 0 0 0 180
trans 5953 0 0 0 0 0 180
trans 5954 0 0 0 0 0 180
trans 5955 0 0 0 0 0 180
trans 5956 0 0 0 0 0 180
trans 5957 0 0 0 0 0 180
trans 5958 0 0 0 0 0 180
trans 5959 0 0 0 0 0 180
trans 5960 0 0 0 0 0 180
trans 5961 0 0 0 0 0 180
trans 5962 0 0 0 0 0 180
trans 5963 0 0 0 0 0 180

%%%

%%%

% Build Assembly to match universe sizes in STD assembly (South-Side)

%%%

%%%

cell 5899 5950 fill 5951	-11	% Steel Grid Plate + Aluminum bottom fitting
cell 5898 5950 fill 5952	11 -12	% Oct graphite XS region 1 -- bottom
cell 5897 5950 fill 5953	12 -13	% Oct graphite XS region 2 -- bottom
cell 5896 5950 fill 5954	13 -14	% square graphite bottom + air gap + Al clad

```

cell 5895 5950 fill 5955      14 -17 % axial interface
cell 5894 5950 fill 5956      17 -18 % Fuel1 bottom
cell 5893 5950 fill 5957      18 -19 % Fuel2
cell 5892 5950 fill 5958      19 -20 % Fuel1 top
cell 5891 5950 fill 5959      20 -23 % axial interface
cell 5890 5950 fill 5960      23 -25 % square graphite w hole top + Oct graphite with hole +
air + Al clad
cell 5889 5950 fill 5961      25 -26 % Oct graphite XS region 2 -- top
cell 5888 5950 fill 5962      26 -27 % Oct graphite XS region 1 -- top
cell 5887 5950 fill 5963      27    % top fitting

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
% Debug Assembly
```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
%
```

```
%include "/Users/bakeba/Desktop/HPC-Serpent/Assemblies/DebugAssembly.i"
```

```
%cell 3 1 fill 5900 -5900
```

```
%
```

```
%
```

```
%%%%%%%%% --- Geometry and mesh plots:
```

```

%plot 3 1000 1000  1.5  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000  2.0  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 42.0  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 59.0  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 59.8  -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 186.7 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 186.85 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 222.0 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 243.1 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 247.1 -5.08 5.08  -5.08  5.08    % xy-plot
%plot 3 1000 1000 248.1 -5.08 5.08  -5.08  5.08    % xy-plot

```

```
D0.sss
```

```
% TREAT Dummy Zirconium Clad Assembly
```

```
% Type D
```

```
% Modification: NO outgas hole.
```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
% for cross section preparation we have the following regions
```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% universe    material
%
%
% 6021      Oct graphite XS + air gap + Al clad + air channel
% 6022      Square graphite + air gap + Al clad + air channel + Oct Graphite on top
% 6023      axial interface + air channel
% 6024      Fuel region + air gap + Zr clad + air channel
%
% 6001      Al-steel for baseplate
% 6013      Al top fitting (The slotted assembly has lead all the way up)
%
% 6002-12   Copy universes to build final
% 6000      Build Assembly
%
%#####
##
%#####
##
%
% Universe 6000 - 6024
% Surfaces  -   (Uses same surfaces as A's)
% Cells    6000 - 6047
%
%#####
##
%#####
##
% Full homogenization with homogenized channels
%#####
##
%#####
##
% Reflector Oct graphite XS
cell 6001 6021 reflector -4      % Oct graphite reflector
cell 6002 6021 air      -5  4    % air gap
cell 6003 6021 aluminum -3  5    % Al clad
cell 6004 6021 air_out   3      % air out
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Square reflector up to top Oct XS region
cell 6005 6022 reflector -6      -24 % Square graphite bottom to top
cell 6006 6022 air      -5  6  -24 % air gap between square graphite
cell 6007 6022 reflector -4  24    % Oct graphite no hole on top
cell 6008 6022 air      -5  4 24    % air gap between oct graphite and clad
cell 6009 6022 aluminum -3  5      % Al clad

```

[illegible]

```

% Reflector Oct Region 2 Top
cell 6031 6011 fill 6021 -90
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Reflector Oct Region 1 Top
cell 6032 6012 fill 6021 -90
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%
% INF top and bottom
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Infinite Aluminum base
cell 6033 6001 Al_steel -90      % Solid base - INF down and INF across
cell 6034 6013 Al_air -90      % Solid base - INF down and INF across

%#####
##
%#####
##
% Build std assembly
%#####
##
%#####
##
% start at bottom then from the center out
cell 6035 6000 fill 6001      -11 % Steel Grid Plate + Aluminum bottom fitting
cell 6036 6000 fill 6002      11 -12 % Oct graphite XS region 1 -- bottom
cell 6037 6000 fill 6003      12 -13 % Oct graphite XS region 2 -- bottom
cell 6038 6000 fill 6004      13 -14 % square graphite bottom + air gap + Al clad
cell 6039 6000 fill 6005      14 -17 % axial interface
cell 6040 6000 fill 6006      17 -18 % Fuel1 bottom
cell 6041 6000 fill 6007      18 -19 % Fuel2
cell 6042 6000 fill 6008      19 -20 % Fuel1 top
cell 6043 6000 fill 6009      20 -23 % aixal interface
cell 6044 6000 fill 6010      23 -25 % square graphite w hole top + Oct graphite with hole +
air + Al clad
cell 6045 6000 fill 6011      25 -26 % Oct graphite XS region 2 -- top
cell 6046 6000 fill 6012      26 -27 % Oct graphite XS region 1 -- top
cell 6047 6000 fill 6013      27      % top fitting

```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
% Debug Assembly
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
%include "/Users/bakeba/Desktop/HPC-Serpent/Assemblies/DebugAssembly.i"
```

```
%cell 3 1 fill 6000 -5900
```

```
%%%%%%%% --- Geometry and mesh plots:
```

```
%plot 3 1000 1000 1.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 5.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 31.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 54.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 62.1 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 62.3 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 62.6 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 70.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 90.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 170.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 183.9 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 184.2 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 184.5 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 185.0 -5.08 5.08 -5.08 5.08 % xy-plot
%plot 3 1000 1000 194.0 -5.08 5.08 -5.08 5.08 % xy-plot (hex + air hole)
%plot 3 1000 1000 207.0 -5.08 5.08 -5.08 5.08 % xy-plot (hex + no hole)
%plot 3 1000 1000 222.0 -5.08 5.08 -5.08 5.08 % xy-plot (hex + no hole)
%plot 3 1000 1000 249.0 -5.08 5.08 -5.08 5.08 % xy-plot (hex + no hole)
```

```
%plot 2 800 4000 0.0 -5.08 5.08 0.0 247.65 % xz-plot
```

```
%plot 1 800 4000 0.0 -5.08 5.08 0.0 247.65 % yz-plot
```

```
D1-Half.sss
```

```
% TREAT Half Assembly (Next to M8)
```

```
% Ben Baker
```

```
% Idaho National Laboratory
```

```
% Feb 2, 2016
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
% Half-Slotted Assembly
```

%%%%%%%%%%
 %%%%%%%%%%
 %

% Reserve

% Universe [6100, 6101-6113, 6120] [Final 6100]

% Cells [6100-6132]

% Surf Derived from half-slotted

% We can use many of the same surfaces or universes as the half-slotted assembly

%%%%%%%%%%
 %%%%%%%%%%
 %

Build Assembly (Surf and fill universes come from Half-Slotted)

%%%%%%%%%%
 %%%%%%%%%%

cell 6100	6120	fill 5926	-5070	% Al-steel outside
cell 6101	6120	fill 5921	5070 -5166	% Al Fitting & P2
cell 6102	6120	fill 5922	5166 -5168	% Lead bottom
cell 6103	6120	fill 5923	5168 -5174	% Graphite
cell 6104	6120	fill 5924	5174 -5176	% Al Fitting & P1
cell 6105	6120	fill 5927	5176	% Fill Area above

%%%%%%%%%%
 %%%%%%%%%%

% Copy Assembly to multiple universes to match STD assembly

%%%%%%%%%%
 %%%%%%%%%%

cell 6106	6101	fill 6120	-90
cell 6107	6102	fill 6120	-90
cell 6108	6103	fill 6120	-90
cell 6109	6104	fill 6120	-90
cell 6110	6105	fill 6120	-90
cell 6111	6106	fill 6120	-90
cell 6112	6107	fill 6120	-90
cell 6113	6108	fill 6120	-90
cell 6114	6109	fill 6120	-90
cell 6115	6110	fill 6120	-90
cell 6116	6111	fill 6120	-90
cell 6117	6112	fill 6120	-90
cell 6118	6113	fill 6120	-90

cell 6206	6201	fill 6120	-90
cell 6207	6202	fill 6120	-90
cell 6208	6203	fill 6120	-90
cell 6209	6204	fill 6120	-90
cell 6210	6205	fill 6120	-90

```

cell 6211 6206 fill 6120 -90
cell 6212 6207 fill 6120 -90
cell 6213 6208 fill 6120 -90
cell 6214 6209 fill 6120 -90
cell 6215 6210 fill 6120 -90
cell 6216 6211 fill 6120 -90
cell 6217 6212 fill 6120 -90
cell 6218 6213 fill 6120 -90

```

% Switch Directions 180 degrees

```

trans 6201 0 0 0 0 0 180
trans 6202 0 0 0 0 0 180
trans 6203 0 0 0 0 0 180
trans 6204 0 0 0 0 0 180
trans 6205 0 0 0 0 0 180
trans 6206 0 0 0 0 0 180
trans 6207 0 0 0 0 0 180
trans 6208 0 0 0 0 0 180
trans 6209 0 0 0 0 0 180
trans 6210 0 0 0 0 0 180
trans 6211 0 0 0 0 0 180
trans 6212 0 0 0 0 0 180
trans 6213 0 0 0 0 0 180

```

```

%%%%%%%%%
%%%%%%%%%

```

% Build Assembly to match universe sizes in STD assembly

```

%%%%%%%%%
%%%%%%%%%

```

```

cell 6120 6100 fill 6101 -11 % Steel Grid Plate + Aluminum bottom fitting
cell 6121 6100 fill 6102 11 -12 % Oct graphite XS region 1 -- bottom
cell 6122 6100 fill 6103 12 -13 % Oct graphite XS region 2 -- bottom
cell 6123 6100 fill 6104 13 -14 % square graphite bottom + air gap + Al clad
cell 6124 6100 fill 6105 14 -17 % axial interface
cell 6125 6100 fill 6106 17 -18 % Fuel1 bottom
cell 6126 6100 fill 6107 18 -19 % Fuel2
cell 6127 6100 fill 6108 19 -20 % Fuel1 top
cell 6128 6100 fill 6109 20 -23 % axial interface
cell 6129 6100 fill 6110 23 -25 % square graphite w hole top + Oct graphite with hole + air
+ Al clad
cell 6130 6100 fill 6111 25 -26 % Oct graphite XS region 2 -- top
cell 6131 6100 fill 6112 26 -27 % Oct graphite XS region 1 -- top
cell 6132 6100 fill 6113 27 % top fitting

```

% Copy but Reverse Direction

```

cell 6220 6200 fill 6201 -11 % Steel Grid Plate + Aluminum bottom fitting

```

```

cell 6221 6200 fill 6202      11 -12 % Oct graphite XS region 1 -- bottom
cell 6222 6200 fill 6203      12 -13 % Oct graphite XS region 2 -- bottom
cell 6223 6200 fill 6204      13 -14 % square graphite bottom + air gap + Al clad
cell 6224 6200 fill 6205      14 -17 % axial interface
cell 6225 6200 fill 6206      17 -18 % Fuel1 bottom
cell 6226 6200 fill 6207      18 -19 % Fuel2
cell 6227 6200 fill 6208      19 -20 % Fuel1 top
cell 6228 6200 fill 6209      20 -23 % axial interface
cell 6229 6200 fill 6210      23 -25 % square graphite w hole top + Oct graphite with hole +
air + Al clad
cell 6230 6200 fill 6211      25 -26 % Oct graphite XS region 2 -- top
cell 6231 6200 fill 6212      26 -27 % Oct graphite XS region 1 -- top
cell 6232 6200 fill 6213      27      % top fitting

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
% Debug Assembly
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
%
```

```
%include "/Users/bakeba/Desktop/HPC-Serpent/Assemblies/C/C1_Half-Slot.i"
```

```
%include "/Users/bakeba/Desktop/HPC-Serpent/Assemblies/DebugAssembly.i"
```

```
%cell 3 1 fill 6100 -5900
```

```
%
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% --- Geometry plots:
```

```

%plot 3 1000 1000  1.5  -5.08 5.08  -5.08  5.08      % xy-plot
%plot 3 1000 1000  2.0  -5.08 5.08  -5.08  5.08      % xy-plot
%plot 3 1000 1000 42.0  -5.08 5.08  -5.08  5.08      % xy-plot
%plot 3 1000 1000 59.0  -5.08 5.08  -5.08  5.08      % xy-plot
%plot 3 1000 1000 59.8  -5.08 5.08  -5.08  5.08      % xy-plot
%plot 3 1000 1000 186.7 -5.08 5.08  -5.08  5.08      % xy-plot
%plot 3 1000 1000 186.85 -5.08 5.08  -5.08  5.08      % xy-plot
%plot 3 1000 1000 222.0 -5.08 5.08  -5.08  5.08      % xy-plot
%plot 3 1000 1000 243.1 -5.08 5.08  -5.08  5.08      % xy-plot
%plot 3 1000 1000 247.1 -5.08 5.08  -5.08  5.08      % xy-plot
%plot 3 1000 1000 248.1 -5.08 5.08  -5.08  5.08      % xy-plot

```

```
%plot 2 800 4000  -5.0  -5.08 5.08  0.0  247.65      % yz-plot
```

```
%plot 2 800 4000  -4.0  -5.08 5.08  0.0  247.65      % yz-plot
```

```
%plot 2 800 4000  -3.0  -5.08 5.08  0.0  247.65      % yz-plot
```

```

%plot 2 800 4000 -2.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 -1.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 0.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 1.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 2.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 3.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 4.0 -5.08 5.08 0.0 247.65 % yz-plot
%plot 2 800 4000 5.0 -5.08 5.08 0.0 247.65 % yz-plot
%
%plot 1 800 4000 -5.0 -5.08 5.08 0.0 247.65 % xz-plot
%plot 1 800 4000 -4.0 -5.08 5.08 0.0 247.65 % xz-plot
%plot 1 800 4000 -3.0 -5.08 5.08 0.0 247.65 % xz-plot
%plot 1 800 4000 -2.0 -5.08 5.08 0.0 247.65 % xz-plot
%plot 1 800 4000 -1.0 -5.08 5.08 0.0 247.65 % xz-plot
%plot 1 800 4000 0.0 -5.08 5.08 0.0 247.65 % xz-plot
%plot 1 800 4000 1.0 -5.08 5.08 0.0 247.65 % xz-plot
%plot 1 800 4000 2.0 -5.08 5.08 0.0 247.65 % xz-plot
%plot 1 800 4000 3.0 -5.08 5.08 0.0 247.65 % xz-plot
%plot 1 800 4000 4.0 -5.08 5.08 0.0 247.65 % xz-plot
%plot 1 800 4000 5.0 -5.08 5.08 0.0 247.65 % xz-plot

```

M8Center_wDy-22R-fuel-region.sss

% TREAT M8-Calibration Vehicle

% Ben Baker

% Idaho National Laboratory

% Feb 2, 2016

% 4"x8" M8-Cal vehicle

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

% M8 VEHICLE

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

% Core CenterLine = 123.3105 cm

% Test Sample (Flux Wire 60" about core center line)

% U-Zr Sample 0.040" = 0.1016cm in diameter. R = 0.0508 cm

surf 9049 cyl 0.0 -5.08 0.0508 %62.82675 183.79425 %47.1105 % Radius of flux-wire

% Experiment Leg (Guess Center at x-y (0,-5.08))

surf 9050 cyl 0.0 -5.08 1.4224 % Stainless Steel Outer Tube I.D. (1.12" = 2.8448cm, R = 1.4224cm)

surf 9051 cyl 0.0 -5.08 1.5875 % SS Outer Tube O.D. (1.25" = 3.125 cm, R = 1.5875cm)

surf 9052 cyl 0.0 -5.08 1.63703 % SS Cal. Loop Test Section I.D. (1.289" = 3.27406cm, R = 1.63703cm)

surf 9053 cyl 0.0 -5.08 2.56921 % SS Cal. Loop Test Section O.D. (2.023" = 5.13842cm, R = 2.56921 cm)
surf 9054 cyl 0.0 -5.08 2.5781 % Al Sleeve I.D. (2.03" = 5.1562 cm, R = 2.5781 cm)
surf 9055 cyl 0.0 -5.08 2.7051 % Al Sleeve O.D. (2.13" = 5.4102 cm, R = 2.7051 cm)
also SS Sleeve I.D. (2.13"): Al-Part1,2,3 Length (14-3/4", 15", 10")
surf 9056 cyl 0.0 -5.08 2.86258 % SS Sleeve O.D. (2.254" = 5.72516 cm, R = 2.86258 cm) SS-Part1,2 Length (14-3/4", 15")
surf 9057 cyl 0.0 -5.08 2.86766 % SS & Dy collar: Part 6 (SS) O.D. (I.D. 2.254" OD = 2.258" = 5.73532 cm, R = 2.86766 cm) Length = 3.5" Lower 4" Upper, Same OD for initial Dy 0.002" thick
surf 9058 cyl 0.0 -5.08 2.90576 % SS & Dy Coller: O.D (I.D. 2.258" OD = 2.288" = 5.81152 cm, R = 2.90576 cm) SS Lengths = 6-3/4" (Both sides)
surf 9059 cyl 0.0 -5.08 2.91338 % SS & Dy Coller: (I.D. 2.288" OD = 2.294" = 5.82676 cm, R = 2.91338 cm) SS Lengths = 12" (Both Sides- Part 4)
surf 9060 cyl 0.0 -5.08 3.03022 % SS Dummy Heaters (I.D. 2.294" OD = 2.386" = 6.06044 cm, R = 3.03022 cm)

% Pump Leg (Guess Center at x-y (0,1.75" = 4.445cm))

surf 9061 cyl 0.0 4.445 1.063625 % Clamp says 1.464" OD and Pump Leg Flow meter Magnet 1.4375" OD. Assume 0.3" thick. Thus, R = 1.063625 cm
surf 9062 cyl 0.0 4.445 1.82563 % R = 1.82563 cm or OD 1.4375 use flow magnet"

% Axial regions for Experimental Leg

surf 9070 pz 21.7105 % Start of SS + Al support for Dy
surf 9071 pz 47.1105 % Lower End (Start of Dy full thickness)
surf 9072 pz 92.8305 % Lower End (Start of Dy 0.015 + 0.002" thick zone)
surf 9073 pz 106.1655 % Lower End (Start of Dy 0.002" thick)
surf 9074 pz 114.4205 % Lower End (End of Dy 0.002" thick)
surf 9075 pz 133.4705 % Upper End (Start of Dy 0.002" thick)
surf 9076 pz 140.4555 % Upper End (Start of Dy 0.015 + 0.002" thick)
surf 9077 pz 153.7905 % Upper End (Start of Dy 0.02" thick)
surf 9078 pz 198.2405 % Upper End (End of Dy and everything else up to Al)

% Calibration Vehicle Container

surf 9079 cuboid -4.7117 4.7117 -9.7917 9.7917 0.3175 255.289250 %258.148965 % Assume 1/8" thick steel (0.3175cm)
surf 9080 cuboid -5.02920 5.02920 -10.1092 10.1092 0.0 255.289250 %258.148965 % Outside of can
surf 9081 cuboid -5.08 5.08 -10.16 10.16 0.0 258.148965 % Cuboid must match definition for 19x19 lat cuboid or greater

% M8 Cal Vehicle

surf 9099 cuboid -5.08 5.08 -10.16 10.16 0.0 500.0

%%%%%%%%%

% Test Leg (Mainly in Order)

[illegible]

%surf 9047 pz 62.85 % Bottom of fuel pin
 %surf 9048 pz 183.75 % Top of fuel pin

cell 9179 9136 air_fuel1 17 -20 % 9047 -9048
 cell 9181 9136 air -17 % -9047
 cell 9182 9136 air 20 % 9048

%%
 %%%

% Common Internals (Level 5)

%%
 %%%

cell 9151 9128 fill 9136 -9050 % Air inside tube + fuel pin (Dispersed pin)
 cell 9152 9128 steel -9051 9050 % SS Cal Test Outer Tube
 cell 9153 9128 air -9052 9051 % Air gap
 cell 9154 9128 steel -9053 9052 % SS Cal Loop Test Section (Extends all
 the way)

cell 9155 9128 air 9053 % Inf Air outside

%%
 %%%

% Common Al + Steel shells (shells Al + steel all the way out) (Level 4)

%%
 %%%

cell 9156 9129 fill 9128 -9054 % Common Internals

cell 9157 9129 aluminum -9055 9054 % Al cylinder

cell 9158 9129 steel 9055 % Steel

%%
 %%%

% Inner Tube (Level 3)

%%
 %%%

cell 9160 9137 fill 9128 -90 % Need to move back an extra level to align with others

cell 9162 9130 fill 9137 -90

%%
 %%%

% Al Tube Empty (Level 3)

%%
 %%%

cell 9161 9131 fill 9129 -90

%%
 %%%

% First Dy region - Bottom (0.02" thick) (Level 3)

%%
 %%%

cell 9163 9132 fill 9129 -9056 % Common Internals

cell 9164 9132 Dy -9059 9056 % CHANGE FROM Dy layer

```

cell 9165 9132 steel          9059          % Steel outer layer
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%          Second Dy region - Bottom (0.002" + 0.015" thick) (Level 3)
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
cell 9168 9133 fill 9129 -9056          % Common Internals
cell 9169 9133 Dy      -9058 9056          % CHANGE FROM Dy layer
cell 9170 9133 steel      9058          % Steel outer layer
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%          Third Dy region - Bottom (0.002" thick) (Level 3)
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
cell 9173 9134 fill 9129 -9056          % Common Internals
cell 9174 9134 Dy      -9057 9056          % CHANGED FROM Dy layer
cell 9175 9134 steel      9057          % Steel outer layer
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%          Space between regions (Steel) (Level 3)
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
cell 9178 9135 fill 9129 -90          % Common Internals

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%          Build Experiment Leg (Level 2 & 1)
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% XS generattion -- axial partition
cell 9101 9101 Al_steel -90
cell 9102 9102 fill 9130 -90
cell 9103 9103 fill 9131 -90
cell 9104 9104 fill 9131 -90
cell 9105 9105 fill 9132 -90
cell 9106 9106 fill 9132 -90
cell 9107 9107 fill 9132 -90
cell 9108 9108 fill 9132 -90
cell 9109 9109 fill 9132 -90
cell 9110 9110 fill 9133 -90
cell 9111 9111 fill 9134 -90
cell 9112 9112 fill 9135 -90
cell 9113 9113 fill 9134 -90
cell 9114 9114 fill 9133 -90
cell 9115 9115 fill 9132 -90
cell 9116 9116 fill 9132 -90

```

cell 9117 9117 fill 9132 -90
 cell 9118 9118 fill 9132 -90
 cell 9119 9119 fill 9130 -90
 cell 9120 9120 fill 9130 -90
 cell 9121 9121 fill 9130 -90
 cell 9122 9122 Al_air -90

cell 9125 9100 fill 9101	-11	% Steel Grid Plate + Aluminum bottom fitting
cell 9126 9100 fill 9102	11 -9070	% Common Internals (Begin Al + shells)
cell 9127 9100 fill 9103	9070 -12	% ref1 + Normal Pipe
cell 9128 9100 fill 9104	12 -9071	% Start Dy + Test_begin
cell 9129 9100 fill 9105	9071 -13	% ref2 + Dy (0.2" thick) + Test
cell 9130 9100 fill 9106	13 -14	% ref3 + Dy (0.2") + Test
cell 9131 9100 fill 9107	14 -17	% Al + Dy (0.2") + Test
cell 9132 9100 fill 9108	17 -18	% Fuel1+ Dy (0.2") + Test
cell 9133 9100 fill 9109	18 -9072	% Fuel2+ Start Dy (0.017")+ Test
cell 9134 9100 fill 9110	9072 -9073	% Fuel2 + End Dy(0.017") + Test
cell 9135 9100 fill 9111	9073 -9074	% Fuel2 + End Dy(0.002") + Test
cell 9136 9100 fill 9112	9074 -9075	% Fuel2 + Steel Zone + Test
cell 9137 9100 fill 9113	9075 -9076	% Fuel2 + Dy(0.002") + Test
cell 9138 9100 fill 9114	9076 -9077	% Fuel2 + Dy(0.017") + Test
cell 9139 9100 fill 9115	9077 -19	% Fuel2_end + Dy(0.02") + Test
cell 9140 9100 fill 9116	19 -20	% Fuel3_end+ Dy(0.02") + Test
cell 9141 9100 fill 9117	20 -23	% Al + Dy(0.02") + Test
cell 9142 9100 fill 9118	23 -9078	% Ref3_start+ Dy_end + Test_end
cell 9143 9100 fill 9119	9078 -25	% Ref3_end + Normal Pipe
cell 9144 9100 fill 9120	25 -26	% Ref2
cell 9145 9100 fill 9121	26 -27	% Ref1
cell 9146 9100 fill 9122	27	% top fitting

%%
 %%%

% Pump Leg

%%
 %%%

cell 9250 9250 air -9061 % Inside of pump leg

cell 9251 9250 steel 9061 % Steel cladding

%%
 %%%

% Build Pump Leg

%%
 %%%

cell 9201 9201 Al_steel -90

cell 9202 9202 fill 9250 -90

cell 9203 9203 fill 9250 -90

cell 9204 9204 fill 9250 -90

cell 9205 9205 fill 9250 -90
 cell 9206 9206 fill 9250 -90
 cell 9207 9207 fill 9250 -90
 cell 9208 9208 fill 9250 -90
 cell 9209 9209 fill 9250 -90
 cell 9210 9210 fill 9250 -90
 cell 9211 9211 fill 9250 -90
 cell 9212 9212 fill 9250 -90
 cell 9213 9213 fill 9250 -90
 cell 9214 9214 fill 9250 -90
 cell 9215 9215 fill 9250 -90
 cell 9216 9216 fill 9250 -90
 cell 9217 9217 fill 9250 -90
 cell 9218 9218 fill 9250 -90
 cell 9219 9219 fill 9250 -90
 cell 9220 9220 fill 9250 -90
 cell 9221 9221 fill 9250 -90
 cell 9222 9222 Al_air -90

cell 9225 9200 fill 9201 -11 % Steel Grid Plate + Aluminum bottom fitting
 cell 9226 9200 fill 9202 11 -9070 % Common Internals (Begin Al + shells)
 cell 9227 9200 fill 9203 9070 -12 % ref1 + Normal Pipe
 cell 9228 9200 fill 9204 12 -9071 % Start Dy + Test_begin
 cell 9229 9200 fill 9205 9071 -13 % ref2 + Dy (0.2" thick) + Test
 cell 9230 9200 fill 9206 13 -14 % ref3 + Dy (0.2") + Test
 cell 9231 9200 fill 9207 14 -17 % Al + Dy (0.2") + Test
 cell 9232 9200 fill 9208 17 -18 % Fuel1+ Dy (0.2") + Test
 cell 9233 9200 fill 9209 18 -9072 % Fuel1+ Start Dy (0.017")+ Test
 cell 9234 9200 fill 9210 9072 -9073 % Fuel1 + End Dy(0.017") + Test
 cell 9235 9200 fill 9211 9073 -9074 % Fuel1 + End Dy(0.002") + Test
 cell 9236 9200 fill 9212 9074 -9075 % Fuel1 + Steel Zone + Test
 cell 9237 9200 fill 9213 9075 -9076 % Fuel1 + Dy(0.002") + Test
 cell 9238 9200 fill 9214 9076 -9077 % Fuel1 + Dy(0.017") + Test
 cell 9239 9200 fill 9215 9077 -19 % Fuel1_end + Dy(0.02") + Test
 cell 9240 9200 fill 9216 19 -20 % Fuel2_end+ Dy(0.02") + Test
 cell 9241 9200 fill 9217 20 -23 % Al + Dy(0.02") + Test
 cell 9242 9200 fill 9218 23 -9078 % Ref3_start+ Dy_end + Test_end
 cell 9243 9200 fill 9219 9078 -25 % Ref3_end + Normal Pipe
 cell 9244 9200 fill 9220 25 -26 % Ref2
 cell 9245 9200 fill 9221 26 -27 % Ref1
 cell 9246 9200 fill 9222 27 % top fitting

%%%%%%%%%%%
 %%%%%%%%%%

% Air Between pump and experiment legs and vehicle clad

```

%%%%%%%%%
%%%%%%%%%
% cell 9350 9350 fuel2 -90 % replace air with fuel

```

```

cell 9301 9301 Al_steel -90
cell 9302 9302 air -90
cell 9303 9303 air -90
cell 9304 9304 air -90
cell 9305 9305 air -90
cell 9306 9306 air -90
cell 9307 9307 air -90
cell 9308 9308 air -90
cell 9309 9309 air -90
cell 9310 9310 air -90
cell 9311 9311 air -90
cell 9312 9312 air -90
cell 9313 9313 air -90
cell 9314 9314 air -90
cell 9315 9315 air -90
cell 9316 9316 air -90
cell 9317 9317 air -90
cell 9318 9318 air -90
cell 9319 9319 air -90
cell 9320 9320 air -90
cell 9321 9321 air -90
cell 9322 9322 Al_air -90

```

```

cell 9325 9300 fill 9301 -11 % Steel Grid Plate + Aluminum bottom fitting
cell 9326 9300 fill 9302 11 -9070 % Common Internals (Begin Al + shells)
cell 9327 9300 fill 9303 9070 -12 % ref1 + Normal Pipe
cell 9328 9300 fill 9304 12 -9071 % Start Dy + Test_begin
cell 9329 9300 fill 9305 9071 -13 % ref2 + Dy (0.2" thick) + Test
cell 9330 9300 fill 9306 13 -14 % ref3 + Dy (0.2") + Test
cell 9331 9300 fill 9307 14 -17 % Al + Dy (0.2") + Test
cell 9332 9300 fill 9308 17 -18 % Fuel1+ Dy (0.2") + Test
cell 9333 9300 fill 9309 18 -9072 % Fuel1+ Start Dy (0.017")+ Test
cell 9334 9300 fill 9310 9072 -9073 % Fuel1 + End Dy(0.017") + Test
cell 9335 9300 fill 9311 9073 -9074 % Fuel1 + End Dy(0.002") + Test
cell 9336 9300 fill 9312 9074 -9075 % Fuel1 + Steel Zone + Test
cell 9337 9300 fill 9313 9075 -9076 % Fuel1 + Dy(0.002") + Test
cell 9338 9300 fill 9314 9076 -9077 % Fuel1 + Dy(0.017") + Test
cell 9339 9300 fill 9315 9077 -19 % Fuel1_end + Dy(0.02") + Test
cell 9340 9300 fill 9316 19 -20 % Fuel2_end+ Dy(0.02") + Test
cell 9341 9300 fill 9317 20 -23 % Al + Dy(0.02") + Test
cell 9342 9300 fill 9318 23 -9078 % Ref3_start+ Dy_end + Test_end
cell 9343 9300 fill 9319 9078 -25 % Ref3_end + Normal Pipe

```

cell 9344 9300 fill 9320	25 -26	% Ref2
cell 9345 9300 fill 9321	26 -27	% Ref1
cell 9346 9300 fill 9322	27	% top fitting

%%%%%%%%%
 %%%%%%%%%

% Steel Frame on Cal Vehicle

%%%%%%%%%
 %%%%%%%%%

cell 9451 9450 steel	-9080	% Steel Walls
cell 9452 9450 air_out	9080	% Air outside of walls

cell 9401 9401 Al_steel	-90
cell 9402 9402 fill 9450	-90
cell 9403 9403 fill 9450	-90
cell 9404 9404 fill 9450	-90
cell 9405 9405 fill 9450	-90
cell 9406 9406 fill 9450	-90
cell 9407 9407 fill 9450	-90
cell 9408 9408 fill 9450	-90
cell 9409 9409 fill 9450	-90
cell 9410 9410 fill 9450	-90
cell 9411 9411 fill 9450	-90
cell 9412 9412 fill 9450	-90
cell 9413 9413 fill 9450	-90
cell 9414 9414 fill 9450	-90
cell 9415 9415 fill 9450	-90
cell 9416 9416 fill 9450	-90
cell 9417 9417 fill 9450	-90
cell 9418 9418 fill 9450	-90
cell 9419 9419 fill 9450	-90
cell 9420 9420 fill 9450	-90
cell 9421 9421 fill 9450	-90
cell 9422 9422 Al_air	-90

cell 9425 9400 fill 9401	-11	% Steel Grid Plate + Aluminum bottom fitting
cell 9426 9400 fill 9402	11 -9070	% Common Internals (Begin Al + shells)
cell 9427 9400 fill 9403	9070 -12	% ref1 + Normal Pipe
cell 9428 9400 fill 9404	12 -9071	% Start Dy + Test_begin
cell 9429 9400 fill 9405	9071 -13	% ref2 + Dy (0.2" thick) + Test
cell 9430 9400 fill 9406	13 -14	% ref3 + Dy (0.2") + Test
cell 9431 9400 fill 9407	14 -17	% Al + Dy (0.2") + Test
cell 9432 9400 fill 9408	17 -18	% Fuel1+ Dy (0.2") + Test
cell 9433 9400 fill 9409	18 -9072	% Fuel1+ Start Dy (0.017")+ Test
cell 9434 9400 fill 9410	9072 -9073	% Fuel1 + End Dy(0.017") + Test

```

cell 9435 9400 fill 9411    9073 -9074 % Fuel1 + End Dy(0.002") + Test
cell 9436 9400 fill 9412    9074 -9075 % Fuel1 + Steel Zone    + Test
cell 9437 9400 fill 9413    9075 -9076 % Fuel1 + Dy(0.002")    + Test
cell 9438 9400 fill 9414    9076 -9077 % Fuel1 + Dy(0.017")    + Test
cell 9439 9400 fill 9415    9077 -19  % Fuel1_end + Dy(0.02")    + Test
cell 9440 9400 fill 9416    19 -20  % Fuel2_+end+ Dy(0.02")    + Test
cell 9441 9400 fill 9417    20 -23  % Al    + Dy(0.02")    + Test
cell 9442 9400 fill 9418    23 -9078 % Ref3_start+ Dy_end    + Test_end
cell 9443 9400 fill 9419    9078 -25  % Ref3_end + Normal Pipe
cell 9444 9400 fill 9420    25 -26  % Ref2
cell 9445 9400 fill 9421    26 -27  % Ref1
cell 9446 9400 fill 9422    27      % top fitting

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
% Build Entire Assembly
```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```

cell 9070 9000 fill 9100    -9079 -9060          % Exp leg
cell 9071 9000 fill 9200    -9079 -9062          % pump leg
cell 9072 9000 fill 9300    -9079 9060 9062      % air inside vehicle
cell 9073 9000 fill 9400      9079          % veh wall

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
% Run Parameters
```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
%set micro egl
```

```

%ene egl 1 1.00000E-11 2.00100E-08 4.73020E-08 7.64970E-08 2.09610E-07 6.25000E-07
8.100030E-06

```

```
%          1.32700E-04 3.48110E-03 1.15620E-01 3.32870E+00 2.00000E+01
```

```
%
```

```
%set gcu 9101 9201 9301 9401
```

```
%          9102 9202 9302 9402
```

```
%          9103 9203 9303 9403
```

```
%          9104 9204 9304 9404
```

```
%          9105 9205 9305 9405
```

```
%          9106 9206 9306 9406
```

```
%          9107 9207 9307 9407
```

```
%          9108 9208 9308 9408
```

```
%          9109 9209 9309 9409
```

```
%          9110 9210 9310 9410
```

```
%          9111 9211 9311 9411
```

```
%          9112 9212 9312 9412
```

```

%          9113 9213 9313 9413
%          9114 9214 9314 9414
%          9115 9215 9315 9415
%          9116 9216 9316 9416
%          9117 9217 9317 9417
%          9118 9218 9318 9418
%          9119 9219 9319 9419
%          9120 9220 9320 9420
%          9121 9221 9321 9421
%          9122 9222 9322 9422
%
%set blockdt Dy
%
%set nfg 11 2.00100E-08 4.73020E-08 7.64970E-08 2.09610E-07 6.25000E-07 8.100030E-06
1.32700E-04 3.48110E-03 1.15620E-01 3.32870E+00
%
%det Flux du 0 de eg1 dx -0.7112 0.7112 1 dy -5.7912 -4.3688 1 dz 62.826700 183.7942500
40 % ~every 3 cm

%% Power in fuel zone
%det 1 du 0 dm fuel dx -5.08 5.08 1 dy -10.16 10.16 1 dz 62.8267500 82.8267500 2 dr -8
void % fuel region 1
%det 2 du 0 dm fuel dx -5.08 5.08 1 dy -10.16 10.16 1 dz 82.8267500 92.83058 1 dr -8
void % fuel region 2
%det 3 du 0 dm fuel dx -5.08 5.08 1 dy -10.16 10.16 1 dz 92.83058 106.1655 1 dr -8
void % fuel region 2
%det 4 du 0 dm fuel dx -5.08 5.08 1 dy -10.16 10.16 1 dz 106.1655 114.4205 1 dr -8
void % fuel region 2
%det 5 du 0 dm fuel dx -5.08 5.08 1 dy -10.16 10.16 1 dz 114.4205 133.4705 2 dr -8
void % fuel region 2
%det 6 du 0 dm fuel dx -5.08 5.08 1 dy -10.16 10.16 1 dz 133.4705 140.4555 1 dr -8
void % fuel region 2
%det 7 du 0 dm fuel dx -5.08 5.08 1 dy -10.16 10.16 1 dz 140.4555 153.7905 1 dr -8
void % fuel region 2
%det 8 du 0 dm fuel dx -5.08 5.08 1 dy -10.16 10.16 1 dz 153.7905 163.79425 1 dr -8
void % fuel region 2
%det 9 du 0 dm fuel dx -5.08 5.08 1 dy -10.16 10.16 1 dz 163.79425 183.79425 2 dr -8
void % fuel region 1
%
%% Power in experiment zone
%det 11 du 0 dm air_fuel1 dx -1.4225 1.4225 1 dy -6.5025 -3.6577 1 dz 62.8267500
82.8267500 2 dr -8 void % fuel region 1
%det 12 du 0 dm air_fuel1 dx -1.4225 1.4225 1 dy -6.5025 -3.6577 1 dz 82.8267500
92.83058 1 dr -8 void % fuel region 2
%det 13 du 0 dm air_fuel1 dx -1.4225 1.4225 1 dy -6.5025 -3.6577 1 dz 92.83058
106.1655 1 dr -8 void % fuel region 2

```

```
%det 14 du 0 dm air_fuel1 dx -1.4225 1.4225 1 dy -6.5025 -3.6577 1 dz 106.1655
114.4205 1 dr -8 void % fuel region 2
%det 15 du 0 dm air_fuel1 dx -1.4225 1.4225 1 dy -6.5025 -3.6577 1 dz 114.4205
133.4705 2 dr -8 void % fuel region 2
%det 16 du 0 dm air_fuel1 dx -1.4225 1.4225 1 dy -6.5025 -3.6577 1 dz 133.4705
140.4555 1 dr -8 void % fuel region 2
%det 17 du 0 dm air_fuel1 dx -1.4225 1.4225 1 dy -6.5025 -3.6577 1 dz 140.4555
153.7905 1 dr -8 void % fuel region 2
%det 18 du 0 dm air_fuel1 dx -1.4225 1.4225 1 dy -6.5025 -3.6577 1 dz 153.7905
163.79425 1 dr -8 void % fuel region 2
%det 19 du 0 dm air_fuel1 dx -1.4225 1.4225 1 dy -6.5025 -3.6577 1 dz 163.79425
183.79425 2 dr -8 void % fuel region 1
```

```
%plot 3 500 500 82.83 -1.4225 1.4225 -6.5025 -3.6577
%plot 1 2500 6000 0 -10.16 10.16 0 250
%plot 3 500 1000 82.83 -5.08 5.08 -10.16 10.16
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
%% Debug Assembly
```

```
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```
%%
```

```
%%
```

```
%cell 1 0 fill 9000 -9099 % surf 5900 4"x4" and surf 9099 for 4"x8"
```

```
%cell 2 0 outside 9099 % Outside of cladding
```

```
%
```

```
%% Surfaces
```

```
%include "surfaces_new.inp"
```

```
%
```

```
%% Materials
```

```
%include "mat_Ben.inp"
```

```
%
```

```
%% --- Cross section library file path:
```

```
%%set acelib "/Users/ortej/CODES/SERPENT/xsdata/ser_xmdir_endfb7.r1"
```

```
%%set acelib "/home/ortej/SERPENT/data/ENDFB-VII.r1/ser_xmdir_endfb7.r1"
```

```
%set acelib "/Users/bakeba/Desktop/Serpent2/SerpentData/ser_xmdir_desktop"
```

```
%
```

```
%% --- Reflective boundary condition (1-black, 2-reflective , 3-periodic):
```

```
%set bc 2 2 1
```

```
%
```

```
%% estimators use (0/1 0 - collision 1- track-length)
```

```
%% if 1 dt is switched off
```

```
%set tle 0
```

```
%
```

```
%% --- Neutron population and criticality cycles:
```

```

%set pop 1000000 800 50
%set nbuf 7
%
%
%
%
%
%
% --- Geometry and mesh plots:
%plot 3 1000 1000 2.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 7.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 42.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 50.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 57.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 59.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 59.48 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 62.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 72.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 82.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 184.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 187.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 187.18 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 188.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 196.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 208.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 243.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 247.0 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 248.0 -10.16 10.16 -10.16 10.16 % xy-plot
%
%plot 1 1000 2000 0.0 -10.16 10.16 -10.0 250.65 % xz-plot
M8Center-Transient-Prescription.sss
% TREAT M8-Calibration Vehicle

% Ben Baker
% Idaho National Laboratory
% Feb 2, 2016
% 4"x8" M8-Cal vehicle

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% M8 VEHICLE
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Core CenterLine = 123.3105 cm

% Test Sample (Flux Wire 60" about core center line)
% U-Zr Sample 0.040" = 0.1016cm in diameter. R = 0.0508 cm
% surf 9049 cyl 0.0 5.08 0.0508 %62.82675 183.79425 %47.1105 % Radius of flux-wire

```

% Experiment Leg (Guess Center at x-y (0,-5.08))

surf 9050 cyl 0.0 5.08 1.4224	% Stainless Steel Outer Tube I.D. (1.12" = 2.8448cm, R = 1.4224cm)
surf 9051 cyl 0.0 5.08 1.5875	% SS Outer Tube O.D. (1.25" = 3.125 cm, R = 1.5875cm)
surf 9052 cyl 0.0 5.08 1.63703	% SS Cal. Loop Test Section I.D. (1.289" = 3.27406cm, R = 1.63703cm)
surf 9053 cyl 0.0 5.08 2.56921	% SS Cal. Loop Test Section O.D. (2.023" = 5.13842cm, R = 2.56921 cm)
surf 9054 cyl 0.0 5.08 2.5781	% Al Sleeve I.D. (2.03" = 5.1562 cm, R = 2.5781 cm)
surf 9055 cyl 0.0 5.08 2.7051	% Al Sleeve O.D. (2.13" = 5.4102 cm, R = 2.7051 cm)
also SS Sleeve I.D. (2.13"): Al-Part1,2,3 Length (14-3/4",15",10")	
surf 9056 cyl 0.0 5.08 2.86258	% SS Sleeve O.D. (2.254" = 5.72516 cm, R = 2.86258 cm) SS-Part1,2 Length (14-3/4", 15")
surf 9057 cyl 0.0 5.08 2.86766	% SS & Dy collar: Part 6 (SS) O.D. (I.D. 2.254" OD = 2.258" = 5.73532 cm, R = 2.86766 cm) Length = 3.5" Lower 4" Upper, Same OD for initial Dy 0.002" thick
surf 9058 cyl 0.0 5.08 2.90576	% SS & Dy Coller: O.D (I.D. 2.258" OD = 2.288" = 5.81152 cm, R = 2.90576 cm) SS Lengths = 6-3/4" (Both sides)
surf 9059 cyl 0.0 5.08 2.91338	% SS & Dy Coller: (I.D. 2.288" OD = 2.294" = 5.82676 cm, R = 2.91338 cm) SS Lengths = 12" (Both Sides- Part 4)
surf 9060 cyl 0.0 5.08 3.03022	% SS Dummy Heaters (I.D. 2.294" OD = 2.386" = 6.06044 cm, R = 3.03022 cm)

% Pump Leg (Guess Center at x-y (0,1.75" = 4.445cm))

surf 9061 cyl 0.0 -4.445 1.063625	% Clamp says 1.464" OD and Pump Leg Flow meter Magnet 1.4375" OD. Assume 0.3" thick. Thus, R = 1.063625 cm
surf 9062 cyl 0.0 -4.445 1.82563	% R = 1.82563 cm or OD 1.4375 use flow magnet"

% Axial regions for Experimental Leg

surf 9070 pz 21.7105	% Start of SS + Al support for Dy
surf 9071 pz 47.1105	% Lower End (Start of Dy full thickness)
surf 9072 pz 92.8305	% Lower End (Start of Dy 0.015 + 0.002" thick zone)
surf 9073 pz 106.1655	% Lower End (Start of Dy 0.002" thick)
surf 9074 pz 114.4205	% Lower End (End of Dy 0.002" thick)
surf 9075 pz 133.4705	% Upper End (Start of Dy 0.002" thick)
surf 9076 pz 140.4555	% Upper End (Start of Dy 0.015 + 0.002" thick)
surf 9077 pz 153.7905	% Upper End (Start of Dy 0.02" thick)
surf 9078 pz 198.2405	% Upper End (End of Dy and everything else up to Al)

% Calibration Vehicle Container

surf 9079 cuboid -4.7117 4.7117 -9.7917 9.7917 0.3175 255.289250 %258.148965	% Assume 1/8" thick steel (0.3175cm)
surf 9080 cuboid -5.02920 5.02920 -10.1092 10.1092 0.0 255.289250 %258.148965	% Outside of can

surf 9081 cuboid -5.08 5.08 -10.16 10.16 0.0 258.148965 % Cuboid must match definition
for 19x19 lat cuboid or greater

```

%%%%%%%%%%
% Test Leg (Mainly in Order)
%
%
%      xxxxxxxxxxxx Al_air
%      x x  Common Internals
%      x x  "
%      x x  Common Internals
%      xxx w xxx End Dy and Al (0.02")
%      xxx w xxx Dy (0.02")
%      xxx w xxx Dy (0.02")
%      xxx w xxx Step up to Dy (0.02")
%      xx w xx  Dy (0.017")
%      xx w xx  Dy (0.017")
%      xx w xx  Step up to Dy (0.017")
%      x w x    Dy (0.002")
%      x w x    Step up to Dy (0.002")
%      -x w x-  Steel
%      x w x    Dy (0.002")
%      x w x    Step down to Dy (0.002")
%      xx w xx  Dy (0.017")
%      xx w xx  Dy (0.017")
%      xx w xx  Step down to Dy (0.017")
%      xxx w xxx Dy (0.02")
%      xxx w xxx Dy (0.02")
%      xxx w xxx Dy (0.02")
%      xxx w xxx Start Dy (0.02") and wire
%      xxx  xxx Al + Steel (No Dy)
%      xxx  xxx Start Al (No Dy)
%      x x    Common Internals
%      x x    "
%      x x    Common Internals
%      xxxxxxxxxxxx Al_steel
%
%%%%%%%%%%
%      INF top and bottom
%%%%%%%%%%
% Infinite Aluminum base
%cell 9098 9098 Al_steel -90          % Solid base - INF down and INF across
%cell 9099 9099 Al_air -90           % Solid base - INF down and INF across

```

%%
 %%%

% Experiment Region

%%
 %%%

% Wire Diameter = 0.0625cm

% Wire holder titanium Diameter = 0.635 cm

%%
 %%%

% Core Axial CenterLine = 123.3105 cm (Ref for Holes)

%%
 %%%

% Increase Length of DU wires from 0.5cm to 2cm for stats, centered on DU position.

% Position A Centered 18inch above Centerline

% Position B Centered 5.13inch above Centerline

% Position C Centered 0.25inch below Centerline

% Position D Centered 5.38inch below Centerline

% Position E Centered 18inch below Centerline

% Du is centered 1cm below Position Centers

% CoAl is centered 0.5cm below Position Centers

% Nb is centered at Position Centers

% Ti is centered 0.5cm above Position Centers

% Fe is centered 1cm above Position Centers

% Surface Tracking (Use 2cm for each wire)

% Radius Z1 Z2

surf 9082 cyl 0.0 5.08 1.4224 169.0305 247.2625

surf 9083 cyl 0.0 5.08 1.4224 167.0305 169.0305 % Wire A

surf 9084 cyl 0.0 5.08 1.4224 136.3407 167.0305

surf 9085 cyl 0.0 5.08 1.4224 134.3407 136.3407 % Wire B

surf 9086 cyl 0.0 5.08 1.4224 122.6755 134.3407

surf 9087 cyl 0.0 5.08 1.4224 120.6755 122.6755 % Wire C

surf 9088 cyl 0.0 5.08 1.4224 109.6453 120.6755

surf 9089 cyl 0.0 5.08 1.4224 107.6453 109.6453 % Wire D

surf 9090 cyl 0.0 5.08 1.4224 77.5905 107.6453

surf 9091 cyl 0.0 5.08 1.4224 75.5905 77.5905 % Wire E

surf 9092 cyl 0.0 5.08 1.4224 3.486 75.5905

cell 9048 9112 fill 9013 27

cell 9049 9112 fill 9012 -9082

cell 9050 9112 fill 9011 -9083 % Wire A

cell 9051 9112 fill 9010 -9084
 cell 9052 9112 fill 9009 -9085 % Wire B
 cell 9053 9112 fill 9008 -9086
 cell 9054 9112 fill 9007 -9087 % Wire C
 cell 9055 9112 fill 9006 -9088
 cell 9056 9112 fill 9005 -9089 % Wire D
 cell 9057 9112 fill 9004 -9090
 cell 9058 9112 fill 9003 -9091 % Wire E
 cell 9059 9112 fill 9002 -9092
 cell 9060 9112 fill 9001 -11

cell 9061 9013 Al_air -90
 cell 9062 9012 WireHolder -90
 cell 9063 9011 FissionWire -90
 cell 9064 9010 WireHolder -90
 cell 9065 9009 FissionWire -90
 cell 9066 9008 WireHolder -90
 cell 9067 9007 FissionWire -90
 cell 9068 9006 WireHolder -90
 cell 9069 9005 FissionWire -90
 cell 9070 9004 WireHolder -90
 cell 9071 9003 FissionWire -90
 cell 9072 9002 WireHolder -90
 cell 9073 9001 Al_steel -90

%%
 %%%

% Common Al + Steel shells (shells Al + steel all the way out) (Level 4)

%%
 %%%

cell 9082 9115 steel -9051 9050 % SS Cal Test Outer Tube
 cell 9083 9115 air -9052 9051 % Air gap
 cell 9084 9115 steel -9053 9052 % SS Cal Loop Test Section (Extends all
 the way)
 cell 9085 9115 air -9054 9053 % Inf Air outside
 cell 9087 9115 aluminum -9055 9054 % Al cylinder
 cell 9088 9115 steel 9055 % Steel

%%
 %%%

% HOMOGENIZATION REGIONS outside the wire radius 1.4224

%%
 %%%
 %%%
 %%%

% Bottom fitting

%%%%%%%%%%
 %%%%%%%%%%
 cell 9151 9119 Al_steel -90 % bottom fitting
 %%%%%%%%%%
 %%%%%%%%%%
 % Inner Tube (Level 3)
 %%%%%%%%%%
 %%%%%%%%%%
 cell 9152 9120 steel -9051 9050 % SS Cal Test Outer Tube
 cell 9153 9120 air -9052 9051 % Air gap
 cell 9154 9120 steel -9053 9052 % SS Cal Loop Test Section (Extends all
 the way)
 cell 9155 9120 air 9053 % Inf Air outside
 %%%%%%%%%%
 %%%%%%%%%%
 % Al Tube Empty (Level 3)
 %%%%%%%%%%
 %%%%%%%%%%
 cell 9161 9121 fill 9115 -90
 %%%%%%%%%%
 %%%%%%%%%%
 % First Dy region - Bottom (0.02" thick) (Level 3)
 %%%%%%%%%%
 %%%%%%%%%%
 cell 9163 9122 fill 9115 -9056 % Common Internals
 cell 9164 9122 Dy -9059 9056 % CHANGE FROM Dy layer
 cell 9165 9122 steel 9059 % Steel outer layer
 %%%%%%%%%%
 %%%%%%%%%%
 % Second Dy region - Bottom (0.002" + 0.015" thick) (Level 3)
 %%%%%%%%%%
 %%%%%%%%%%
 cell 9168 9123 fill 9115 -9056 % Common Internals
 cell 9169 9123 Dy -9058 9056 % CHANGE FROM Dy layer
 cell 9170 9123 steel 9058 % Steel outer layer
 %%%%%%%%%%
 %%%%%%%%%%
 % Third Dy region - Bottom (0.002" thick) (Level 3)
 %%%%%%%%%%
 %%%%%%%%%%
 cell 9173 9124 fill 9115 -9056 % Common Internals
 cell 9174 9124 Dy -9057 9056 % CHANGED FROM Dy layer
 cell 9175 9124 steel 9057 % Steel outer layer
 %%%%%%%%%%
 %%%%%%%%%%
 % Space between regions (Steel) (Level 3)

```

%%%%%%%%%
%%%%%%%%%
cell 9178 9125 fill 9115   -90                                % Common Internals
%%%%%%%%%
%%%%%%%%%
%                               Top fitting
%%%%%%%%%
%%%%%%%%%
cell 9179 9126 Al_air   -90                                % top fitting
%%%%%%%%%
%%%%%%%%%
%                               PUT BOTH HOMOGENIZATION REGIONS TOGETHER
%%%%%%%%%
%%%%%%%%%
%                               bottom fitting
%%%%%%%%%
%%%%%%%%%
cell 9180 9129 fill 9112 -9050
cell 9181 9129 fill 9119  9050
%%%%%%%%%
%%%%%%%%%
%                               Inner Tube      (Level 3)
%%%%%%%%%
%%%%%%%%%
cell 9182 9130 fill 9112 -9050
cell 9183 9130 fill 9120  9050
%%%%%%%%%
%%%%%%%%%
%                               Al Tube Empty   (Level 3)
%%%%%%%%%
%%%%%%%%%
cell 9185 9131 fill 9112 -9050
cell 9186 9131 fill 9121  9050
%%%%%%%%%
%%%%%%%%%
%                               First Dy region - Bottom (0.02" thick) (Level 3)
%%%%%%%%%
%%%%%%%%%
cell 9188 9132 fill 9112 -9050
cell 9189 9132 fill 9122  9050
%%%%%%%%%
%%%%%%%%%
%                               Second Dy region - Bottom (0.002" + 0.015" thick) (Level 3)

```

%%%%%%%%%
 %%%%%%%%%

cell 9190 9133 fill 9112 -9050

cell 9192 9133 fill 9123 9050

%%%%%%%%%
 %%%%%%%%%

% Third Dy region - Bottom (0.002" thick) (Level 3)

%%%%%%%%%
 %%%%%%%%%

cell 9194 9134 fill 9112 -9050

cell 9195 9134 fill 9124 9050

%%%%%%%%%
 %%%%%%%%%

% Space between regions (Steel) (Level 3)

%%%%%%%%%
 %%%%%%%%%

cell 9198 9135 fill 9112 -9050

cell 9199 9135 fill 9125 9050

%%%%%%%%%
 %%%%%%%%%

% top fitting

%%%%%%%%%
 %%%%%%%%%

cell 9210 9136 fill 9112 -9050

cell 9211 9136 fill 9126 9050

%%%%%%%%%
 %%%%%%%%%

% Build Experiment Leg (Level 2 & 1)

%%%%%%%%%
 %%%%%%%%%

% XS generattion -- axial partition

cell 9125 9100 fill 9129 -11 % Steel Grid Plate + Aluminum bottom fitting

cell 9126 9100 fill 9130 11 -9070 % Common Internals (Begin Al + shells)

cell 9127 9100 fill 9131 9070 -9071 % Start Dy + Test_begin

cell 9129 9100 fill 9132 9071 -9072 % Dy (0.2" thick) + Test

cell 9134 9100 fill 9133 9072 -9073 % Dy(0.017") + Test

cell 9135 9100 fill 9134 9073 -9074 % Dy(0.002") + Test

cell 9136 9100 fill 9135 9074 -9075 % Steel Zone + Test

cell 9137 9100 fill 9134 9075 -9076 % Dy(0.002") + Test

cell 9138 9100 fill 9133 9076 -9077 % Dy(0.017") + Test

cell 9139 9100 fill 9132 9077 -9078 % Dy(0.02") + Test

cell 9143 9100 fill 9130 9078 -27 % Normal Pipe

cell 9146 9100 fill 9136 27 % top fitting

%%%%%%%%%
 %%%%%%%%%

% Pump leg + air + Steel Frame on Cal Vehicle

%%
 %%%

cell 9348 9350 air -9061 % Inside of pump leg

cell 9349 9350 steel 9061 -9062 % Steel cladding

cell 9350 9350 air 9062 -9079 % replace air with fuel

cell 9351 9350 steel 9079 -9080 % Steel Walls

cell 9352 9350 air_out 9080 % Air outside of walls

cell 9353 9351 Al_steel -90 % bottom fitting

cell 9354 9352 Al_air -90 % top fitting

cell 9301 9300 fill 9351 -11

cell 9303 9300 fill 9350 11 -27

cell 9304 9300 fill 9352 27

%%
 %%%

% Build Entire Assembly

%%
 %%%

cell 9470 9500 fill 9100 -9060 % Exp leg

cell 9472 9500 fill 9300 9060 % Pump leg & air inside & vehicle wall

% chop into 30 axial levels

cell 9501 9501 fill 9500 -90 %% Steel Grid Plate + Aluminum bottom fitting

cell 9502 9502 fill 9500 -90 %% Added Region

cell 9503 9503 fill 9500 -90 %% Added Region

cell 9504 9504 fill 9500 -90 %% Oct graphite XS region 1 -- bottom

cell 9505 9505 fill 9500 -90 %% Added Region

cell 9506 9506 fill 9500 -90 %% Oct graphite XS region 2 -- bottom

cell 9507 9507 fill 9500 -90 %% square graphite bottom + air gap + Al clad

cell 9508 9508 fill 9500 -90 %% axial interface

cell 9509 9509 fill 9500 -90 %% Added Region

cell 9510 9510 fill 9500 -90 %% Fuel1 bottom

cell 9511 9511 fill 9500 -90 %% Added Region

cell 9512 9512 fill 9500 -90 %% Added Region

cell 9513 9513 fill 9500 -90 %% Added Region

cell 9514 9514 fill 9500 -90 %% Added Region

cell 9515 9515 fill 9500 -90 %% Added Region

cell 9516 9516 fill 9500 -90 %% Added Region

cell 9517 9517 fill 9500 -90 %% Added Region

cell 9518 9518 fill 9500 -90 %% Added Region

cell 9519 9519 fill 9500 -90 %% Fuel2

cell 9520 9520 fill 9500 -90 %% Added Region

cell 9521 9521 fill 9500 -90 %% Fuel1 top

cell 9522 9522 fill 9500 -90 %% axial interface

```

cell 9523 9523 fill 9500 -90  %% Added Region
cell 9524 9524 fill 9500 -90  %% Added Region
cell 9525 9525 fill 9500 -90  %% square graphite w hole top + Oct graphite with hole + air + Al
clad
cell 9526 9526 fill 9500 -90  %% Oct graphite XS region 2 -- top
cell 9527 9527 fill 9500 -90  %% Added Region
cell 9528 9528 fill 9500 -90  %% Added Region
cell 9529 9529 fill 9500 -90  %% Oct graphite XS region 1 -- top
cell 9530 9530 fill 9500 -90  %% top fitting

```

```

% put together again

```

```

cell 9541 9000 fill 9501    -11  %% Steel Grid Plate + Aluminum bottom fitting
cell 9542 9000 fill 9502  11  -250 %% Added Region
cell 9543 9000 fill 9503 250  -251 %% Added Region
cell 9544 9000 fill 9504 251  -12  %% Oct graphite XS region 1 -- bottom
cell 9545 9000 fill 9505  12  -252 %% Added Region
cell 9546 9000 fill 9506 252  -13  %% Oct graphite XS region 2 -- bottom
cell 9547 9000 fill 9507  13  -14  %% square graphite bottom + air gap + Al clad
cell 9548 9000 fill 9508  14  -17  %% axial interface
cell 9549 9000 fill 9509  17  -253 %% Added Region
cell 9550 9000 fill 9510 253  -18  %% Fuel1 bottom
cell 9551 9000 fill 9511  18  -254 %% Added Region
cell 9552 9000 fill 9512 254  -255 %% Added Region
cell 9553 9000 fill 9513 255  -256 %% Added Region
cell 9554 9000 fill 9514 256  -257 %% Added Region
cell 9555 9000 fill 9515 257  -258 %% Added Region
cell 9556 9000 fill 9516 258  -259 %% Added Region
cell 9557 9000 fill 9517 259  -260 %% Added Region
cell 9558 9000 fill 9518 260  -261 %% Added Region
cell 9559 9000 fill 9519 261  -19  %% Fuel2
cell 9560 9000 fill 9520  19  -262 %% Added Region
cell 9561 9000 fill 9521 262  -20  %% Fuel1 top
cell 9562 9000 fill 9522  20  -23  %% axial interface
cell 9563 9000 fill 9523  23  -263 %% Added Region
cell 9564 9000 fill 9524 263  -264 %% Added Region
cell 9565 9000 fill 9525 264  -25  %% square graphite w hole top + Oct graphite with hole +
air + Al clad
cell 9566 9000 fill 9526  25  -26  %% Oct graphite XS region 2 -- top
cell 9567 9000 fill 9527  26  -265 %% Added Region
cell 9568 9000 fill 9528 265  -266 %% Added Region
cell 9569 9000 fill 9529 266  -27  %% Oct graphite XS region 1 -- top
cell 9580 9000 fill 9530  27      %% top fitting

```

```

%plot 3 1000 1000  2.50  -10.16 10.16  -10.16 10.16  % xy-plot
%plot 3 1000 1000 11.00  -10.16 10.16  -10.16 10.16  % xy-plot

```

```

%plot 3 1000 1000 30.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 76.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 80.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 100.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 108.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 112.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 121.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 130.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 135.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 138.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 150.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 168.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 190.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 220.00 -10.16 10.16 -10.16 10.16 % xy-plot
%plot 3 1000 1000 250.00 -10.16 10.16 -10.16 10.16 % xy-plot
%
%plot 1 1000 2000 0.0 -10.16 10.16 -10.0 250.65 % xz-plot

```

CR-Type_cyl.sss

```

%%% Javier Ortensi
%%% Assume that the CRs are banked together for the three types
%%% separate cross section regions for the 3 types
%#####
##
% CONTROL ROD REGIONS (Compensation Rods)
%#####
##
% Dynamic Control Rod
cell 800 811 graphite -50 % Graphite - Upper follower
cell 801 811 steel 50 % lower carbon steel clad
cell 802 812 steel -50 % Steel plug - Upper follower
cell 803 812 steel 50 % lower carbon steel clad
cell 804 813 zr_steel -50 % Zr/Steel plug - Zr follower
cell 805 813 zr 50 % zirc-3 clad (zirc follower)
cell 806 814 graphite -50 % Graphite - Zr follower
cell 807 814 zr 50 % zirc-3 clad (zirc follower)
cell 808 815 zr_steel -50 % Zr/Steel plug - Zr follower
cell 809 815 zr 50 % zirc-3 clad (zirc follower)
cell 810 816 steel -50 % Steel plug - poison section
cell 811 816 steel 50 % upper carbon steel clad
cell 812 817 b4c_new -50 % B4C - poison section
cell 813 817 steel 50 % upper carbon steel clad
cell 814 818 steel -50 % steel plug | grapple adaptor
cell 815 818 steel 50 % steel plug | grapple adaptor
cell 816 819 Air_steel -90 % grapple and air
cell 817 820 airCR -90 % air above CR

```

```

%#####
##
cell 820 801 fill 811      -855 % P1/P2 Graphite
cell 821 801 fill 812      855 -856 % steel plug
cell 822 801 fill 813      856 -857 % Zr/Steel plug
cell 823 801 fill 814      857 -858 % Graphite
cell 824 801 fill 815      858 -859 % Zr/Steel plug
cell 825 801 fill 816      859 -860 % Steel plug
cell 826 801 fill 817      860 -861 % B4C
cell 827 801 fill 818      861 -862 % Top of grapple adaptor coupling
cell 828 801 fill 819      862 -863 % Top of grapple adaptor
cell 829 801 fill 820      863      % air
%#####
##
% CONTROL ROD REGIONS (Control/Shutdown Rods)
%#####
##
% Dynamic Control Rod
cell 830 831 graphite -50      % Graphite      - Upper follower
cell 831 831 steel    50      % lower carbon steel clad
cell 832 832 steel   -50      % Steel plug      - Upper follower
cell 833 832 steel    50      % lower carbon steel clad
cell 834 833 zr_steel -50      % Zr/Steel plug - Zr follower
cell 835 833 zr       50      % zirc-3 clad (zirc follower)
cell 836 834 graphite -50      % Graphite      - Zr follower
cell 837 834 zr       50      % zirc-3 clad (zirc follower)
cell 838 835 zr_steel -50      % Zr/Steel plug - Zr follower
cell 839 835 zr       50      % zirc-3 clad (zirc follower)
cell 840 836 steel   -50      % Steel plug      - poison section
cell 841 836 steel    50      % upper carbon steel clad
cell 842 837 b4c_new  -50      % B4C            - poison section
cell 843 837 steel    50      % upper carbon steel clad
cell 844 838 steel   -50      % steel plug | grapple adaptor
cell 845 838 steel    50      % steel plug | grapple adaptor
cell 846 839 Air_steel -90      % grapple and air
cell 847 840 airCR    -90      % air above CR
%#####
##
% (Control/Shutdown Rods)
cell 850 802 fill 831      -855 % P1/P2 Graphite
cell 851 802 fill 832      855 -856 % steel plug
cell 852 802 fill 833      856 -857 % Zr/Steel plug
cell 853 802 fill 834      857 -858 % Graphite
cell 854 802 fill 835      858 -859 % Zr/Steel plug
cell 855 802 fill 836      859 -860 % Steel plug
cell 856 802 fill 837      860 -861 % B4C

```

```

cell 857 802 fill 838      861 -862 % Top of grapple adaptor coupling
cell 858 802 fill 839      862 -863 % Top of grapple adaptor
cell 859 802 fill 840      863   % air
%#####
##
% CONTROL ROD REGIONS (Transient Rod)
%#####
##
% Dynamic Control Rod
cell 860 851 graphite -50   % Graphite   - Upper follower
cell 861 851 steel    50    % lower carbon steel clad
cell 862 852 steel    -50   % Steel plug   - Upper follower
cell 863 852 steel     50   % lower carbon steel clad
cell 864 853 zr_steel -50   % Zr/Steel plug - Zr follower
cell 865 853 zr       50    % zirc-3 clad (zirc follower)
cell 866 854 graphite -50   % Graphite     - Zr follower
cell 867 854 zr       50    % zirc-3 clad (zirc follower)
cell 868 855 zr_steel -50   % Zr/Steel plug - Zr follower
cell 869 855 zr       50    % zirc-3 clad (zirc follower)
cell 870 856 steel    -50   % Steel plug   - poison section
cell 871 856 steel     50   % upper carbon steel clad
cell 872 857 b4c_new  -50   % B4C          - poison section
cell 873 857 steel     50   % upper carbon steel clad
cell 874 858 steel    -50   % steel plug | grapple adaptor
cell 875 858 steel     50   % steel plug | grapple adaptor
cell 876 859 Air_steel -90   % grapple and air
cell 877 860 airCR     -90   % air above CR
%#####
##
cell 880 803 fill 851      -875 % P1/P2 Graphite
cell 881 803 fill 852      875 -876 % steel plug
cell 882 803 fill 853      876 -877 % Zr/Steel plug
cell 883 803 fill 854      877 -878 % Graphite
cell 884 803 fill 855      878 -879 % Zr/Steel plug
cell 885 803 fill 856      879 -880 % Steel plug
cell 886 803 fill 857      880 -881 % B4C
cell 887 803 fill 858      881 -882 % Top of grapple adaptor coupling
cell 888 803 fill 859      882 -883 % Top of grapple adaptor
cell 889 803 fill 860      883   % air

```

Extra_Surfaces.sss

```

%%%%%%%%%
%% Added Plains for extra cuts
%%%%%%%%%

```

surf 250 pz 12.486 %% Extra Axial Cut

surf 251 pz 21.486 %% Extra Axial Cut
surf 252 pz 41.830375 %% Extra Axial Cut
surf 253 pz 72.82675 %% Extra Axial Cut
surf 254 pz 87.21075 %% Extra Axial Cut
surf 255 pz 97.21075 %% Extra Axial Cut
surf 256 pz 107.21075 %% Extra Axial Cut
surf 257 pz 117.21075 %% Extra Axial Cut
surf 258 pz 127.21075 %% Extra Axial Cut
surf 259 pz 137.21075 %% Extra Axial Cut
surf 260 pz 147.21075 %% Extra Axial Cut
surf 261 pz 156.46075 %% Extra Axial Cut
surf 262 pz 172.21075 %% Extra Axial Cut
surf 263 pz 188.81075 %% Extra Axial Cut
surf 264 pz 195.589375 %% Extra Axial Cut
surf 265 pz 229.2625 %% Extra Axial Cut
surf 266 pz 238.2625 %% Extra Axial Cut

A-s.sss

%%%%%%%%%%

% Define A1

% Description of Placement:

% Copy Universes

cell 11101	11101 fill 11001	-90	%% Axial Position to end at = 3.486
cell 11102	11102 fill 11002	-90	%% Axial Position to end at = 30.486
cell 11103	11103 fill 11003	-90	%% Axial Position to end at = 53.17475
cell 11104	11104 fill 11004	-90	%% Axial Position to end at = 62.06475
cell 11105	11105 fill 11005	-90	%% Axial Position to end at = 62.82675
cell 11106	11106 fill 11006	-90	%% Axial Position to end at = 82.82675
cell 11107	11107 fill 11006	-90	%% Added Lines for axial position 106.1655
cell 11108	11108 fill 11006	-90	%% Added Lines for axial position 109.11825
cell 11109	11109 fill 11006	-90	%% Added Lines for axial position 114.4205
cell 11110	11110 fill 11007	-90	%% Axial Position to end at = 163.79425
cell 11111	11111 fill 11008	-90	%% Axial Position to end at = 183.79425
cell 11112	11112 fill 11009	-90	%% Axial Position to end at = 184.55625
cell 11113	11113 fill 11010	-90	%% Axial Position to end at = 206.6225
cell 11114	11114 fill 11011	-90	%% Axial Position to end at = 220.2625
cell 11115	11115 fill 11012	-90	%% Axial Position to end at = 247.2625
cell 11116	11116 fill 11013	-90	%% All the way to the top

%% BUILD A1

cell 11117	11100 fill 11101	-11	%% Steel Grid Plate + Aluminum bottom fitting
cell 11118	11100 fill 11102	11 -12	%% Oct graphite XS region 1 -- bottom
cell 11119	11100 fill 11103	12 -13	%% Oct graphite XS region 2 -- bottom
cell 11120	11100 fill 11104	13 -14	%% square graphite bottom + air gap + Al clad

```

cell 11121      11100fill 11105      14 -17  %% axial interface
cell 11122      11100fill 11106      17 -18  %% Fuel1 bottom
cell 11123      11100fill 11107      18 -250  %% Added Region
cell 11124      11100fill 11108      250 -251  %% Added Region
cell 11125      11100fill 11109      251 -252  %% Added Region
cell 11126      11100fill 11110      252 -19  %% Fuel2
cell 11127      11100fill 11111      19 -20  %% Fuel1 top
cell 11128      11100fill 11112      20 -23  %% aixal interface
cell 11129      11100fill 11113      23 -25  %% square graphite w hole top + Oct graphite
with hole + air + Al clad
cell 11130      11100fill 11114      25 -26  %% Oct graphite XS region 2 -- top
cell 11131      11100fill 11115      26 -27  %% Oct graphite XS region 1 -- top
cell 11132      11100fill 11116      27      %% top fitting
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Define A2
% Description of Placement:

% Copy Universes
cell 11201      11201 fill 11001      -90  %% Axial Position to end at = 3.486
cell 11202      11202 fill 11002      -90  %% Axial Position to end at = 30.486
cell 11203      11203 fill 11003      -90  %% Axial Position to end at = 53.17475
cell 11204      11204 fill 11004      -90  %% Axial Position to end at = 62.06475
cell 11205      11205 fill 11005      -90  %% Axial Position to end at = 62.82675
cell 11206      11206 fill 11006      -90  %% Axial Position to end at = 82.82675
cell 11207      11207 fill 11006      -90  %% Added Lines for axial position 106.1655
cell 11208      11208 fill 11006      -90  %% Added Lines for axial position 109.11825
cell 11209      11209 fill 11006      -90  %% Added Lines for axial position 114.4205
cell 11210      11210 fill 11007      -90  %% Axial Position to end at = 163.79425
cell 11211      11211 fill 11008      -90  %% Axial Position to end at = 183.79425
cell 11212      11212 fill 11009      -90  %% Axial Position to end at = 184.55625
cell 11213      11213 fill 11010      -90  %% Axial Position to end at = 206.6225
cell 11214      11214 fill 11011      -90  %% Axial Position to end at = 220.2625
cell 11215      11215 fill 11012      -90  %% Axial Position to end at = 247.2625
cell 11216      11216 fill 11013      -90  %% All the way to the top

%% BUILD A2
cell 11217      11200fill 11201      -11  %% Steel Grid Plate + Aluminum bottom
fitting
cell 11218      11200fill 11202      11 -12  %% Oct graphite XS region 1 -- bottom
cell 11219      11200fill 11203      12 -13  %% Oct graphite XS region 2 -- bottom
cell 11220      11200fill 11204      13 -14  %% square graphite bottom + air gap + Al clad
cell 11221      11200fill 11205      14 -17  %% axial interface
cell 11222      11200fill 11206      17 -18  %% Fuel1 bottom
cell 11223      11200fill 11207      18 -250  %% Added Region
cell 11224      11200fill 11208      250 -251  %% Added Region
cell 11225      11200fill 11209      251 -252  %% Added Region

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cell 11226      11200fill 11210      252 -19  %% Fuel2
cell 11227      11200fill 11211      19  -20  %% Fuel1 top
cell 11228      11200fill 11212      20  -23  %% aixal interface
cell 11229      11200fill 11213      23  -25  %% square graphite w hole top + Oct graphite
with hole + air + Al clad
cell 11230      11200fill 11214      25  -26  %% Oct graphite XS region 2 -- top
cell 11231      11200fill 11215      26  -27  %% Oct graphite XS region 1 -- top
cell 11232      11200fill 11216      27      %% top fitting
%%%%%%%%%%%%%%
% Define A3
% Description of Placement:

% Copy Universes
cell 11301      11301 fill 11001      -90  %% Axial Position to end at = 3.486
cell 11302      11302 fill 11002      -90  %% Axial Position to end at = 30.486
cell 11303      11303 fill 11003      -90  %% Axial Position to end at = 53.17475
cell 11304      11304 fill 11004      -90  %% Axial Position to end at = 62.06475
cell 11305      11305 fill 11005      -90  %% Axial Position to end at = 62.82675
cell 11306      11306 fill 11006      -90  %% Axial Position to end at = 82.82675
cell 11307      11307 fill 11006      -90  %% Added Lines for axial position 106.1655
cell 11308      11308 fill 11006      -90  %% Added Lines for axial position 109.11825
cell 11309      11309 fill 11006      -90  %% Added Lines for axial position 114.4205
cell 11310      11310 fill 11007      -90  %% Axial Position to end at = 163.79425
cell 11311      11311 fill 11008      -90  %% Axial Position to end at = 183.79425
cell 11312      11312 fill 11009      -90  %% Axial Position to end at = 184.55625
cell 11313      11313 fill 11010      -90  %% Axial Position to end at = 206.6225
cell 11314      11314 fill 11011      -90  %% Axial Position to end at = 220.2625
cell 11315      11315 fill 11012      -90  %% Axial Position to end at = 247.2625
cell 11316      11316 fill 11013      -90  %% All the way to the top

%% BUILD A3
cell 11317      11300fill 11301      -11  %% Steel Grid Plate + Aluminum bottom
fitting
cell 11318      11300fill 11302      11 -12  %% Oct graphite XS region 1 -- bottom
cell 11319      11300fill 11303      12 -13  %% Oct graphite XS region 2 -- bottom
cell 11320      11300fill 11304      13 -14  %% square graphite bottom + air gap + Al clad
cell 11321      11300fill 11305      14 -17  %% axial interface
cell 11322      11300fill 11306      17 -18  %% Fuel1 bottom
cell 11323      11300fill 11307      18 -250  %% Added Region
cell 11324      11300fill 11308      250 -251  %% Added Region
cell 11325      11300fill 11309      251 -252  %% Added Region
cell 11326      11300fill 11310      252 -19  %% Fuel2
cell 11327      11300fill 11311      19 -20  %% Fuel1 top
cell 11328      11300fill 11312      20 -23  %% aixal interface
cell 11329      11300fill 11313      23 -25  %% square graphite w hole top + Oct graphite
with hole + air + Al clad

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```

cell 11330      11300fill 11314      25 -26  %% Oct graphite XS region 2 -- top
cell 11331      11300fill 11315      26 -27  %% Oct graphite XS region 1 -- top
cell 11332      11300fill 11316      27      %% top fitting

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

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```

% Define A4

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% Description of Placement:

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% Copy Universes

```

```

cell 11401      11401 fill 11001      -90  %% Axial Position to end at = 3.486
cell 11402      11402 fill 11002      -90  %% Axial Position to end at = 30.486
cell 11403      11403 fill 11003      -90  %% Axial Position to end at = 53.17475
cell 11404      11404 fill 11004      -90  %% Axial Position to end at = 62.06475
cell 11405      11405 fill 11005      -90  %% Axial Position to end at = 62.82675
cell 11406      11406 fill 11006      -90  %% Axial Position to end at = 82.82675
cell 11407      11407 fill 11006      -90  %% Added Lines for axial position 106.1655
cell 11408      11408 fill 11006      -90  %% Added Lines for axial position 109.11825
cell 11409      11409 fill 11006      -90  %% Added Lines for axial position 114.4205
cell 11410      11410 fill 11007      -90  %% Axial Position to end at = 163.79425
cell 11411      11411 fill 11008      -90  %% Axial Position to end at = 183.79425
cell 11412      11412 fill 11009      -90  %% Axial Position to end at = 184.55625
cell 11413      11413 fill 11010      -90  %% Axial Position to end at = 206.6225
cell 11414      11414 fill 11011      -90  %% Axial Position to end at = 220.2625
cell 11415      11415 fill 11012      -90  %% Axial Position to end at = 247.2625
cell 11416      11416 fill 11013      -90  %% All the way to the top

```

```

%% BUILD A4

```

```

cell 11417      11400fill 11401      -11  %% Steel Grid Plate + Aluminum bottom
fitting
cell 11418      11400fill 11402      11 -12  %% Oct graphite XS region 1 -- bottom
cell 11419      11400fill 11403      12 -13  %% Oct graphite XS region 2 -- bottom
cell 11420      11400fill 11404      13 -14  %% square graphite bottom + air gap + Al clad
cell 11421      11400fill 11405      14 -17  %% axial interface
cell 11422      11400fill 11406      17 -18  %% Fuel1 bottom
cell 11423      11400fill 11407      18 -250  %% Added Region
cell 11424      11400fill 11408      250 -251  %% Added Region
cell 11425      11400fill 11409      251 -252  %% Added Region
cell 11426      11400fill 11410      252 -19  %% Fuel2
cell 11427      11400fill 11411      19 -20  %% Fuel1 top
cell 11428      11400fill 11412      20 -23  %% axial interface
cell 11429      11400fill 11413      23 -25  %% square graphite w hole top + Oct graphite
with hole + air + Al clad
cell 11430      11400fill 11414      25 -26  %% Oct graphite XS region 2 -- top
cell 11431      11400fill 11415      26 -27  %% Oct graphite XS region 1 -- top
cell 11432      11400fill 11416      27      %% top fitting

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```

% Define A5

```

% Description of Placement:

% Copy Universes

cell 11501	11501 fill 11001	-90	%% Axial Position to end at = 3.486
cell 11502	11502 fill 11002	-90	%% Axial Position to end at = 30.486
cell 11503	11503 fill 11003	-90	%% Axial Position to end at = 53.17475
cell 11504	11504 fill 11004	-90	%% Axial Position to end at = 62.06475
cell 11505	11505 fill 11005	-90	%% Axial Position to end at = 62.82675
cell 11506	11506 fill 11006	-90	%% Axial Position to end at = 82.82675
cell 11507	11507 fill 11006	-90	%% Added Lines for axial position 106.1655
cell 11508	11508 fill 11006	-90	%% Added Lines for axial position 109.11825
cell 11509	11509 fill 11006	-90	%% Added Lines for axial position 114.4205
cell 11510	11510 fill 11007	-90	%% Axial Position to end at = 163.79425
cell 11511	11511 fill 11008	-90	%% Axial Position to end at = 183.79425
cell 11512	11512 fill 11009	-90	%% Axial Position to end at = 184.55625
cell 11513	11513 fill 11010	-90	%% Axial Position to end at = 206.6225
cell 11514	11514 fill 11011	-90	%% Axial Position to end at = 220.2625
cell 11515	11515 fill 11012	-90	%% Axial Position to end at = 247.2625
cell 11516	11516 fill 11013	-90	%% All the way to the top

%% BUILD A5

cell 11517	11500fill 11501	-11	%% Steel Grid Plate + Aluminum bottom fitting
cell 11518	11500fill 11502	11 -12	%% Oct graphite XS region 1 -- bottom
cell 11519	11500fill 11503	12 -13	%% Oct graphite XS region 2 -- bottom
cell 11520	11500fill 11504	13 -14	%% square graphite bottom + air gap + Al clad
cell 11521	11500fill 11505	14 -17	%% axial interface
cell 11522	11500fill 11506	17 -18	%% Fuel1 bottom
cell 11523	11500fill 11507	18 -250	%% Added Region
cell 11524	11500fill 11508	250 -251	%% Added Region
cell 11525	11500fill 11509	251 -252	%% Added Region
cell 11526	11500fill 11510	252 -19	%% Fuel2
cell 11527	11500fill 11511	19 -20	%% Fuel1 top
cell 11528	11500fill 11512	20 -23	%% axial interface
cell 11529	11500fill 11513	23 -25	%% square graphite w hole top + Oct graphite with hole + air + Al clad
cell 11530	11500fill 11514	25 -26	%% Oct graphite XS region 2 -- top
cell 11531	11500fill 11515	26 -27	%% Oct graphite XS region 1 -- top
cell 11532	11500fill 11516	27	%% top fitting

%%%

% Define A6

% Description of Placement:

% Copy Universes

cell 11601	11601 fill 11001	-90	%% Axial Position to end at = 3.486
cell 11602	11602 fill 11002	-90	%% Axial Position to end at = 30.486

cell 11603	11603 fill 11003	-90	%% Axial Position to end at = 53.17475
cell 11604	11604 fill 11004	-90	%% Axial Position to end at = 62.06475
cell 11605	11605 fill 11005	-90	%% Axial Position to end at = 62.82675
cell 11606	11606 fill 11006	-90	%% Axial Position to end at = 82.82675
cell 11607	11607 fill 11006	-90	%% Added Lines for axial position 106.1655
cell 11608	11608 fill 11006	-90	%% Added Lines for axial position 109.11825
cell 11609	11609 fill 11006	-90	%% Added Lines for axial position 114.4205
cell 11610	11610 fill 11007	-90	%% Axial Position to end at = 163.79425
cell 11611	11611 fill 11008	-90	%% Axial Position to end at = 183.79425
cell 11612	11612 fill 11009	-90	%% Axial Position to end at = 184.55625
cell 11613	11613 fill 11010	-90	%% Axial Position to end at = 206.6225
cell 11614	11614 fill 11011	-90	%% Axial Position to end at = 220.2625
cell 11615	11615 fill 11012	-90	%% Axial Position to end at = 247.2625
cell 11616	11616 fill 11013	-90	%% All the way to the top

%% BUILD A6

cell 11617	11600fill 11601	-11	%% Steel Grid Plate + Aluminum bottom
fitting			
cell 11618	11600fill 11602	11 -12	%% Oct graphite XS region 1 -- bottom
cell 11619	11600fill 11603	12 -13	%% Oct graphite XS region 2 -- bottom
cell 11620	11600fill 11604	13 -14	%% square graphite bottom + air gap + Al clad
cell 11621	11600fill 11605	14 -17	%% axial interface
cell 11622	11600fill 11606	17 -18	%% Fuel1 bottom
cell 11623	11600fill 11607	18 -250	%% Added Region
cell 11624	11600fill 11608	250 -251	%% Added Region
cell 11625	11600fill 11609	251 -252	%% Added Region
cell 11626	11600fill 11610	252 -19	%% Fuel2
cell 11627	11600fill 11611	19 -20	%% Fuel1 top
cell 11628	11600fill 11612	20 -23	%% axial interface
cell 11629	11600fill 11613	23 -25	%% square graphite w hole top + Oct graphite
with hole + air + Al clad			
cell 11630	11600fill 11614	25 -26	%% Oct graphite XS region 2 -- top
cell 11631	11600fill 11615	26 -27	%% Oct graphite XS region 1 -- top
cell 11632	11600fill 11616	27	%% top fitting

%%%

% Define A7

% Description of Placement:

% Copy Universes

cell 11701	11701 fill 11001	-90	%% Axial Position to end at = 3.486
cell 11702	11702 fill 11002	-90	%% Axial Position to end at = 30.486
cell 11703	11703 fill 11003	-90	%% Axial Position to end at = 53.17475
cell 11704	11704 fill 11004	-90	%% Axial Position to end at = 62.06475
cell 11705	11705 fill 11005	-90	%% Axial Position to end at = 62.82675
cell 11706	11706 fill 11006	-90	%% Axial Position to end at = 82.82675
cell 11707	11707 fill 11006	-90	%% Added Lines for axial position 106.1655

cell 11708	11708 fill 11006	-90	%% Added Lines for axial position 109.11825
cell 11709	11709 fill 11006	-90	%% Added Lines for axial position 114.4205
cell 11710	11710 fill 11007	-90	%% Axial Position to end at = 163.79425
cell 11711	11711 fill 11008	-90	%% Axial Position to end at = 183.79425
cell 11712	11712 fill 11009	-90	%% Axial Position to end at = 184.55625
cell 11713	11713 fill 11010	-90	%% Axial Position to end at = 206.6225
cell 11714	11714 fill 11011	-90	%% Axial Position to end at = 220.2625
cell 11715	11715 fill 11012	-90	%% Axial Position to end at = 247.2625
cell 11716	11716 fill 11013	-90	%% All the way to the top

%% BUILD A7

cell 11717	11700fill 11701	-11	%% Steel Grid Plate + Aluminum bottom fitting
cell 11718	11700fill 11702	11 -12	%% Oct graphite XS region 1 -- bottom
cell 11719	11700fill 11703	12 -13	%% Oct graphite XS region 2 -- bottom
cell 11720	11700fill 11704	13 -14	%% square graphite bottom + air gap + Al clad
cell 11721	11700fill 11705	14 -17	%% axial interface
cell 11722	11700fill 11706	17 -18	%% Fuel1 bottom
cell 11723	11700fill 11707	18 -250	%% Added Region
cell 11724	11700fill 11708	250 -251	%% Added Region
cell 11725	11700fill 11709	251 -252	%% Added Region
cell 11726	11700fill 11710	252 -19	%% Fuel2
cell 11727	11700fill 11711	19 -20	%% Fuel1 top
cell 11728	11700fill 11712	20 -23	%% axial interface
cell 11729	11700fill 11713	23 -25	%% square graphite w hole top + Oct graphite with hole + air + Al clad
cell 11730	11700fill 11714	25 -26	%% Oct graphite XS region 2 -- top
cell 11731	11700fill 11715	26 -27	%% Oct graphite XS region 1 -- top
cell 11732	11700fill 11716	27	%% top fitting

%%%

% Define A8

% Description of Placement:

% Copy Universes

cell 11801	11801 fill 11001	-90	%% Axial Position to end at = 3.486
cell 11802	11802 fill 11002	-90	%% Axial Position to end at = 30.486
cell 11803	11803 fill 11003	-90	%% Axial Position to end at = 53.17475
cell 11804	11804 fill 11004	-90	%% Axial Position to end at = 62.06475
cell 11805	11805 fill 11005	-90	%% Axial Position to end at = 62.82675
cell 11806	11806 fill 11006	-90	%% Axial Position to end at = 82.82675
cell 11807	11807 fill 11006	-90	%% Added Lines for axial position 106.1655
cell 11808	11808 fill 11006	-90	%% Added Lines for axial position 109.11825
cell 11809	11809 fill 11006	-90	%% Added Lines for axial position 114.4205
cell 11810	11810 fill 11007	-90	%% Axial Position to end at = 163.79425
cell 11811	11811 fill 11008	-90	%% Axial Position to end at = 183.79425
cell 11812	11812 fill 11009	-90	%% Axial Position to end at = 184.55625

cell 11813	11813 fill 11010	-90	%% Axial Position to end at = 206.6225
cell 11814	11814 fill 11011	-90	%% Axial Position to end at = 220.2625
cell 11815	11815 fill 11012	-90	%% Axial Position to end at = 247.2625
cell 11816	11816 fill 11013	-90	%% All the way to the top

%% BUILD A8

cell 11817	11800fill 11801	-11	%% Steel Grid Plate + Aluminum bottom fitting
cell 11818	11800fill 11802	11 -12	%% Oct graphite XS region 1 -- bottom
cell 11819	11800fill 11803	12 -13	%% Oct graphite XS region 2 -- bottom
cell 11820	11800fill 11804	13 -14	%% square graphite bottom + air gap + Al clad
cell 11821	11800fill 11805	14 -17	%% axial interface
cell 11822	11800fill 11806	17 -18	%% Fuel1 bottom
cell 11823	11800fill 11807	18 -250	%% Added Region
cell 11824	11800fill 11808	250 -251	%% Added Region
cell 11825	11800fill 11809	251 -252	%% Added Region
cell 11826	11800fill 11810	252 -19	%% Fuel2
cell 11827	11800fill 11811	19 -20	%% Fuel1 top
cell 11828	11800fill 11812	20 -23	%% axial interface
cell 11829	11800fill 11813	23 -25	%% square graphite w hole top + Oct graphite with hole + air + Al clad
cell 11830	11800fill 11814	25 -26	%% Oct graphite XS region 2 -- top
cell 11831	11800fill 11815	26 -27	%% Oct graphite XS region 1 -- top
cell 11832	11800fill 11816	27	%% top fitting

%%%

% Define A9

% Description of Placement:

% Copy Universes

cell 11901	11901 fill 11001	-90	%% Axial Position to end at = 3.486
cell 11902	11902 fill 11002	-90	%% Axial Position to end at = 30.486
cell 11903	11903 fill 11003	-90	%% Axial Position to end at = 53.17475
cell 11904	11904 fill 11004	-90	%% Axial Position to end at = 62.06475
cell 11905	11905 fill 11005	-90	%% Axial Position to end at = 62.82675
cell 11906	11906 fill 11006	-90	%% Axial Position to end at = 82.82675
cell 11907	11907 fill 11006	-90	%% Added Lines for axial position 106.1655
cell 11908	11908 fill 11006	-90	%% Added Lines for axial position 109.11825
cell 11909	11909 fill 11006	-90	%% Added Lines for axial position 114.4205
cell 11910	11910 fill 11007	-90	%% Axial Position to end at = 163.79425
cell 11911	11911 fill 11008	-90	%% Axial Position to end at = 183.79425
cell 11912	11912 fill 11009	-90	%% Axial Position to end at = 184.55625
cell 11913	11913 fill 11010	-90	%% Axial Position to end at = 206.6225
cell 11914	11914 fill 11011	-90	%% Axial Position to end at = 220.2625
cell 11915	11915 fill 11012	-90	%% Axial Position to end at = 247.2625
cell 11916	11916 fill 11013	-90	%% All the way to the top

%% BUILD A9

cell 11917	11900fill 11901	-11	%% Steel Grid Plate + Aluminum bottom fitting
cell 11918	11900fill 11902	11 -12	%% Oct graphite XS region 1 -- bottom
cell 11919	11900fill 11903	12 -13	%% Oct graphite XS region 2 -- bottom
cell 11920	11900fill 11904	13 -14	%% square graphite bottom + air gap + Al clad
cell 11921	11900fill 11905	14 -17	%% axial interface
cell 11922	11900fill 11906	17 -18	%% Fuel1 bottom
cell 11923	11900fill 11907	18 -250	%% Added Region
cell 11924	11900fill 11908	250 -251	%% Added Region
cell 11925	11900fill 11909	251 -252	%% Added Region
cell 11926	11900fill 11910	252 -19	%% Fuel2
cell 11927	11900fill 11911	19 -20	%% Fuel1 top
cell 11928	11900fill 11912	20 -23	%% axial interface
cell 11929	11900fill 11913	23 -25	%% square graphite w hole top + Oct graphite with hole + air + Al clad
cell 11930	11900fill 11914	25 -26	%% Oct graphite XS region 2 -- top
cell 11931	11900fill 11915	26 -27	%% Oct graphite XS region 1 -- top
cell 11932	11900fill 11916	27	%% top fitting

%%%

% Define A10

% Description of Placement:

% Copy Universes

cell 12001	12001	fill 11001	-90	%% Axial Position to end at = 3.486
cell 12002	12002	fill 11002	-90	%% Axial Position to end at = 30.486
cell 12003	12003	fill 11003	-90	%% Axial Position to end at = 53.17475
cell 12004	12004	fill 11004	-90	%% Axial Position to end at = 62.06475
cell 12005	12005	fill 11005	-90	%% Axial Position to end at = 62.82675
cell 12006	12006	fill 11006	-90	%% Axial Position to end at = 82.82675
cell 12007	12007	fill 11006	-90	%% Added Lines for axial position 106.1655
cell 12008	12008	fill 11006	-90	%% Added Lines for axial position 109.11825
cell 12009	12009	fill 11006	-90	%% Added Lines for axial position 114.4205
cell 12010	12010	fill 11007	-90	%% Axial Position to end at = 163.79425
cell 12011	12011	fill 11008	-90	%% Axial Position to end at = 183.79425
cell 12012	12012	fill 11009	-90	%% Axial Position to end at = 184.55625

cell 12013	12013	fill 11010	-90	%% Axial Position to end at =
206.6225				
cell 12014	12014	fill 11011	-90	%% Axial Position to end at =
220.2625				
cell 12015	12015	fill 11012	-90	%% Axial Position to end at =
247.2625				
cell 12016	12016	fill 11013	-90	%% All the way to the top

%% BUILD A10

cell 12017	12000	fill 12001	-11	%% Steel Grid Plate + Aluminum
bottom fitting				
cell 12018	12000	fill 12002	11 -12	%% Oct graphite XS region 1 -- bottom
cell 12019	12000	fill 12003	12 -13	%% Oct graphite XS region 2 -- bottom
cell 12020	12000	fill 12004	13 -14	%% square graphite bottom + air gap +
Al clad				
cell 12021	12000	fill 12005	14 -17	%% axial interface
cell 12022	12000	fill 12006	17 -18	%% Fuel1 bottom
cell 12023	12000	fill 12007	18 -250	%% Added Region
cell 12024	12000	fill 12008	250 -251	%% Added Region
cell 12025	12000	fill 12009	251 -252	%% Added Region
cell 12026	12000	fill 12010	252 -19	%% Fuel2
cell 12027	12000	fill 12011	19 -20	%% Fuel1 top
cell 12028	12000	fill 12012	20 -23	%% axial interface
cell 12029	12000	fill 12013	23 -25	%% square graphite w hole top + Oct
graphite with hole + air + Al clad				
cell 12030	12000	fill 12014	25 -26	%% Oct graphite XS region 2 -- top
cell 12031	12000	fill 12015	26 -27	%% Oct graphite XS region 1 -- top
cell 12032	12000	fill 12016	27	%% top fitting

%%%%%%%%%%

% Define A11

% Description of Placement:

% Copy Universes

cell 12101	12101	fill 11001	-90	%% Axial Position to end at = 3.486
cell 12102	12102	fill 11002	-90	%% Axial Position to end at = 30.486
cell 12103	12103	fill 11003	-90	%% Axial Position to end at =
53.17475				
cell 12104	12104	fill 11004	-90	%% Axial Position to end at =
62.06475				
cell 12105	12105	fill 11005	-90	%% Axial Position to end at =
62.82675				
cell 12106	12106	fill 11006	-90	%% Axial Position to end at =
82.82675				
cell 12107	12107	fill 11006	-90	%% Added Lines for axial position
106.1655				

cell 12108	12108	fill 11006	-90	%% Added Lines for axial position
109.11825				
cell 12109	12109	fill 11006	-90	%% Added Lines for axial position
114.4205				
cell 12110	12110	fill 11007	-90	%% Axial Position to end at = 163.79425
cell 12111	12111	fill 11008	-90	%% Axial Position to end at = 183.79425
cell 12112	12112	fill 11009	-90	%% Axial Position to end at = 184.55625
cell 12113	12113	fill 11010	-90	%% Axial Position to end at = 206.6225
cell 12114	12114	fill 11011	-90	%% Axial Position to end at = 220.2625
cell 12115	12115	fill 11012	-90	%% Axial Position to end at = 247.2625
cell 12116	12116	fill 11013	-90	%% All the way to the top

%% BUILD A11

cell 12117	12100	fill 12101	-11	%% Steel Grid Plate + Aluminum
bottom fitting				
cell 12118	12100	fill 12102	11 -12	%% Oct graphite XS region 1 -- bottom
cell 12119	12100	fill 12103	12 -13	%% Oct graphite XS region 2 -- bottom
cell 12120	12100	fill 12104	13 -14	%% square graphite bottom + air gap +
Al clad				
cell 12121	12100	fill 12105	14 -17	%% axial interface
cell 12122	12100	fill 12106	17 -18	%% Fuel1 bottom
cell 12123	12100	fill 12107	18 -250	%% Added Region
cell 12124	12100	fill 12108	250 -251	%% Added Region
cell 12125	12100	fill 12109	251 -252	%% Added Region
cell 12126	12100	fill 12110	252 -19	%% Fuel2
cell 12127	12100	fill 12111	19 -20	%% Fuel1 top
cell 12128	12100	fill 12112	20 -23	%% axial interface
cell 12129	12100	fill 12113	23 -25	%% square graphite w hole top + Oct
graphite with hole + air + Al clad				
cell 12130	12100	fill 12114	25 -26	%% Oct graphite XS region 2 -- top
cell 12131	12100	fill 12115	26 -27	%% Oct graphite XS region 1 -- top
cell 12132	12100	fill 12116	27	%% top fitting

%%%

% Define A12

% Description of Placement:

% Copy Universes

cell 12201	12201	fill 11001	-90	%% Axial Position to end at = 3.486
cell 12202	12202	fill 11002	-90	%% Axial Position to end at = 30.486
cell 12203	12203	fill 11003	-90	%% Axial Position to end at =
53.17475				
cell 12204	12204	fill 11004	-90	%% Axial Position to end at =
62.06475				
cell 12205	12205	fill 11005	-90	%% Axial Position to end at =
62.82675				

cell 12206	12206	fill 11006	-90	%% Axial Position to end at =
82.82675				
cell 12207	12207	fill 11006	-90	%% Added Lines for axial position
106.1655				
cell 12208	12208	fill 11006	-90	%% Added Lines for axial position
109.11825				
cell 12209	12209	fill 11006	-90	%% Added Lines for axial position
114.4205				
cell 12210	12210	fill 11007	-90	%% Axial Position to end at =
163.79425				
cell 12211	12211	fill 11008	-90	%% Axial Position to end at = 183.79425
cell 12212	12212	fill 11009	-90	%% Axial Position to end at =
184.55625				
cell 12213	12213	fill 11010	-90	%% Axial Position to end at =
206.6225				
cell 12214	12214	fill 11011	-90	%% Axial Position to end at =
220.2625				
cell 12215	12215	fill 11012	-90	%% Axial Position to end at =
247.2625				
cell 12216	12216	fill 11013	-90	%% All the way to the top
%% BUILD A12				
cell 12217	12200	fill 12201	-11	%% Steel Grid Plate + Aluminum
bottom fitting				
cell 12218	12200	fill 12202	11 -12	%% Oct graphite XS region 1 -- bottom
cell 12219	12200	fill 12203	12 -13	%% Oct graphite XS region 2 -- bottom
cell 12220	12200	fill 12204	13 -14	%% square graphite bottom + air gap +
Al clad				
cell 12221	12200	fill 12205	14 -17	%% axial interface
cell 12222	12200	fill 12206	17 -18	%% Fuel1 bottom
cell 12223	12200	fill 12207	18 -250	%% Added Region
cell 12224	12200	fill 12208	250 -251	%% Added Region
cell 12225	12200	fill 12209	251 -252	%% Added Region
cell 12226	12200	fill 12210	252 -19	%% Fuel2
cell 12227	12200	fill 12211	19 -20	%% Fuel1 top
cell 12228	12200	fill 12212	20 -23	%% axial interface
cell 12229	12200	fill 12213	23 -25	%% square graphite w hole top + Oct
graphite with hole + air + Al clad				
cell 12230	12200	fill 12214	25 -26	%% Oct graphite XS region 2 -- top
cell 12231	12200	fill 12215	26 -27	%% Oct graphite XS region 1 -- top
cell 12232	12200	fill 12216	27	%% top fitting
%%%				
% Define A13				
% Description of Placement:				
% Copy Universes				

cell 12301	12301	fill 11001	-90	%% Axial Position to end at = 3.486
cell 12302	12302	fill 11002	-90	%% Axial Position to end at = 30.486
cell 12303	12303	fill 11003	-90	%% Axial Position to end at =
53.17475				
cell 12304	12304	fill 11004	-90	%% Axial Position to end at =
62.06475				
cell 12305	12305	fill 11005	-90	%% Axial Position to end at =
62.82675				
cell 12306	12306	fill 11006	-90	%% Axial Position to end at =
82.82675				
cell 12307	12307	fill 11006	-90	%% Added Lines for axial position
106.1655				
cell 12308	12308	fill 11006	-90	%% Added Lines for axial position
109.11825				
cell 12309	12309	fill 11006	-90	%% Added Lines for axial position
114.4205				
cell 12310	12310	fill 11007	-90	%% Axial Position to end at =
163.79425				
cell 12311	12311	fill 11008	-90	%% Axial Position to end at = 183.79425
cell 12312	12312	fill 11009	-90	%% Axial Position to end at =
184.55625				
cell 12313	12313	fill 11010	-90	%% Axial Position to end at =
206.6225				
cell 12314	12314	fill 11011	-90	%% Axial Position to end at =
220.2625				
cell 12315	12315	fill 11012	-90	%% Axial Position to end at =
247.2625				
cell 12316	12316	fill 11013	-90	%% All the way to the top
%% BUILD A13				
cell 12317	12300	fill 12301	-11	%% Steel Grid Plate + Aluminum
bottom fitting				
cell 12318	12300	fill 12302	11 -12	%% Oct graphite XS region 1 -- bottom
cell 12319	12300	fill 12303	12 -13	%% Oct graphite XS region 2 -- bottom
cell 12320	12300	fill 12304	13 -14	%% square graphite bottom + air gap +
Al clad				
cell 12321	12300	fill 12305	14 -17	%% axial interface
cell 12322	12300	fill 12306	17 -18	%% Fuel1 bottom
cell 12323	12300	fill 12307	18 -250	%% Added Region
cell 12324	12300	fill 12308	250 -251	%% Added Region
cell 12325	12300	fill 12309	251 -252	%% Added Region
cell 12326	12300	fill 12310	252 -19	%% Fuel2
cell 12327	12300	fill 12311	19 -20	%% Fuel1 top
cell 12328	12300	fill 12312	20 -23	%% axial interface
cell 12329	12300	fill 12313	23 -25	%% square graphite w hole top + Oct
graphite with hole + air + Al clad				

```

cell 12330      12300      fill 12314      25 -26  %% Oct graphite XS region 2 -- top
cell 12331      12300      fill 12315      26 -27  %% Oct graphite XS region 1 -- top
cell 12332      12300      fill 12316      27      %% top fitting

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%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

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% Define A14

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% Description of Placement:

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% Copy Universes

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cell 12401      12401      fill 11001      -90  %% Axial Position to end at = 3.486
cell 12402      12402      fill 11002      -90  %% Axial Position to end at = 30.486
cell 12403      12403      fill 11003      -90  %% Axial Position to end at =
53.17475
cell 12404      12404      fill 11004      -90  %% Axial Position to end at =
62.06475
cell 12405      12405      fill 11005      -90  %% Axial Position to end at =
62.82675
cell 12406      12406      fill 11006      -90  %% Axial Position to end at =
82.82675
cell 12407      12407      fill 11006      -90  %% Added Lines for axial position
106.1655
cell 12408      12408      fill 11006      -90  %% Added Lines for axial position
109.11825
cell 12409      12409      fill 11006      -90  %% Added Lines for axial position
114.4205
cell 12410      12410      fill 11007      -90  %% Axial Position to end at =
163.79425
cell 12411      12411      fill 11008      -90  %% Axial Position to end at = 183.79425
cell 12412      12412      fill 11009      -90  %% Axial Position to end at =
184.55625
cell 12413      12413      fill 11010      -90  %% Axial Position to end at =
206.6225
cell 12414      12414      fill 11011      -90  %% Axial Position to end at =
220.2625
cell 12415      12415      fill 11012      -90  %% Axial Position to end at =
247.2625
cell 12416      12416      fill 11013      -90  %% All the way to the top

```

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%% BUILD A14

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cell 12417      12400      fill 12401      -11  %% Steel Grid Plate + Aluminum
bottom fitting
cell 12418      12400      fill 12402      11 -12  %% Oct graphite XS region 1 -- bottom
cell 12419      12400      fill 12403      12 -13  %% Oct graphite XS region 2 -- bottom
cell 12420      12400      fill 12404      13 -14  %% square graphite bottom + air gap +
Al clad
cell 12421      12400      fill 12405      14 -17  %% axial interface
cell 12422      12400      fill 12406      17 -18  %% Fuel bottom

```

cell 12423	12400	fill 12407	18 -250	%% Added Region
cell 12424	12400	fill 12408	250 -251	%% Added Region
cell 12425	12400	fill 12409	251 -252	%% Added Region
cell 12426	12400	fill 12410	252 -19	%% Fuel2
cell 12427	12400	fill 12411	19 -20	%% Fuel1 top
cell 12428	12400	fill 12412	20 -23	%% aixal interface
cell 12429	12400	fill 12413	23 -25	%% square graphite w hole top + Oct
graphite with hole + air + Al clad				
cell 12430	12400	fill 12414	25 -26	%% Oct graphite XS region 2 -- top
cell 12431	12400	fill 12415	26 -27	%% Oct graphite XS region 1 -- top
cell 12432	12400	fill 12416	27	%% top fitting

%%%

% Define A15

% Description of Placement:

% Copy Universes

cell 12501	12501	fill 11001	-90	%% Axial Position to end at = 3.486
cell 12502	12502	fill 11002	-90	%% Axial Position to end at = 30.486
cell 12503	12503	fill 11003	-90	%% Axial Position to end at =
53.17475				
cell 12504	12504	fill 11004	-90	%% Axial Position to end at =
62.06475				
cell 12505	12505	fill 11005	-90	%% Axial Position to end at =
62.82675				
cell 12506	12506	fill 11006	-90	%% Axial Position to end at =
82.82675				
cell 12507	12507	fill 11006	-90	%% Added Lines for axial position
106.1655				
cell 12508	12508	fill 11006	-90	%% Added Lines for axial position
109.11825				
cell 12509	12509	fill 11006	-90	%% Added Lines for axial position
114.4205				
cell 12510	12510	fill 11007	-90	%% Axial Position to end at =
163.79425				
cell 12511	12511	fill 11008	-90	%% Axial Position to end at = 183.79425
cell 12512	12512	fill 11009	-90	%% Axial Position to end at =
184.55625				
cell 12513	12513	fill 11010	-90	%% Axial Position to end at =
206.6225				
cell 12514	12514	fill 11011	-90	%% Axial Position to end at =
220.2625				
cell 12515	12515	fill 11012	-90	%% Axial Position to end at =
247.2625				
cell 12516	12516	fill 11013	-90	%% All the way to the top

%% BUILD A15

cell 12517	12500	fill 12501	-11	%%	Steel Grid Plate + Aluminum
bottom fitting					
cell 12518	12500	fill 12502	11	-12	%% Oct graphite XS region 1 -- bottom
cell 12519	12500	fill 12503	12	-13	%% Oct graphite XS region 2 -- bottom
cell 12520	12500	fill 12504	13	-14	%% square graphite bottom + air gap +
Al clad					
cell 12521	12500	fill 12505	14	-17	%% axial interface
cell 12522	12500	fill 12506	17	-18	%% Fuel1 bottom
cell 12523	12500	fill 12507	18	-250	%% Added Region
cell 12524	12500	fill 12508	250	-251	%% Added Region
cell 12525	12500	fill 12509	251	-252	%% Added Region
cell 12526	12500	fill 12510	252	-19	%% Fuel2
cell 12527	12500	fill 12511	19	-20	%% Fuel1 top
cell 12528	12500	fill 12512	20	-23	%% axial interface
cell 12529	12500	fill 12513	23	-25	%% square graphite w hole top + Oct
graphite with hole + air + Al clad					
cell 12530	12500	fill 12514	25	-26	%% Oct graphite XS region 2 -- top
cell 12531	12500	fill 12515	26	-27	%% Oct graphite XS region 1 -- top
cell 12532	12500	fill 12516	27		%% top fitting

%%%%%%%%%

% Define A16

% Description of Placement:

% Copy Universes

cell 12601	12601	fill 11001	-90	%%	Axial Position to end at = 3.486
cell 12602	12602	fill 11002	-90	%%	Axial Position to end at = 30.486
cell 12603	12603	fill 11003	-90	%%	Axial Position to end at =
53.17475					
cell 12604	12604	fill 11004	-90	%%	Axial Position to end at =
62.06475					
cell 12605	12605	fill 11005	-90	%%	Axial Position to end at =
62.82675					
cell 12606	12606	fill 11006	-90	%%	Axial Position to end at =
82.82675					
cell 12607	12607	fill 11006	-90	%%	Added Lines for axial position
106.1655					
cell 12608	12608	fill 11006	-90	%%	Added Lines for axial position
109.11825					
cell 12609	12609	fill 11006	-90	%%	Added Lines for axial position
114.4205					
cell 12610	12610	fill 11007	-90	%%	Axial Position to end at =
163.79425					
cell 12611	12611	fill 11008	-90	%%	Axial Position to end at = 183.79425
cell 12612	12612	fill 11009	-90	%%	Axial Position to end at =
184.55625					

cell 12613	12613	fill 11010	-90	%% Axial Position to end at =
206.6225				
cell 12614	12614	fill 11011	-90	%% Axial Position to end at =
220.2625				
cell 12615	12615	fill 11012	-90	%% Axial Position to end at =
247.2625				
cell 12616	12616	fill 11013	-90	%% All the way to the top

%% BUILD A16

cell 12617	12600	fill 12601	-11	%% Steel Grid Plate + Aluminum
bottom fitting				
cell 12618	12600	fill 12602	11 -12	%% Oct graphite XS region 1 -- bottom
cell 12619	12600	fill 12603	12 -13	%% Oct graphite XS region 2 -- bottom
cell 12620	12600	fill 12604	13 -14	%% square graphite bottom + air gap +
Al clad				
cell 12621	12600	fill 12605	14 -17	%% axial interface
cell 12622	12600	fill 12606	17 -18	%% Fuel1 bottom
cell 12623	12600	fill 12607	18 -250	%% Added Region
cell 12624	12600	fill 12608	250 -251	%% Added Region
cell 12625	12600	fill 12609	251 -252	%% Added Region
cell 12626	12600	fill 12610	252 -19	%% Fuel2
cell 12627	12600	fill 12611	19 -20	%% Fuel1 top
cell 12628	12600	fill 12612	20 -23	%% axial interface
cell 12629	12600	fill 12613	23 -25	%% square graphite w hole top + Oct
graphite with hole + air + Al clad				
cell 12630	12600	fill 12614	25 -26	%% Oct graphite XS region 2 -- top
cell 12631	12600	fill 12615	26 -27	%% Oct graphite XS region 1 -- top
cell 12632	12600	fill 12616	27	%% top fitting

%%%%%%%%%%

% Define A17

% Description of Placement:

% Copy Universes

cell 12701	12701	fill 11001	-90	%% Axial Position to end at = 3.486
cell 12702	12702	fill 11002	-90	%% Axial Position to end at = 30.486
cell 12703	12703	fill 11003	-90	%% Axial Position to end at =
53.17475				
cell 12704	12704	fill 11004	-90	%% Axial Position to end at =
62.06475				
cell 12705	12705	fill 11005	-90	%% Axial Position to end at =
62.82675				
cell 12706	12706	fill 11006	-90	%% Axial Position to end at =
82.82675				
cell 12707	12707	fill 11006	-90	%% Added Lines for axial position
106.1655				

cell 12708	12708	fill 11006	-90	%% Added Lines for axial position
109.11825				
cell 12709	12709	fill 11006	-90	%% Added Lines for axial position
114.4205				
cell 12710	12710	fill 11007	-90	%% Axial Position to end at =
163.79425				
cell 12711	12711	fill 11008	-90	%% Axial Position to end at = 183.79425
cell 12712	12712	fill 11009	-90	%% Axial Position to end at =
184.55625				
cell 12713	12713	fill 11010	-90	%% Axial Position to end at =
206.6225				
cell 12714	12714	fill 11011	-90	%% Axial Position to end at =
220.2625				
cell 12715	12715	fill 11012	-90	%% Axial Position to end at =
247.2625				
cell 12716	12716	fill 11013	-90	%% All the way to the top
%% BUILD A17				
cell 12717	12700	fill 12701	-11	%% Steel Grid Plate + Aluminum
bottom fitting				
cell 12718	12700	fill 12702	11 -12	%% Oct graphite XS region 1 -- bottom
cell 12719	12700	fill 12703	12 -13	%% Oct graphite XS region 2 -- bottom
cell 12720	12700	fill 12704	13 -14	%% square graphite bottom + air gap +
Al clad				
cell 12721	12700	fill 12705	14 -17	%% axial interface
cell 12722	12700	fill 12706	17 -18	%% Fuel1 bottom
cell 12723	12700	fill 12707	18 -250	%% Added Region
cell 12724	12700	fill 12708	250 -251	%% Added Region
cell 12725	12700	fill 12709	251 -252	%% Added Region
cell 12726	12700	fill 12710	252 -19	%% Fuel2
cell 12727	12700	fill 12711	19 -20	%% Fuel1 top
cell 12728	12700	fill 12712	20 -23	%% axial interface
cell 12729	12700	fill 12713	23 -25	%% square graphite w hole top + Oct
graphite with hole + air + Al clad				
cell 12730	12700	fill 12714	25 -26	%% Oct graphite XS region 2 -- top
cell 12731	12700	fill 12715	26 -27	%% Oct graphite XS region 1 -- top
cell 12732	12700	fill 12716	27	%% top fitting

Rods.sss

%%
 %%
 %%

% Define B100 - Comp rods

%%
 %%
 %%

%% COPY UNIVERSES from Static Part

cell 1101 1101 fill 1001 -90 %% Axial Position to end at = 3.486

cell 1102 1102 fill 1002	-90 %% Axial Position to end at = 30.486
cell 1103 1103 fill 1003	-90 %% Axial Position to end at = 53.17475
cell 1104 1104 fill 1004	-90 %% Axial Position to end at = 62.06475
cell 1105 1105 fill 1005	-90 %% Axial Position to end at = 62.82675
cell 1106 1106 fill 1006	-90 %% Axial Position to end at = 82.82675
cell 1107 1107 fill 1007	-90 %% Axial Position to end at = 163.79425
cell 1108 1108 fill 1008	-90 %% Axial Position to end at = 183.79425
cell 1109 1109 fill 1009	-90 %% Axial Position to end at = 184.55625
cell 1110 1110 fill 1010	-90 %% Axial Position to end at = 206.6225
cell 1111 1111 fill 1011	-90 %% Axial Position to end at = 220.2625
cell 1112 1112 fill 1012	-90 %% Axial Position to end at = 247.2625
cell 1113 1113 fill 1013	-90 %% All the way to the top

% Copy Universes

cell 1120 1121 fill 801	-90 %% Axial Position to end at = 3.486
cell 1121 1122 fill 801	-90 %% Added Lines for axial position 12.486
cell 1122 1123 fill 801	-90 %% Added Lines for axial position 21.486
cell 1123 1124 fill 801	-90 %% Axial Position to end at = 30.486
cell 1124 1125 fill 801	-90 %% Added Lines for axial position 41.830375
cell 1125 1126 fill 801	-90 %% Axial Position to end at = 53.17475
cell 1126 1127 fill 801	-90 %% Axial Position to end at = 62.06475
cell 1127 1128 fill 801	-90 %% Axial Position to end at = 62.82675
cell 1128 1129 fill 801	-90 %% Added Lines for axial position 72.82675
cell 1129 1130 fill 801	-90 %% Axial Position to end at = 82.82675
cell 1130 1131 fill 801	-90 %% Added Lines for axial position 87.21075
cell 1131 1132 fill 801	-90 %% Added Lines for axial position 97.21075
cell 1132 1133 fill 801	-90 %% Added Lines for axial position 107.21075
cell 1133 1134 fill 801	-90 %% Added Lines for axial position 117.21075
cell 1134 1135 fill 801	-90 %% Added Lines for axial position 127.21075
cell 1135 1136 fill 801	-90 %% Added Lines for axial position 137.21075
cell 1136 1137 fill 801	-90 %% Added Lines for axial position 147.21075
cell 1137 1138 fill 801	-90 %% Added Lines for axial position 157.21075
cell 1138 1139 fill 801	-90 %% Axial Position to end at = 163.79425
cell 1139 1140 fill 801	-90 %% Added Lines for axial position 172.21075
cell 1140 1141 fill 801	-90 %% Axial Position to end at = 183.79425
cell 1141 1142 fill 801	-90 %% Axial Position to end at = 184.55625
cell 1142 1143 fill 801	-90 %% Added Lines for axial position 188.81075
cell 1143 1144 fill 801	-90 %% Added Lines for axial position 195.589375
cell 1144 1145 fill 801	-90 %% Axial Position to end at = 206.6225
cell 1145 1146 fill 801	-90 %% Axial Position to end at = 220.2625
cell 1146 1147 fill 801	-90 %% Added Lines for axial position 229.2625
cell 1147 1148 fill 801	-90 %% Added Lines for axial position 238.2625
cell 1148 1149 fill 801	-90 %% Axial Position to end at = 247.2625
cell 1149 1150 fill 801	-90 %% All the way to the top

%% BUILD complete CR element - outside CR

```

cell 1150 1100 fill 1101 51 -11 %% Steel Grid Plate + Aluminum bottom fitting
cell 1151 1100 fill 1102 51 11 -250 %% Added Region
cell 1152 1100 fill 1102 51 250 -251 %% Added Region
cell 1153 1100 fill 1102 51 251 -12 %% Oct graphite XS region 1 -- bottom
cell 1154 1100 fill 1103 51 12 -252 %% Added Region
cell 1155 1100 fill 1103 51 252 -13 %% Oct graphite XS region 2 -- bottom
cell 1156 1100 fill 1104 51 13 -14 %% square graphite bottom + air gap + Al clad
cell 1157 1100 fill 1105 51 14 -17 %% axial interface
cell 1158 1100 fill 1106 51 17 -253 %% Added Region
cell 1159 1100 fill 1106 51 253 -18 %% Fuel1 bottom
cell 1160 1100 fill 1107 51 18 -254 %% Added Region
cell 1161 1100 fill 1107 51 254 -255 %% Added Region
cell 1162 1100 fill 1107 51 255 -256 %% Added Region
cell 1163 1100 fill 1107 51 256 -257 %% Added Region
cell 1164 1100 fill 1107 51 257 -258 %% Added Region
cell 1165 1100 fill 1107 51 258 -259 %% Added Region
cell 1166 1100 fill 1107 51 259 -260 %% Added Region
cell 1167 1100 fill 1107 51 260 -261 %% Added Region
cell 1168 1100 fill 1107 51 261 -19 %% Fuel2
cell 1169 1100 fill 1108 51 19 -262 %% Added Region
cell 1170 1100 fill 1108 51 262 -20 %% Fuel1 top
cell 1171 1100 fill 1109 51 20 -23 %% axial interface
cell 1172 1100 fill 1110 51 23 -263 %% Added Region
cell 1173 1100 fill 1110 51 263 -264 %% Added Region
cell 1174 1100 fill 1110 51 264 -25 %% square graphite w hole top + Oct graphite with
hole + air + Al clad
cell 1175 1100 fill 1111 51 25 -26 %% Oct graphite XS region 2 -- top
cell 1176 1100 fill 1112 51 26 -265 %% Added Region
cell 1177 1100 fill 1112 51 265 -266 %% Added Region
cell 1178 1100 fill 1112 51 266 -27 %% Oct graphite XS region 1 -- top
cell 1179 1100 fill 1113 51 27 %% top fitting

```

%% BUILD complete CR element - inside CR

```

cell 1180 1100 fill 1121 -51 -11 %% Steel Grid Plate + Aluminum bottom fitting
cell 1181 1100 fill 1122 -51 11 -250 %% Added Region
cell 1182 1100 fill 1123 -51 250 -251 %% Added Region
cell 1183 1100 fill 1124 -51 251 -12 %% Oct graphite XS region 1 -- bottom
cell 1184 1100 fill 1125 -51 12 -252 %% Added Region
cell 1185 1100 fill 1126 -51 252 -13 %% Oct graphite XS region 2 -- bottom
cell 1186 1100 fill 1127 -51 13 -14 %% square graphite bottom + air gap + Al clad
cell 1187 1100 fill 1128 -51 14 -17 %% axial interface
cell 1188 1100 fill 1129 -51 17 -253 %% Added Region
cell 1189 1100 fill 1130 -51 253 -18 %% Fuel1 bottom
cell 1190 1100 fill 1131 -51 18 -254 %% Added Region
cell 1191 1100 fill 1132 -51 254 -255 %% Added Region
cell 1192 1100 fill 1133 -51 255 -256 %% Added Region

```

```

cell 1193 1100 fill 1134 -51 256 -257 %% Added Region
cell 1194 1100 fill 1135 -51 257 -258 %% Added Region
cell 1195 1100 fill 1136 -51 258 -259 %% Added Region
cell 1196 1100 fill 1137 -51 259 -260 %% Added Region
cell 1197 1100 fill 1138 -51 260 -261 %% Added Region
cell 1198 1100 fill 1139 -51 261 -19 %% Fuel2
cell 1199 1100 fill 1140 -51 19 -262 %% Added Region
cell 1200 1100 fill 1141 -51 262 -20 %% Fuel1 top
cell 1201 1100 fill 1142 -51 20 -23 %% axial interface
cell 1202 1100 fill 1143 -51 23 -263 %% Added Region
cell 1203 1100 fill 1144 -51 263 -264 %% Added Region
cell 1204 1100 fill 1145 -51 264 -25 %% square graphite w hole top + Oct graphite with
hole + air + Al clad
cell 1205 1100 fill 1146 -51 25 -26 %% Oct graphite XS region 2 -- top
cell 1206 1100 fill 1147 -51 26 -265 %% Added Region
cell 1207 1100 fill 1148 -51 265 -266 %% Added Region
cell 1208 1100 fill 1149 -51 266 -27 %% Oct graphite XS region 1 -- top
cell 1209 1100 fill 1150 -51 27 %% top fitting

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
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```

```
% Define B1200 - Comp rods
```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
%% COPY UNIVERSES from Static Part
```

```

cell 1301 1201 fill 1001 -90 %% Axial Position to end at = 3.486
cell 1302 1202 fill 1002 -90 %% Axial Position to end at = 30.486
cell 1303 1203 fill 1003 -90 %% Axial Position to end at = 53.17475
cell 1304 1204 fill 1004 -90 %% Axial Position to end at = 62.06475
cell 1305 1205 fill 1005 -90 %% Axial Position to end at = 62.82675
cell 1306 1206 fill 1006 -90 %% Axial Position to end at = 82.82675
cell 1307 1207 fill 1007 -90 %% Axial Position to end at = 163.79425
cell 1308 1208 fill 1008 -90 %% Axial Position to end at = 183.79425
cell 1309 1209 fill 1009 -90 %% Axial Position to end at = 184.55625
cell 1310 1210 fill 1010 -90 %% Axial Position to end at = 206.6225
cell 1311 1211 fill 1011 -90 %% Axial Position to end at = 220.2625
cell 1312 1212 fill 1012 -90 %% Axial Position to end at = 247.2625
cell 1313 1213 fill 1013 -90 %% All the way to the top

```

```
% Copy Universes
```

```

cell 1320 1221 fill 802 -90 %% Axial Position to end at = 3.486
cell 1321 1222 fill 802 -90 %% Added Lines for axial position 12.486
cell 1322 1223 fill 802 -90 %% Added Lines for axial position 21.486
cell 1323 1224 fill 802 -90 %% Axial Position to end at = 30.486
cell 1324 1225 fill 802 -90 %% Added Lines for axial position 41.830375
cell 1325 1226 fill 802 -90 %% Axial Position to end at = 53.17475

```

```

cell 1326 1227 fill 802 -90 %% Axial Position to end at = 62.06475
cell 1327 1228 fill 802 -90 %% Axial Position to end at = 62.82675
cell 1328 1229 fill 802 -90 %% Added Lines for axial position 72.82675
cell 1329 1230 fill 802 -90 %% Axial Position to end at = 82.82675
cell 1330 1231 fill 802 -90 %% Added Lines for axial position 87.21075
cell 1331 1232 fill 802 -90 %% Added Lines for axial position 97.21075
cell 1332 1233 fill 802 -90 %% Added Lines for axial position 107.21075
cell 1333 1234 fill 802 -90 %% Added Lines for axial position 117.21075
cell 1334 1235 fill 802 -90 %% Added Lines for axial position 127.21075
cell 1335 1236 fill 802 -90 %% Added Lines for axial position 137.21075
cell 1336 1237 fill 802 -90 %% Added Lines for axial position 147.21075
cell 1337 1238 fill 802 -90 %% Added Lines for axial position 157.21075
cell 1338 1239 fill 802 -90 %% Axial Position to end at = 163.79425
cell 1339 1240 fill 802 -90 %% Added Lines for axial position 172.21075
cell 1340 1241 fill 802 -90 %% Axial Position to end at = 183.79425
cell 1341 1242 fill 802 -90 %% Axial Position to end at = 184.55625
cell 1342 1243 fill 802 -90 %% Added Lines for axial position 188.81075
cell 1343 1244 fill 802 -90 %% Added Lines for axial position 195.589375
cell 1344 1245 fill 802 -90 %% Axial Position to end at = 206.6225
cell 1345 1246 fill 802 -90 %% Axial Position to end at = 220.2625
cell 1346 1247 fill 802 -90 %% Added Lines for axial position 229.2625
cell 1347 1248 fill 802 -90 %% Added Lines for axial position 238.2625
cell 1348 1249 fill 802 -90 %% Axial Position to end at = 247.2625
cell 1349 1250 fill 802 -90 %% All the way to the top

```

%% BUILD complete CR element - outside CR

```

cell 1350 1200 fill 1201 51 -11 %% Steel Grid Plate + Aluminum bottom fitting
cell 1351 1200 fill 1202 51 11 -250 %% Added Region
cell 1352 1200 fill 1202 51 250 -251 %% Added Region
cell 1353 1200 fill 1202 51 251 -12 %% Oct graphite XS region 1 -- bottom
cell 1354 1200 fill 1203 51 12 -252 %% Added Region
cell 1355 1200 fill 1203 51 252 -13 %% Oct graphite XS region 2 -- bottom
cell 1356 1200 fill 1204 51 13 -14 %% square graphite bottom + air gap + Al clad
cell 1357 1200 fill 1205 51 14 -17 %% axial interface
cell 1358 1200 fill 1206 51 17 -253 %% Added Region
cell 1359 1200 fill 1206 51 253 -18 %% Fuel1 bottom
cell 1360 1200 fill 1207 51 18 -254 %% Added Region
cell 1361 1200 fill 1207 51 254 -255 %% Added Region
cell 1362 1200 fill 1207 51 255 -256 %% Added Region
cell 1363 1200 fill 1207 51 256 -257 %% Added Region
cell 1364 1200 fill 1207 51 257 -258 %% Added Region
cell 1365 1200 fill 1207 51 258 -259 %% Added Region
cell 1366 1200 fill 1207 51 259 -260 %% Added Region
cell 1367 1200 fill 1207 51 260 -261 %% Added Region
cell 1368 1200 fill 1207 51 261 -19 %% Fuel2
cell 1369 1200 fill 1208 51 19 -262 %% Added Region

```

```

cell 1370 1200 fill 1208 51 262 -20  %% Fuel1 top
cell 1371 1200 fill 1209 51 20 -23  %% aixal interface
cell 1372 1200 fill 1210 51 23 -263  %% Added Region
cell 1373 1200 fill 1210 51 263 -264  %% Added Region
cell 1374 1200 fill 1210 51 264 -25  %% square graphite w hole top + Oct graphite with
hole + air + Al clad
cell 1375 1200 fill 1211 51 25 -26  %% Oct graphite XS region 2 -- top
cell 1376 1200 fill 1212 51 26 -265  %% Added Region
cell 1377 1200 fill 1212 51 265 -266  %% Added Region
cell 1378 1200 fill 1212 51 266 -27  %% Oct graphite XS region 1 -- top
cell 1379 1200 fill 1213 51 27  %% top fitting

```

%% BUILD complete CR element - inside CR

```

cell 1380 1200 fill 1221 -51 -11  %% Steel Grid Plate + Aluminum bottom fitting
cell 1381 1200 fill 1222 -51 11 -250  %% Added Region
cell 1382 1200 fill 1223 -51 250 -251  %% Added Region
cell 1383 1200 fill 1224 -51 251 -12  %% Oct graphite XS region 1 -- bottom
cell 1384 1200 fill 1225 -51 12 -252  %% Added Region
cell 1385 1200 fill 1226 -51 252 -13  %% Oct graphite XS region 2 -- bottom
cell 1386 1200 fill 1227 -51 13 -14  %% square graphite bottom + air gap + Al clad
cell 1387 1200 fill 1228 -51 14 -17  %% axial interface
cell 1388 1200 fill 1229 -51 17 -253  %% Added Region
cell 1389 1200 fill 1230 -51 253 -18  %% Fuel1 bottom
cell 1390 1200 fill 1231 -51 18 -254  %% Added Region
cell 1391 1200 fill 1232 -51 254 -255  %% Added Region
cell 1392 1200 fill 1233 -51 255 -256  %% Added Region
cell 1393 1200 fill 1234 -51 256 -257  %% Added Region
cell 1394 1200 fill 1235 -51 257 -258  %% Added Region
cell 1395 1200 fill 1236 -51 258 -259  %% Added Region
cell 1396 1200 fill 1237 -51 259 -260  %% Added Region
cell 1397 1200 fill 1238 -51 260 -261  %% Added Region
cell 1398 1200 fill 1239 -51 261 -19  %% Fuel2
cell 1399 1200 fill 1240 -51 19 -262  %% Added Region
cell 1400 1200 fill 1241 -51 262 -20  %% Fuel1 top
cell 1401 1200 fill 1242 -51 20 -23  %% aixal interface
cell 1402 1200 fill 1243 -51 23 -263  %% Added Region
cell 1403 1200 fill 1244 -51 263 -264  %% Added Region
cell 1404 1200 fill 1245 -51 264 -25  %% square graphite w hole top + Oct graphite with
hole + air + Al clad
cell 1405 1200 fill 1246 -51 25 -26  %% Oct graphite XS region 2 -- top
cell 1406 1200 fill 1247 -51 26 -265  %% Added Region
cell 1407 1200 fill 1248 -51 265 -266  %% Added Region
cell 1408 1200 fill 1249 -51 266 -27  %% Oct graphite XS region 1 -- top
cell 1409 1200 fill 1250 -51 27  %% top fitting

```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
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```

```
% Define B1300 - Comp rods
```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```
%% COPY UNIVERSES from Static Part
```

```

cell 1501 1301 fill 1001      -90 %% Axial Position to end at = 3.486
cell 1502 1302 fill 1002      -90 %% Axial Position to end at = 30.486
cell 1503 1303 fill 1003      -90 %% Axial Position to end at = 53.17475
cell 1504 1304 fill 1004      -90 %% Axial Position to end at = 62.06475
cell 1505 1305 fill 1005      -90 %% Axial Position to end at = 62.82675
cell 1506 1306 fill 1006      -90 %% Axial Position to end at = 82.82675
cell 1507 1307 fill 1007      -90 %% Axial Position to end at = 163.79425
cell 1508 1308 fill 1008      -90 %% Axial Position to end at = 183.79425
cell 1509 1309 fill 1009      -90 %% Axial Position to end at = 184.55625
cell 1510 1310 fill 1010      -90 %% Axial Position to end at = 206.6225
cell 1511 1311 fill 1011      -90 %% Axial Position to end at = 220.2625
cell 1512 1312 fill 1012      -90 %% Axial Position to end at = 247.2625
cell 1513 1313 fill 1013      -90 %% All the way to the top

```

```
% Copy Universes
```

```

cell 1520 1321 fill 803 -90 %% Axial Position to end at = 3.486
cell 1521 1322 fill 803 -90 %% Added Lines for axial position 12.486
cell 1522 1323 fill 803 -90 %% Added Lines for axial position 21.486
cell 1523 1324 fill 803 -90 %% Axial Position to end at = 30.486
cell 1524 1325 fill 803 -90 %% Added Lines for axial position 41.830375
cell 1525 1326 fill 803 -90 %% Axial Position to end at = 53.17475
cell 1526 1327 fill 803 -90 %% Axial Position to end at = 62.06475
cell 1527 1328 fill 803 -90 %% Axial Position to end at = 62.82675
cell 1528 1329 fill 803 -90 %% Added Lines for axial position 72.82675
cell 1529 1330 fill 803 -90 %% Axial Position to end at = 82.82675
cell 1530 1331 fill 803 -90 %% Added Lines for axial position 87.21075
cell 1531 1332 fill 803 -90 %% Added Lines for axial position 97.21075
cell 1532 1333 fill 803 -90 %% Added Lines for axial position 107.21075
cell 1533 1334 fill 803 -90 %% Added Lines for axial position 117.21075
cell 1534 1335 fill 803 -90 %% Added Lines for axial position 127.21075
cell 1535 1336 fill 803 -90 %% Added Lines for axial position 137.21075
cell 1536 1337 fill 803 -90 %% Added Lines for axial position 147.21075
cell 1537 1338 fill 803 -90 %% Added Lines for axial position 157.21075
cell 1538 1339 fill 803 -90 %% Axial Position to end at = 163.79425
cell 1539 1340 fill 803 -90 %% Added Lines for axial position 172.21075
cell 1540 1341 fill 803 -90 %% Axial Position to end at = 183.79425
cell 1541 1342 fill 803 -90 %% Axial Position to end at = 184.55625
cell 1542 1343 fill 803 -90 %% Added Lines for axial position 188.81075
cell 1543 1344 fill 803 -90 %% Added Lines for axial position 195.589375
cell 1544 1345 fill 803 -90 %% Axial Position to end at = 206.6225

```

```

cell 1545 1346 fill 803 -90 %% Axial Position to end at = 220.2625
cell 1546 1347 fill 803 -90 %% Added Lines for axial position 229.2625
cell 1547 1348 fill 803 -90 %% Added Lines for axial position 238.2625
cell 1548 1349 fill 803 -90 %% Axial Position to end at = 247.2625
cell 1549 1350 fill 803 -90 %% All the way to the top

```

%% BUILD complete CR element - outside CR

```

cell 1550 1300 fill 1301 51 -11 %% Steel Grid Plate + Aluminum bottom fitting
cell 1551 1300 fill 1302 51 11 -250 %% Added Region
cell 1552 1300 fill 1302 51 250 -251 %% Added Region
cell 1553 1300 fill 1302 51 251 -12 %% Oct graphite XS region 1 -- bottom
cell 1554 1300 fill 1303 51 12 -252 %% Added Region
cell 1555 1300 fill 1303 51 252 -13 %% Oct graphite XS region 2 -- bottom
cell 1556 1300 fill 1304 51 13 -14 %% square graphite bottom + air gap + Al clad
cell 1557 1300 fill 1305 51 14 -17 %% axial interface
cell 1558 1300 fill 1306 51 17 -253 %% Added Region
cell 1559 1300 fill 1306 51 253 -18 %% Fuel1 bottom
cell 1560 1300 fill 1307 51 18 -254 %% Added Region
cell 1561 1300 fill 1307 51 254 -255 %% Added Region
cell 1562 1300 fill 1307 51 255 -256 %% Added Region
cell 1563 1300 fill 1307 51 256 -257 %% Added Region
cell 1564 1300 fill 1307 51 257 -258 %% Added Region
cell 1565 1300 fill 1307 51 258 -259 %% Added Region
cell 1566 1300 fill 1307 51 259 -260 %% Added Region
cell 1567 1300 fill 1307 51 260 -261 %% Added Region
cell 1568 1300 fill 1307 51 261 -19 %% Fuel2
cell 1569 1300 fill 1308 51 19 -262 %% Added Region
cell 1570 1300 fill 1308 51 262 -20 %% Fuel1 top
cell 1571 1300 fill 1309 51 20 -23 %% axial interface
cell 1572 1300 fill 1310 51 23 -263 %% Added Region
cell 1573 1300 fill 1310 51 263 -264 %% Added Region
cell 1574 1300 fill 1310 51 264 -25 %% square graphite w hole top + Oct graphite with
hole + air + Al clad
cell 1575 1300 fill 1311 51 25 -26 %% Oct graphite XS region 2 -- top
cell 1576 1300 fill 1312 51 26 -265 %% Added Region
cell 1577 1300 fill 1312 51 265 -266 %% Added Region
cell 1578 1300 fill 1312 51 266 -27 %% Oct graphite XS region 1 -- top
cell 1579 1300 fill 1313 51 27 %% top fitting

```

%% BUILD complete CR element - inside CR

```

cell 1580 1300 fill 1321 -51 -11 %% Steel Grid Plate + Aluminum bottom fitting
cell 1581 1300 fill 1322 -51 11 -250 %% Added Region
cell 1582 1300 fill 1323 -51 250 -251 %% Added Region
cell 1583 1300 fill 1324 -51 251 -12 %% Oct graphite XS region 1 -- bottom
cell 1584 1300 fill 1325 -51 12 -252 %% Added Region
cell 1585 1300 fill 1326 -51 252 -13 %% Oct graphite XS region 2 -- bottom

```

```

cell 1586 1300 fill 1327 -51 13 -14  %% square graphite bottom + air gap + Al clad
cell 1587 1300 fill 1328 -51 14 -17  %% axial interface
cell 1588 1300 fill 1329 -51 17 -253 %% Added Region
cell 1589 1300 fill 1330 -51 253 -18  %% Fuel1 bottom
cell 1590 1300 fill 1331 -51 18 -254 %% Added Region
cell 1591 1300 fill 1332 -51 254 -255 %% Added Region
cell 1592 1300 fill 1333 -51 255 -256 %% Added Region
cell 1593 1300 fill 1334 -51 256 -257 %% Added Region
cell 1594 1300 fill 1335 -51 257 -258 %% Added Region
cell 1595 1300 fill 1336 -51 258 -259 %% Added Region
cell 1596 1300 fill 1337 -51 259 -260 %% Added Region
cell 1597 1300 fill 1338 -51 260 -261 %% Added Region
cell 1598 1300 fill 1339 -51 261 -19  %% Fuel2
cell 1599 1300 fill 1340 -51 19 -262 %% Added Region
cell 1600 1300 fill 1341 -51 262 -20  %% Fuel1 top
cell 1601 1300 fill 1342 -51 20 -23  %% axial interface
cell 1602 1300 fill 1343 -51 23 -263 %% Added Region
cell 1603 1300 fill 1344 -51 263 -264 %% Added Region
cell 1604 1300 fill 1345 -51 264 -25  %% square graphite w hole top + Oct graphite with
hole + air + Al clad
cell 1605 1300 fill 1346 -51 25 -26  %% Oct graphite XS region 2 -- top
cell 1606 1300 fill 1347 -51 26 -265 %% Added Region
cell 1607 1300 fill 1348 -51 265 -266 %% Added Region
cell 1608 1300 fill 1349 -51 266 -27  %% Oct graphite XS region 1 -- top
cell 1609 1300 fill 1350 -51 27      %% top fitting

```

Excel Data Tables

sss2_treat

Time Intervals	Power (MeV/sec)	Power (Watts)
0.05	5.04E+20	8.08E+07
0.1	2.69E+20	4.30E+07
0.15	1.36E+20	2.18E+07
0.2	1.95E+20	3.13E+07
0.25	2.70E+20	4.32E+07
0.3	1.72E+20	2.75E+07
0.35	1.41E+20	2.25E+07
0.4	1.14E+20	1.83E+07
0.45	1.57E+20	2.52E+07
0.5	3.90E+20	6.25E+07
0.55	9.80E+20	1.57E+08
0.6	8.50E+20	1.36E+08
0.65	3.72E+20	5.96E+07
0.7	4.96E+20	7.95E+07
0.75	1.16E+21	1.85E+08
0.8	4.50E+21	7.21E+08
0.85	1.88E+22	3.01E+09
0.9	1.99E+22	3.19E+09
0.95	7.25E+21	1.16E+09
1	6.31E+21	1.01E+09
1.05	1.78E+22	2.85E+09
1.1	1.76E+21	2.83E+08
1.15	1.31E+21	2.10E+08
1.2	1.27E+21	2.03E+08
1.25	6.89E+21	1.10E+09
1.3	1.09E+22	1.75E+09
1.35	1.96E+22	3.14E+09
1.4	5.83E+22	9.34E+09
1.45	5.83E+22	9.35E+09
1.5	6.69E+22	1.07E+10
1.55	6.72E+21	1.08E+09
1.6	1.16E+22	1.86E+09
1.65	7.73E+22	1.24E+10
1.7	7.54E+22	1.21E+10
1.75	6.68E+22	1.07E+10
1.8	6.49E+22	1.04E+10
1.85	3.31E+22	5.31E+09

1.9	6.91E+23	1.11E+11
1.95	2.01E+24	3.23E+11
2	1.35E+24	2.16E+11
2.05	3.59E+23	5.74E+10
2.1	2.39E+23	3.84E+10
2.15	2.26E+23	3.62E+10
2.2	4.64E+23	7.43E+10
2.25	3.29E+23	5.27E+10
2.3	7.47E+23	1.20E+11
2.35	1.27E+25	2.03E+12
2.4	2.89E+25	4.63E+12
2.45	1.47E+26	2.36E+13
2.5	5.15E+23	8.25E+10
2.55	3.44E+23	5.51E+10
2.6	1.60E+24	2.56E+11
2.65	1.58E+25	2.54E+12
2.7	8.18E+25	1.31E+13
2.75	5.06E+25	8.11E+12
2.8	3.29E+25	5.27E+12
2.85	1.59E+26	2.54E+13
2.9	3.54E+25	5.66E+12
2.95	6.86E+24	1.10E+12
3	4.27E+25	6.85E+12
Period:	3.78	0.264378382

L91-60-1

Time (seconds)	Energy Deposition MeV/sec	Energy Deposition (Watts)	Neutron Density
0.1	3.22E+12	1.30E-01	1.44E+07
0.2	3.02E+12	1.21E-01	1.37E+07
0.3	3.03E+12	1.22E-01	1.38E+07
0.4	4.27E+12	1.72E-01	1.92E+07
0.5	1.35E+13	5.45E-01	6.04E+07
0.6	4.52E+13	1.83E+00	2.01E+08
0.7	1.34E+14	5.42E+00	5.93E+08
0.8	4.60E+14	1.86E+01	2.06E+09
0.9	1.62E+15	6.53E+01	7.20E+09
1	5.68E+15	2.31E+02	2.55E+10
1.1	1.69E+16	6.81E+02	7.50E+10
1.2	5.57E+16	2.25E+03	2.48E+11
1.3	1.12E+17	4.52E+03	5.04E+11
1.4	5.82E+17	2.35E+04	2.56E+12

1.5	2.49E+18	1.00E+05	1.11E+13
1.6	3.77E+18	1.54E+05	1.75E+13
1.7	2.96E+18	1.21E+05	1.34E+13
1.8	1.20E+19	4.84E+05	5.32E+13
1.9	6.56E+19	2.65E+06	2.92E+14
2	2.18E+20	8.80E+06	9.68E+14
2.1	5.31E+20	2.14E+07	2.37E+15
2.2	3.16E+21	1.27E+08	1.37E+16
2.3	1.61E+22	6.50E+08	7.19E+16
2.4	6.58E+22	2.66E+09	2.93E+17
2.5	2.40E+23	9.63E+09	1.04E+18
2.6	8.74E+23	3.53E+10	3.90E+18
2.7	2.27E+24	9.15E+10	1.01E+19
2.8	7.21E+24	2.91E+11	3.19E+19
2.9	4.73E+25	1.91E+12	2.08E+20
3	1.92E+26	7.76E+12	8.54E+20

M8CAL (bad)

Time (seconds)	Neutron Population
0.025	2.60E+09
0.05	2.94E+09
0.075	6.01E+09
0.1	2.07E+10
0.125	9.33E+10
0.15	5.75E+11
0.175	2.59E+12
0.2	1.44E+13
0.225	8.71E+13
0.25	5.20E+14
0.275	4.57E+15
0.3	2.76E+16
0.325	2.22E+17
0.35	9.94E+17
0.375	6.66E+18
0.4	3.35E+19
0.425	1.12E+20
0.45	1.16E+21
0.475	8.05E+21
0.5	2.38E+22
0.525	9.04E+22

0.55	5.38E+23
0.575	4.01E+24
0.6	1.42E+25
0.625	5.77E+25
0.65	2.94E+26
0.675	7.50E+26
0.7	1.38E+27
0.725	8.22E+27
0.75	5.43E+28
0.775	1.70E+29
0.8	8.90E+29
0.825	4.41E+30
0.85	2.10E+31
0.875	3.68E+31
0.9	1.19E+32
0.925	2.20E+32
0.95	1.64E+33
0.975	1.72E+34
1	9.83E+34
1.025	2.44E+35
1.05	8.90E+35
1.075	2.25E+37
1.1	5.18E+37
1.125	6.50E+36
1.15	2.63E+37
1.175	1.19E+38
1.2	1.03E+39
1.225	4.28E+39
1.25	1.74E+40
1.275	9.19E+40
1.3	9.92E+40
1.325	2.47E+41
1.35	1.43E+42
1.375	1.22E+43
1.4	9.06E+43
1.425	5.86E+44
1.45	9.99E+45
1.475	4.84E+46
1.5	5.25E+47
1.525	3.86E+48
1.55	5.24E+49
1.575	3.63E+50
1.6	4.90E+50

1.625	1.96E+49
1.65	1.20E+50
1.675	1.04E+51
1.7	1.05E+51
1.725	3.54E+50
1.75	1.81E+50
1.775	8.26E+50
1.8	1.96E+51
1.825	4.12E+51
1.85	1.18E+52
1.875	2.91E+52
1.9	1.59E+53
1.925	1.06E+54
1.95	5.77E+54
1.975	2.40E+55
2	9.98E+55
2.025	5.35E+56
2.05	3.80E+57
2.075	1.83E+58
2.1	1.83E+58
2.125	8.33E+58
2.15	5.97E+59
2.175	1.27E+60
2.2	5.08E+60
2.225	3.90E+61
2.25	2.89E+62
2.275	1.49E+63
2.3	8.64E+63
2.325	5.54E+64
2.35	2.62E+65
2.375	2.51E+66
2.4	1.90E+67
2.425	7.39E+67
2.45	1.54E+68
2.475	4.03E+68
2.5	9.81E+68
2.525	5.37E+69
2.55	4.96E+70
2.575	5.73E+71
2.6	3.26E+72
2.625	3.31E+73
2.65	1.81E+74
2.675	6.82E+74

2.7	3.68E+75
2.725	2.88E+75
2.75	4.82E+73
2.775	4.34E+73
2.8	2.15E+73
2.825	1.79E+74
2.85	1.03E+75
2.875	8.14E+75
2.9	5.37E+76
2.925	4.60E+77
2.95	2.79E+78
2.975	8.65E+78
3	1.14E+79

1.5% delta k/k

Average Neutron Population	Average error	Average abs stdv	Average variance
5.27E+09	0.02068	1.09E+08	1.19E+16
6.97E+09	0.04275	2.98E+08	8.89E+16
1.15E+10	0.06111	7.00E+08	4.91E+17
2.16E+10	0.08417	1.82E+09	3.31E+18
4.03E+10	0.11313	4.56E+09	2.07E+19
1.23E+11	0.13474	1.66E+10	2.76E+20
1.12E+11	0.16141	1.81E+10	3.29E+20
1.46E+11	0.18199	2.65E+10	7.02E+20
2.38E+11	0.20613	4.90E+10	2.40E+21
3.98E+11	0.23452	9.33E+10	8.70E+21
6.29E+11	0.26517	1.67E+11	2.78E+22
1.14E+12	0.30699	3.51E+11	1.23E+23
3.02E+12	0.36681	1.11E+12	1.23E+24
6.73E+12	0.40246	2.71E+12	7.33E+24
5.77E+12	0.43332	2.50E+12	6.25E+24
1.06E+13	0.47596	5.06E+12	2.56E+25
1.26E+13	0.50186	6.33E+12	4.01E+25
2.15E+13	0.52576	1.13E+13	1.27E+26
2.80E+13	0.53988	1.51E+13	2.28E+26
5.23E+13	0.56570	2.96E+13	8.77E+26
6.76E+13	0.55486	3.75E+13	1.41E+27
1.52E+14	0.58830	8.93E+13	7.97E+27
1.13E+15	0.59657	6.73E+14	4.52E+29
1.17E+16	0.59556	6.99E+15	4.89E+31

5.24E+15	0.61344	3.21E+15	1.03E+31
4.59E+15	0.60329	2.77E+15	7.68E+30
6.48E+15	0.60399	3.91E+15	1.53E+31
3.94E+15	0.60911	2.40E+15	5.77E+30
7.39E+15	0.60807	4.49E+15	2.02E+31
2.17E+16	0.60948	1.32E+16	1.75E+32
1.16E+16	0.62177	7.24E+15	5.24E+31
1.07E+16	0.63698	6.80E+15	4.62E+31
1.24E+16	0.66668	8.26E+15	6.82E+31
1.37E+16	0.67706	9.28E+15	8.62E+31
1.71E+16	0.67616	1.16E+16	1.34E+32
3.35E+16	0.67187	2.25E+16	5.06E+32
9.19E+16	0.66837	6.14E+16	3.77E+33
9.85E+16	0.68009	6.70E+16	4.49E+33
5.11E+16	0.69992	3.58E+16	1.28E+33
8.83E+16	0.69521	6.14E+16	3.77E+33

Slope	7.730836262
Period (seconds)	0.130471925
Standard Deviation	0.01231

Power (Average)	Error	Average abs stdv	Average variance
5092.415	0.0218512	1.112753786	1.238220989
6807.224118	0.04358	2.96658827	8.800645966
11244.85706	0.061818	6.951345737	48.32120755
21179.03235	0.0850918	18.02161985	324.7787821
39772.74412	0.1137942	45.25907599	2048.383959
127042.3794	0.135614	172.2872524	29682.89734
106325.9735	0.1619184	172.1613151	29639.51842
142406.2853	0.1828388	260.3739432	67794.59027
231655.0294	0.2069022	479.2993523	229727.8691
389277	0.2358892	918.2624011	843205.8372
614892.4412	0.2666606	1639.675873	2688536.968
1123785.206	0.3087014	3469.140664	12034936.94
2973915.882	0.3685826	10961.33648	120150897.4
6438674.735	0.402657	25925.77453	672145784.9
5668130.353	0.4339446	24596.54559	604990054.8
10535226.18	0.4768028	50232.2534	2523279281
12330345	0.5029108	62010.63668	3845319062
20696506.76	0.5250492	108666.8432	11808482810
27569935.59	0.5408332	149107.3649	22233006261

51491279.41	0.5653564	291109.2436	84744591707
65791970.59	0.5548076	365018.853	1.33239E+11
156493556.5	0.5899896	923295.7078	8.52475E+11
1168518456	0.5956318	6960067.512	4.84425E+13
12377531915	0.5958094	73746498.64	5.43855E+15
4418393494	0.6120482	27042697.85	7.31308E+14
4672659632	0.6021964	28138588.09	7.9178E+14
6211907203	0.6034712	37487070.94	1.40528E+15
3883156244	0.6085154	23629603.75	5.58358E+14
7175043426	0.6080148	43625325.94	1.90317E+15
22725918100	0.609663	138551514.1	1.91965E+16
9346881491	0.623082	58238736.13	3.39175E+15
10376583891	0.6374154	66141943.72	4.37476E+15
11740334676	0.6679816	78423275.42	6.15021E+15
13396724265	0.6773466	90742256.32	8.23416E+15
16435244676	0.6748678	110916174.2	1.23024E+16
33652780971	0.6728758	226441419.2	5.12757E+16
88940699765	0.6688252	594857813.1	3.53856E+17
94755332118	0.6804478	644760572.8	4.15716E+17
50200974294	0.7003766	351595876.9	1.2362E+17
86919280206	0.694878	603982955.9	3.64795E+17

Slope	7.735570338
Period (seconds)	0.130399765
Standard Deviation	0.012350098

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